

CK Engineering LLC.

19229 38th PL NE
Lake Forest Park, WA 98155

Phone: (206) 417-0670

STRUCTURAL CALCULATIONS
Lateral & Gravity Design
23-043



12/8/2023

NEW HOME AT:
6715 SE 27TH ST.
Mercer Island, WA 98040
December 8, 2023

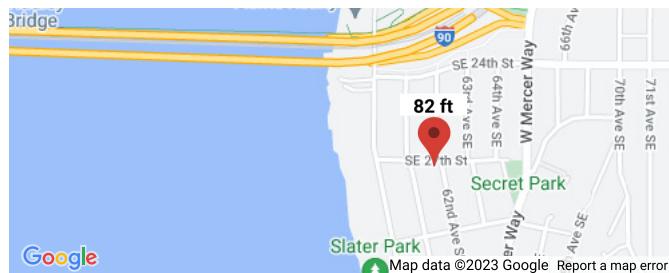
⚠ This is a beta release of the new ATC Hazards by Location website. Please [contact us](#) with feedback.

ⓘ The ATC Hazards by Location website will not be updated to support ASCE 7-22. [Find out why.](#)



Search Information

Address: 6175 SE 27th St, Mercer Island, WA 98040, USA
Coordinates: 47.5868832, -122.2510951
Elevation: 82 ft
Timestamp: 2023-11-24T21:05:14.358Z
Hazard Type: Wind



ASCE 7-16

MRI 10-Year	67 mph
MRI 25-Year	73 mph
MRI 50-Year	78 mph
MRI 100-Year	83 mph
Risk Category I	92 mph
Risk Category II	97 mph
Risk Category III	104 mph
Risk Category IV	108 mph

ASCE 7-10

MRI 10-Year	72 mph
MRI 25-Year	79 mph
MRI 50-Year	85 mph
MRI 100-Year	91 mph
Risk Category I	100 mph
Risk Category II	110 mph
Risk Category III-IV	115 mph

ASCE 7-05

ASCE 7-05 Wind Speed	85 mph
----------------------	--------

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

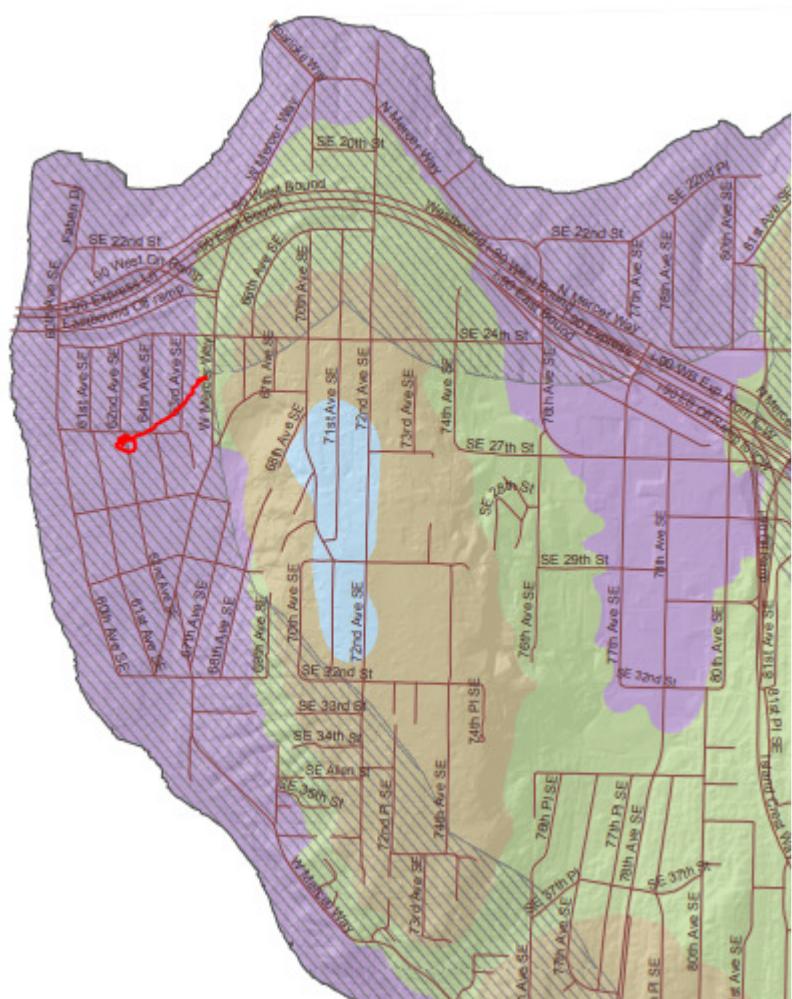
Please note that the ATC Hazards by Location website will not be updated to support ASCE 7-22. [Find out why.](#)

Disclaimer

Hazard loads are interpolated from data provided in ASCE 7 and rounded up to the nearest whole integer. Per ASCE 7, islands and coastal areas outside the last contour should use the last wind speed contour of the coastal area – in some cases, this website will extrapolate past the last wind speed contour and therefore, provide a wind speed that is slightly higher. NOTE: For queries near wind-borne debris region boundaries, the resulting determination is sensitive to rounding which may affect whether or not it is considered to be within a wind-borne debris region.

Mountainous terrain, gorges, ocean promontories, and special wind regions shall be examined for unusual wind conditions.

While the information presented on this website is believed to be correct, ATC and its sponsors and contributors assume no responsibility or liability for its accuracy. The material presented in the report should not be used or relied upon for any specific application without competent examination and verification of its accuracy, suitability and applicability by engineers or other licensed professionals. ATC does not intend that the use of this information replace the sound judgment of such competent professionals, having experience and knowledge in the field of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the results of the report provided by this website. Users of the information from this website assume all liability arising from such use. Use of the output of this website does not imply approval by the governing building code bodies responsible for building code approval and interpretation for the building site described by latitude/longitude location in the report.



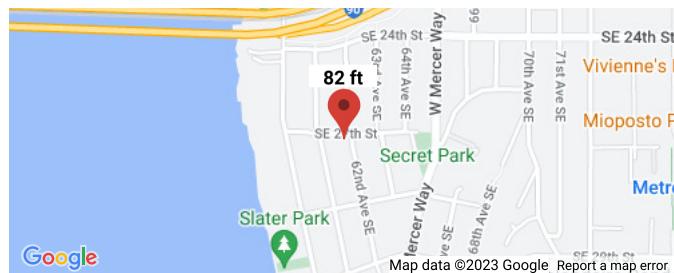
⚠ This is a beta release of the new ATC Hazards by Location website. Please [contact us](#) with feedback.

ⓘ The ATC Hazards by Location website will not be updated to support ASCE 7-22. [Find out why.](#)

ATC Hazards by Location

Search Information

Address:	6175 SE 27th St, Mercer Island, WA 98040, USA
Coordinates:	47.5868832, -122.2510951
Elevation:	82 ft
Timestamp:	2023-11-24T21:06:19.670Z
Hazard Type:	Seismic
Reference Document:	ASCE7-16
Risk Category:	I
Site Class:	D-default



Basic Parameters

Name	Value	Description
S_S	1.4	MCE _R ground motion (period=0.2s)
S_1	0.488	MCE _R ground motion (period=1.0s)
S_{MS}	1.68	Site-modified spectral acceleration value
S_{M1}	* null	Site-modified spectral acceleration value
S_{DS}	1.12	Numeric seismic design value at 0.2s SA
S_{D1}	* null	Numeric seismic design value at 1.0s SA

* See Section 11.4.8

Additional Information

Name	Value	Description
SDC	* null	Seismic design category
F_a	1.2	Site amplification factor at 0.2s
F_v	* null	Site amplification factor at 1.0s
CR_S	0.902	Coefficient of risk (0.2s)
CR_1	0.896	Coefficient of risk (1.0s)
PGA	0.599	MCE _G peak ground acceleration
F_{PGA}	1.2	Site amplification factor at PGA
PGA_M	0.719	Site modified peak ground acceleration
T_L	6	Long-period transition period (s)
SsRT	1.4	Probabilistic risk-targeted ground motion (0.2s)
SsUH	1.552	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
SsD	3.202	Factored deterministic acceleration value (0.2s)
S1RT	0.488	Probabilistic risk-targeted ground motion (1.0s)
S1UH	0.544	Factored uniform-hazard spectral acceleration (2% probability of exceedance in 50 years)
S1D	1.307	Factored deterministic acceleration value (1.0s)
PGAd	1.106	Factored deterministic acceleration value (PGA)

* See Section 11.4.8

The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

Please note that the ATC Hazards by Location website will not be updated to support ASCE 7-22. [Find out why.](#)

Disclaimer

Hazard loads are provided by the U.S. Geological Survey [Seismic Design Web Services](#).

While the information presented on this website is believed to be correct, ATC and its sponsors and contributors assume no responsibility or liability for its accuracy. The material presented in the report should not be used or relied upon for any specific application without competent examination and verification of its accuracy, suitability and applicability by engineers or other licensed professionals. ATC does not intend that the use of this information replace the sound judgment of such competent professionals, having experience and knowledge in the field of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the results of the report provided by this website. Users of the information from this website assume all liability arising from such use. Use of the output of this website does not imply approval by the governing building code bodies responsible for building code approval and interpretation for the building site described by latitude/longitude location in the report.

Design Criteria

Scope of Work:	Lateral & Gravity Design	
Site Address:	6715 SE 27TH ST. Mercer Island, WA 98040	
Number of Stories:	3	Engineer: PK

Roof Loading

Roofing	Torch Down	2.0
Sheathing	3/4" Plywood	2.3
Insulation	Roll/Batt	3.0
Ceiling	5/8" GWB	2.8
Framing	Rafters & Beams	3.0
Miscellaneous	fixtures, mechanical, electrical, etc.	1.9
TOTAL DEAD LOAD:		15.0 psf

ROOF SNOW LOAD: 25.0 psf**Upper Floor Loading**

Floor Covering	Carpet/Hardwood/Tile	3.0
Sheathing	3/4" T&G	2.3
Ceiling	1/2" GWB	2.2
Joists	I-Joists	2.1
Beams		4.0
Miscellaneous	fixtures, mechanical, electrical, etc.	1.4
TOTAL DEAD LOAD:		15.0 psf

FLOOR LIVE LOAD: 40.0 psf**Main Floor Loading**

Floor Covering	Carpet/Hardwood/Tile	3.0
Sheathing	3/4" T&G	2.3
Ceiling	5/8" GWB	2.8
Joists	I-Joists	2.1
Beams		4.2
Miscellaneous	fixtures, mechanical, electrical, etc.	0.6
TOTAL DEAD LOAD:		15.0 psf

FLOOR LIVE LOAD: 40.0 psf

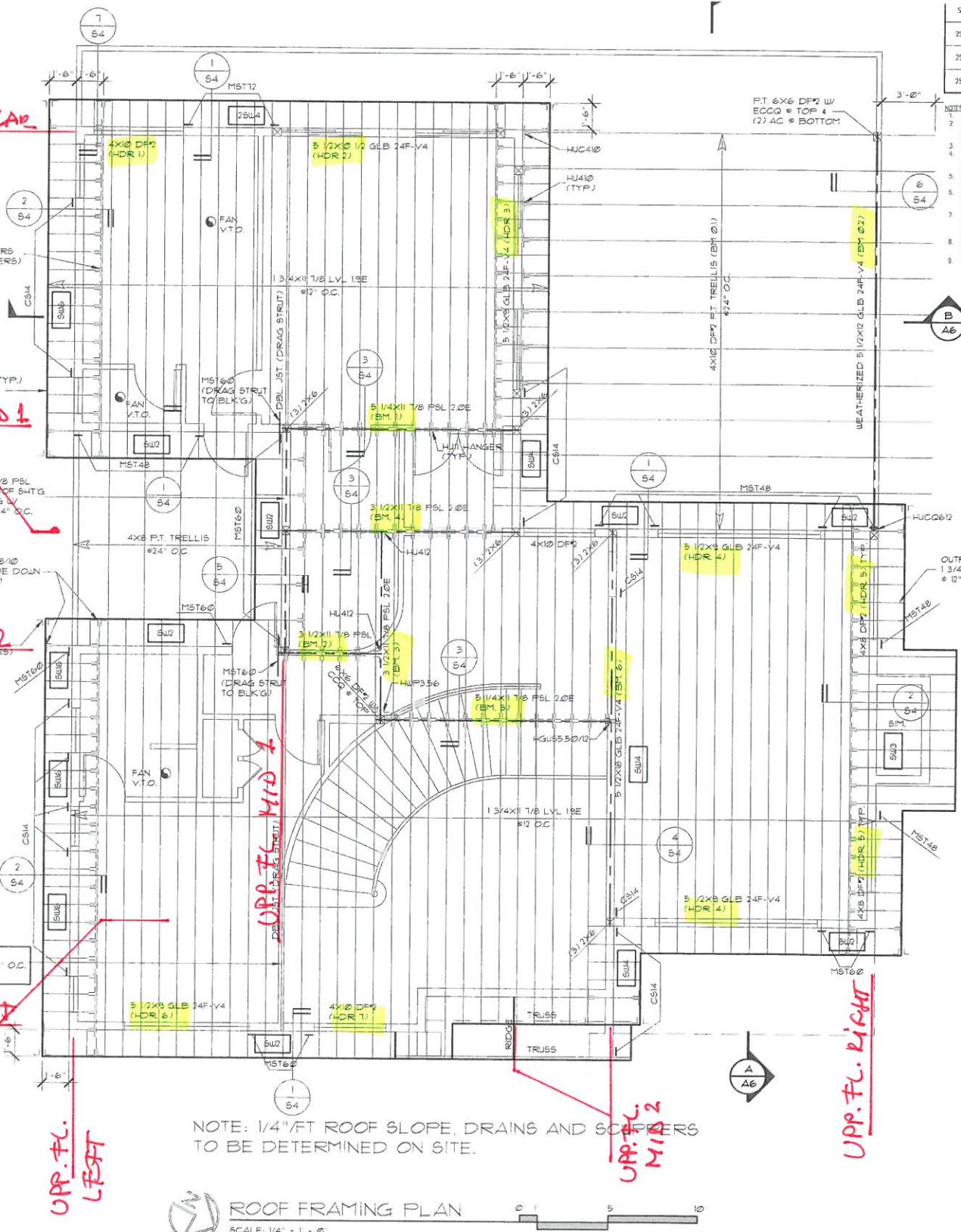
Soil Bearing Capacity:	1500 psf
Frost Depth:	18 in

LATERAL & GRAVITY DESIGN

KFRY PLANS

SW-2	15/32"
2SW-4	15/32" BOTH
2SW-3	15/32" BOTH
2SW-2	15/32" BOTH

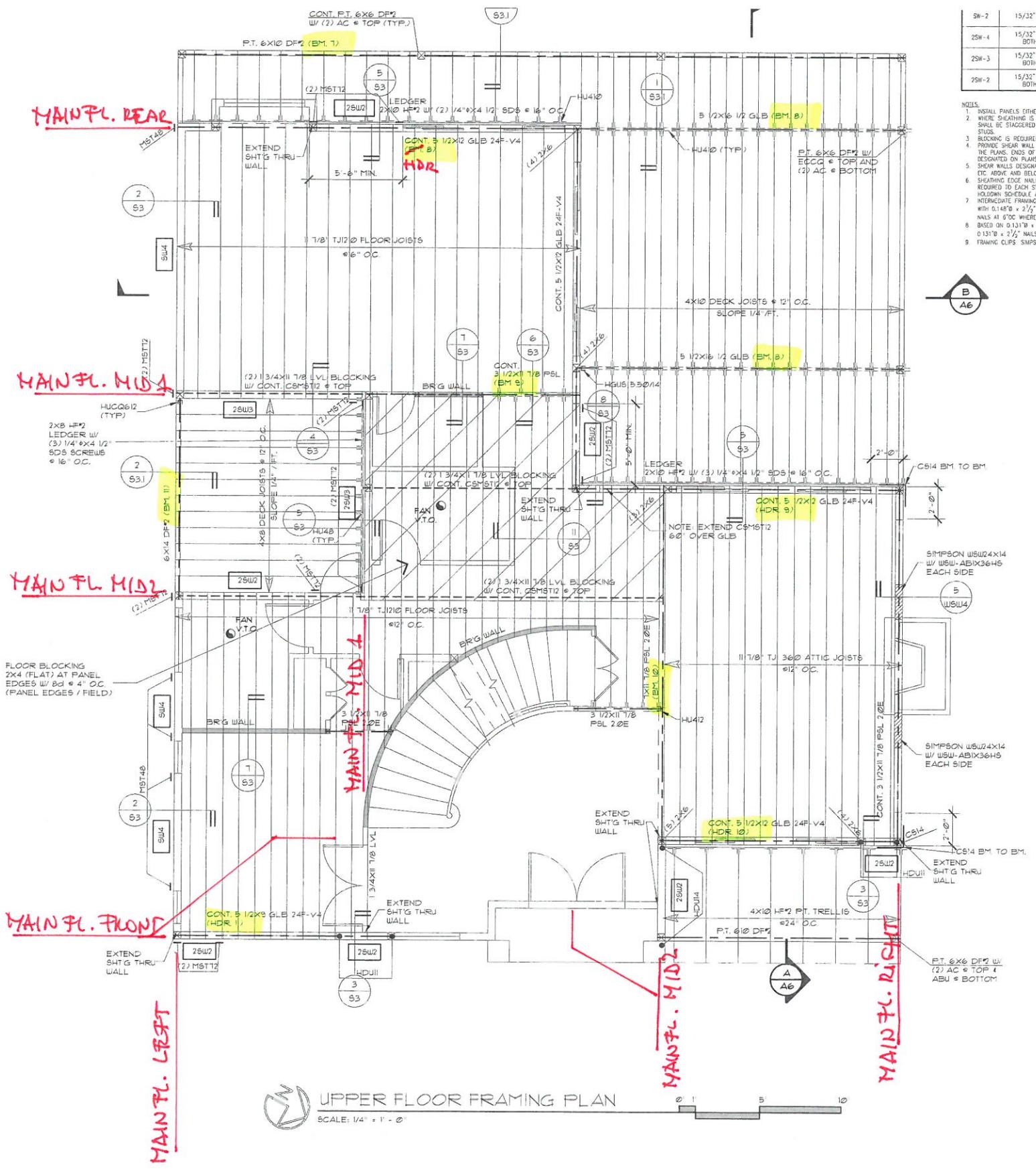
NOTES:
 1. INSTALL PANELS EITHER
 2. WHERE SHEATHING IS A
 3. BLOCKING IS REQUIRED
 4. PLYWOOD SHEATHING IS
 5. SHEAR WALLS DESCRIBED
 6. SHEATHING EDGE NAILIN
 7. INTERMEDIATE FRAMING
 8. BASED ON 0.131" B x
 9. 0.131" x 2 1/2" NAILS
 10. FRAMING CLIPS SIMPSO



SW-2	15/32" C
SW-4	15/32" C BOTH S
SW-3	15/32" C BOTH S
SW-2	15/32" C BOTH S

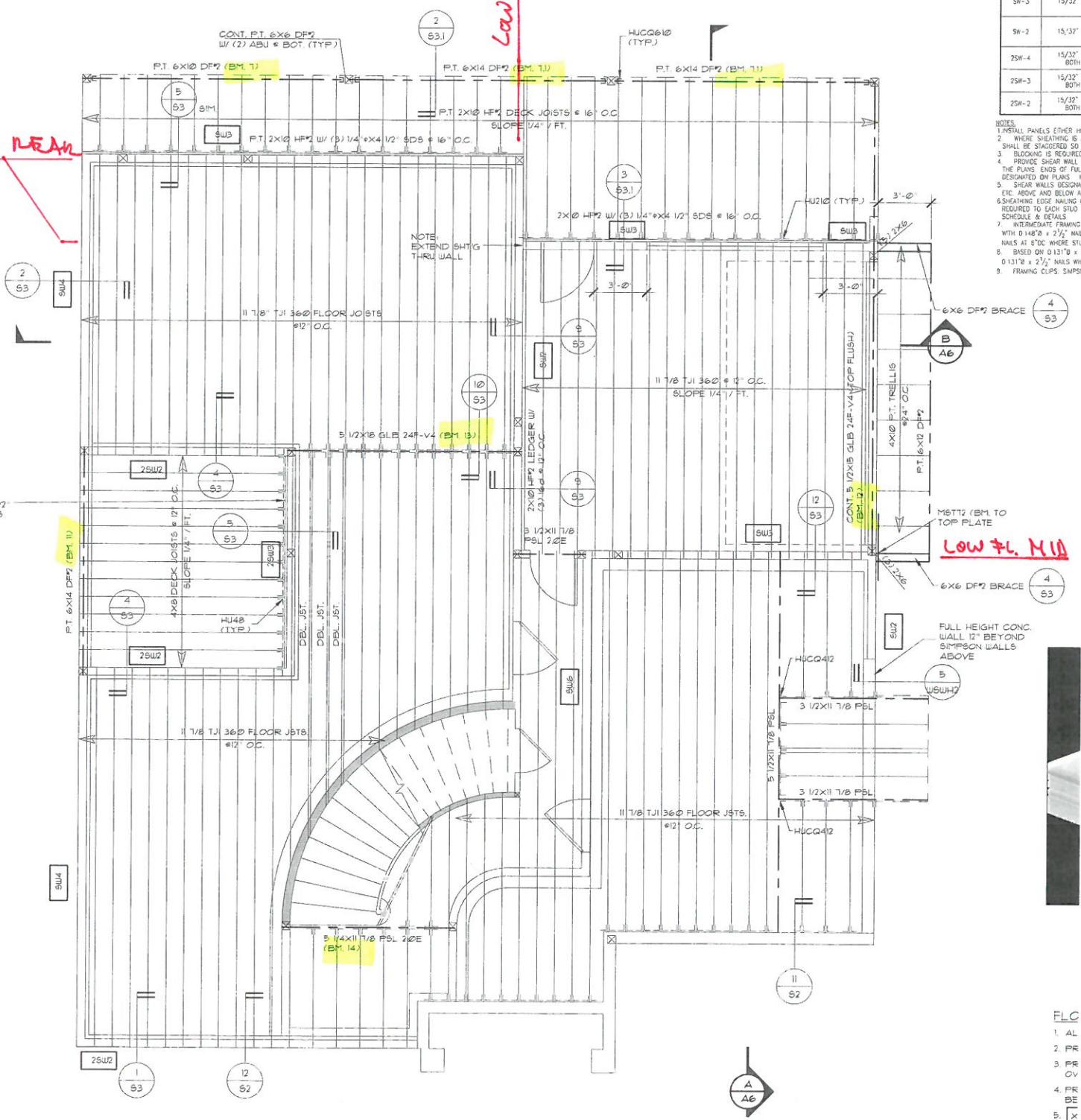
NOTES:

1. INSTALL PANELS EITHER WHERE SHEATHING IS AF SHD OR BE STAGGERED S STUDS.
2. PROVIDE SHEAR WALL IN THE FORM OF A PLATE OR DESIGNATED ON PLANS.
3. SHEATHING EDGE MUST BE ATTACHED TO THE STUDS AS DESIGNATED ON PLANS.
4. PROVIDE SHEAR WALL IN THE FORM OF A PLATE OR DESIGNATED ON PLANS.
5. SHEATH WALL DESIGNATE THE EDGE ABOVE AND BELOW THE SHEATHING.
6. SHEATHING EDGE MUST BE REQUIRED TO EACH STUD HOLDOWN SCHEDULE & ATTACHMENT.
7. ATTACH SHEATHING TO STUDS WITH 0.14" Ø x 2 1/2" NAILS AT 6" OC WHERE S.
8. BASED ON 0.131"Ø x 1 1/2" NAILS 1 0.131"Ø x 2 1/2" NAILS 1
9. FRAMING CLIPS SIMPSO



SW-3	15/32" C
SW-2	15/32" C
2SW-4	15/32" C BOTH
2SW-3	15/32" C BOTH
2SW-2	15/32" C BOTH

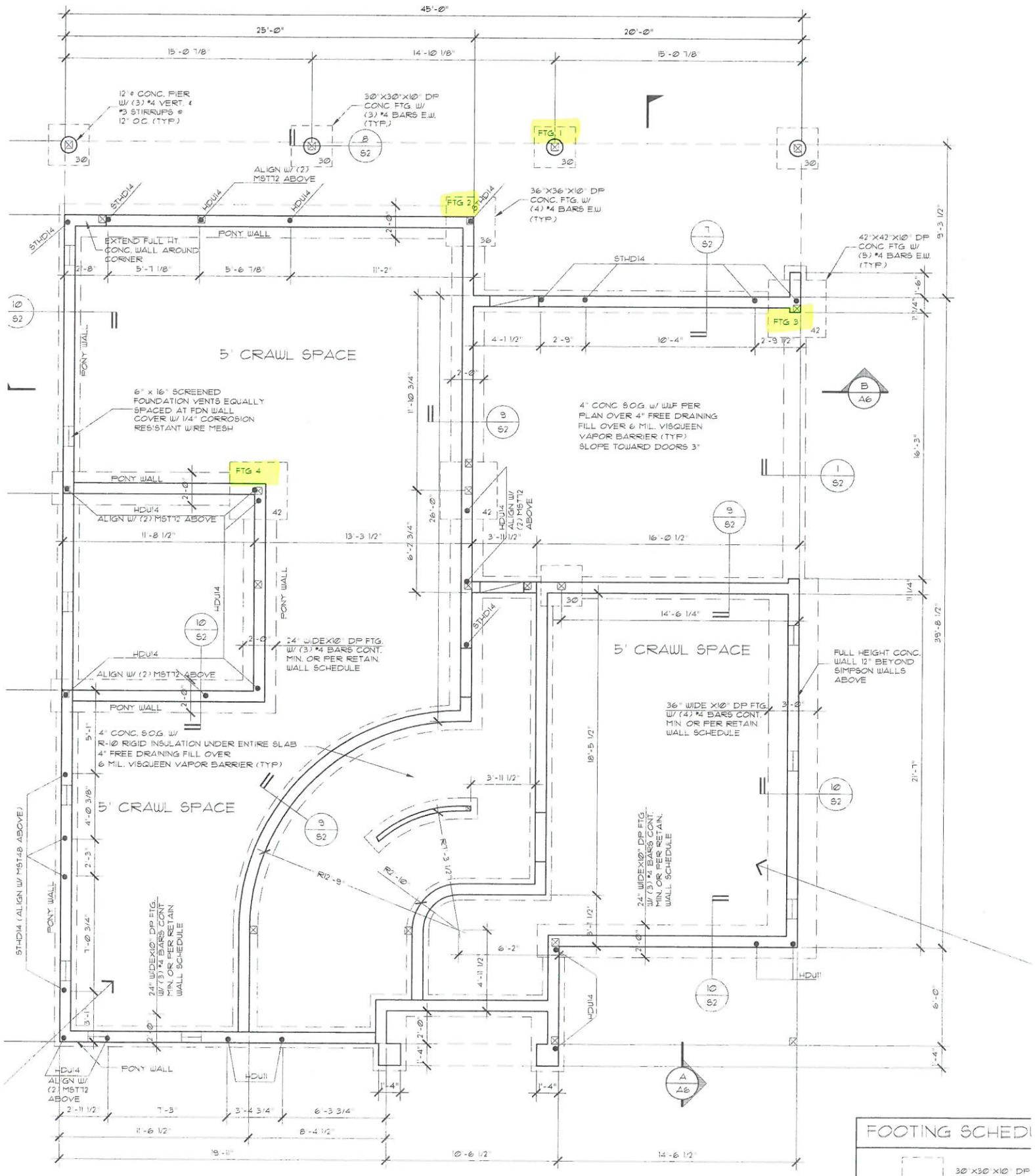
NOTES:
1. INST. PANELS FINGER JOINT
2. WHERE SHEATHING IS A
SHALL BE STAGED SO 1
3. BLOCKING IS REQUIRED
4. PROVIDED SHEATHING WALL.
5. THE PLANS INDICATE WALLS
DESIGNED FOR STUCCO.
6. SHEAR WALLS DESIGN
FOR ABOVE AND BELOW AL
7. SHEATHING MUST BE
REQUIRED TO EACH STUD.
8. SCHEDULE & DETAILS
9. INTERIOR FRAMING
WITH 0.14" X 2" NAILS
NAILS AT 6 OC WHERE STU
10. BASED ON 0.131" X 1
0.131" X 2" NAILS WHI
11. FRAMING CLIPS SPACED



MAIN FLOOR FRAMING PLAN

SCALE: 1/4" = 1 - 0"

Joint
block
attac
edjo
Addl
restri
secti



WIND LOAD CALCULATIONS
LEFT —————→ **RIGHT**

ΣV 3RD FLOOR =

WIND ZONE	A	C										
AVE. HEIGHT	6	6										
AVE. WIDTH	9	46										
Ps	16.01	10.58	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
SUBTOTAL	864	2920	0	0	0	0	0	0	0	0	0	0
TOTAL	3,784 lbs											

ΣV 2ND FLOOR =

WIND ZONE	A	C										
AVE. HEIGHT	10.5	10.5										
AVE. WIDTH	9	46										
Ps	16.01	10.58	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
SUBTOTAL	1513	5110	0	0	0	0	0	0	0	0	0	0
TOTAL	6,623 lbs											

ΣV (1ST FLOOR) =

WIND ZONE	A	C	C									
AVE. HEIGHT	10.5	10.5	7.5									
AVE. WIDTH	9	15	22									
Ps	16.01	10.58	10.58	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
SUBTOTAL	1513	1666	1746	0	0	0	0	0	0	0	0	0
TOTAL	4,925 lbs											

ρ CALCS:

3RD FLOOR CALCULATIONS:

Plate Height:	9.00 ft
Total length of Shearwall in Shortest Line:	12.00 ft
Length of Shortest Segment within Shear Line:	3.00 ft
Length of Longest Segment in Shear Line:	3.00 ft

Tributary Area:	1.0
Total Area:	2.0

$$\rho = \boxed{1.00}$$

ASCE 7-16 12.3.4.2 b

2ND FLOOR CALCULATIONS:

Plate Height:	9.00 ft
Total length of Shearwall in Shortest Line:	9.00 ft
Length of Shortest Shearwall within Shear Line:	3.00 ft
Length of Longest Wall in Shear Line:	3.00 ft

Tributary Area:	1.0
Total Area:	2.0

$$\rho = \boxed{1.00}$$

ASCE 7-16 12.3.4.2 b

MAIN FLOOR CALCULATIONS:

Plate Height:	9.00 ft
Total length of Shearwall in Shortest Line:	10.00 ft
Length of Shortest Shearwall within Shear Line:	4.50 ft
Length of Longest Wall in Shear Line:	5.50 ft

Tributary Area:	1.0
Total Area:	2.0

$$\rho = \boxed{1.00}$$

ASCE 7-16 12.3.4.2 b

WIND (front-rear)	
ΣV (3RD) =	3307 lbs
ΣV (2ND) =	5788 lbs
ΣV (MAIN) =	4661 lbs
TOTAL =	13757 lbs

WIND (left-right)	
	3784 lbs
	6623 lbs
	4925 lbs
	15331 lbs

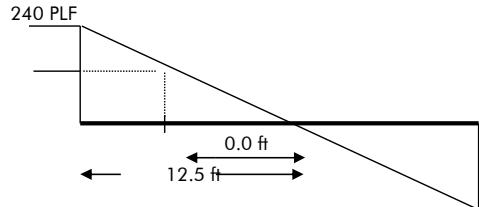
SEISMIC	
	17281 lbs
	12564 lbs
	4742 lbs
	34587 lbs

DIAPHRAGM SHEAR:

Total diaphragm length = 50.0 ft
Sub-diaphragm length = 22.0 ft
Diaphragm width = 25.0 ft
 ΣV (3RD) = 17,281 lbs

$$v = \frac{\Sigma V(\text{roof})}{(2)(\text{width})} = \frac{7604 \text{ lb}}{50 \text{ ft}} = 152 \text{ PLF}$$

IBC Table 2306.3.1 → 240 PLF



USE 15/32 CDX ROOF SHEATHING OR 3/4 T&G CDX SUBFLOORING w/8d AT 6 in o/c(PANEL EDGE), END 8d AT 12in o/c(PANEL FIELD)

CHORD:

Sub-diaphragm length = 22.0 ft Total-diaphragm length = 50.0 ft
Sub-diaphragm width = 25.0 ft

$$T = \frac{M}{B} = \frac{\Sigma V \times (\text{diaphragm length})}{8 \times (\text{diaphragm width})} = \frac{7604}{8} \times \frac{22 \text{ ft}}{25 \text{ ft}} = 836 \text{ lbs}$$

Top Plate Size: 2x6 Species/Grade: HF #2

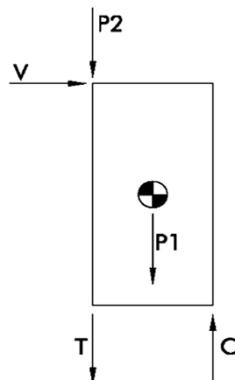
Area = 8.25 in ^ 2 $F_t = 525 \text{ psi}$
Load duration (C_D) = 1.33 $T_{\text{allowable}} = \text{Area} \times C_D \times F_t = 5,761 \text{ lbs}$

Since $T_{\text{allowable}}$ is greater than T_{applied} , OK.

SHEAR CAPACITY OF 10d COMMON NAIL = 102 lbs $102 \times C_d \times p = 136 \text{ lbs}$ 2018 NDS

$$\# \text{ OF NAILS PER 4 FT SPLICE} = \frac{836 \text{ lbs}}{136 \text{ lbs}} = 6$$

USE 2x6 HF #2 TOP PLATE W/ (8) 10d COMMON NAILS PER SPLICE.

Lateral Calculation Key

V = Shear, plf
 H = Height of shearwall
 L = Length of shearwall
 $P1$ = Weight of shearwall and connected framing
 $P2$ = Weight of adjacent wall

$T = V \times H - 0.5P1 - P2$ = Tension reaction to be resisted by holdown
 $C = V \times H + 0.5P1$ = Compression reaction

ASD Basic Load Combinations

For calculation of tension and compression forces in compliance with ASCE 7-16 2.4.1

Tension Equations (Uplift)

$$7. 0.6D + W$$

$$8. (0.6 - 0.14S_{DS})D + E \longrightarrow 0.44 D + E$$

$$*8. (0.6 - 0.14S_{DS})D + 2.5 E \longrightarrow 0.44 D + 2.5 E$$

Compression Equations

$$5. D + W$$

$$5. (1 + 0.14S_{DS})D + E \longrightarrow 1.16 D + E$$

$$6. D + 0.75W + 0.75L + 0.75S$$

$$6. (1.0 + 0.105S_{DS})D + 0.75E + 0.75L + 0.75S \longrightarrow 1.12 D + 0.75 E + 0.75 L + 0.75 S$$

$$*5. (1 + 0.14S_{DS})D + 2.5E \longrightarrow 1.16 D + 2.5 E$$

$$*6. (1.0 + 0.105S_{DS})D + 1.875E + 0.75L + 0.75S \longrightarrow 1.12 D + 1.875 E + 0.75 L + 0.75 S$$

* Equations include overstrength factor.

Note: The 0.7 factor for Earthquake loading has already been incorporated into the calculation of the lateral design force E_h , but not E_v . Therefore this factor has been omitted from equations 5, 6 and 8 where appropriate.

UPPER FL. REAR (MASTER SUITE)			SHEARWALL	WIND	SEISMIC
Floor Info					
Upper	Floor Level, e.g. Upper, Main, Lower		Tributary Width (Upper Floor)	Tributary Area (Upper Floor)	
Lt-Rt	Load Direction, e.g. Left-Right, Front-Rear (For Left Wall, Use Front-Rear Load Direction)		9.0 tributary width	9.0 tributary area	
CDX	Sheathing type Values in accordance with AF&PA SDPWS-2015		50.0 total width	50.0 total area	
Roof	Resisting Dead Load (e.g. Roof, Upper Floor, Main Floor)		Tributary Width (Main Floor)	Tributary Area (Main Floor)	
5.50 ft	Total Length of Shearwalls		1.0 tributary width	1.0 tributary area	
$V_{(from\ upper)} = 3784\ lb$		$17281\ lb$	2.0 total width	2.0 total area	
$V_{(from\ main)} = 0\ lb$		$0\ lb$	Tributary Width (Lower Floor)	Tributary Area (Lower Floor)	
$V_{(from\ lower)} = 0\ lb$		$0\ lb$	1.0 tributary width	1.0 tributary area	
$\Sigma(\text{Wind}) = 3,784\ lb$		$\Sigma(Smc) = 17,281\ lb$	2.0 total width	2.0 total area	
$v = 124\ PLF$		$v = 566\ PLF$	Height of Shearwall = 9.0 ft	Weight of Shearwall = 10.0 lbs	
Aspect Ratio OK					
3x framing required per IBC					
SDPWS, Table 4.3A →			0.93 × 707 = 658 PLF	Length of Shearwall = 5.5 ft	USE (2)SW4
Use alternate R factor for seismic? No					

$$\begin{aligned} C_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = \boxed{} + 3563\ lbs &= 3563\ lbs && \text{Seismic controls} \\ T_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = \boxed{} + 4691\ lbs &= 4691\ lbs && \text{Load case 8 controls - Seismic} \end{aligned}$$

Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8: $E = 5090\ lbs$

USE SIMPSON DESIGNED HOLDOWN:
MST60
OR AT FOUNDATION / INTERIOR WALLS USE:
HDU8-SDS2.5

UPPER FL. MID 1 (DECK, ATTIC)			SHEARWALL	WIND	SEISMIC
Floor Info					
Upper	Floor Level, e.g. Upper, Main, Lower		Tributary Width (Upper Floor)	Tributary Area (Upper Floor)	
Lt-Rt	Load Direction, e.g. Left-Right, Front-Rear (For Left Wall, Use Front-Rear Load Direction)		14.5 tributary width	14.5 tributary area	
CDX	Sheathing type Values in accordance with AF&PA SDPWS-2015		50.0 total width	50.0 total area	
Roof	Resisting Dead Load (e.g. Roof, Upper Floor, Main Floor)		Tributary Width (Main Floor)	Tributary Area (Main Floor)	
13.50 ft	Total Length of Shearwalls		1.0 tributary width	1.0 tributary area	
$V_{(from\ upper)} = 3784\ lb$		$17281\ lb$	2.0 total width	2.0 total area	
$V_{(from\ main)} = 0\ lb$		$0\ lb$	Tributary Width (Lower Floor)	Tributary Area (Lower Floor)	
$V_{(from\ lower)} = 0\ lb$		$0\ lb$	1.0 tributary width	1.0 tributary area	
$\Sigma(\text{Wind}) = 3,784\ lb$		$\Sigma(Smc) = 17,281\ lb$	2.0 total width	2.0 total area	
$v = 81\ PLF$		$v = 371\ PLF$	Height of Shearwall = 9.0 ft	Weight of Shearwall = 10.0 lbs	
Aspect Ratio OK					
3x framing required per IBC					
SDPWS, Table 4.3A →			$(2w/h) \times 0.93 \times 595 = 393\ PLF$	Length of Shearwall = 3.2 ft	USE SW2
Use alternate R factor for seismic? No					

$$\begin{aligned} C_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = \boxed{} + 2339\ lbs &= 2339\ lbs && \text{Seismic controls} \\ T_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = \boxed{} + 3220\ lbs &= 3220\ lbs && \text{Load case 8 controls - Seismic} \end{aligned}$$

Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8: $E = 3341\ lbs$

USE SIMPSON DESIGNED HOLDOWN:
MST48
OR AT FOUNDATION / INTERIOR WALLS USE:
STHD14/RJ

UPPER FL. MID 2 (DECK)			SHEARWALL	WIND	SEISMIC
Floor Info					
Upper	Floor Level, e.g. Upper, Main, Lower		Tributary Width (Upper Floor)	Tributary Area (Upper Floor)	
Lt-Rt	Load Direction, e.g. Left-Right, Front-Rear (For Left Wall, Use Front-Rear Load Direction)		14.0 tributary width	14.0 tributary area	
CDX	Sheathing type Values in accordance with AF&PA SDPWS-2015		50.0 total width	50.0 total area	
Roof	Resisting Dead Load (e.g. Roof, Upper Floor, Main Floor)		Tributary Width (Main Floor)	Tributary Area (Main Floor)	
9.00 ft	Total Length of Shearwalls		1.0 tributary width	1.0 tributary area	
$V_{(from\ upper)} = 3784\ lb$		$17281\ lb$	2.0 total width	2.0 total area	
$V_{(from\ main)} = 0\ lb$		$0\ lb$	Tributary Width (Lower Floor)	Tributary Area (Lower Floor)	
$V_{(from\ lower)} = 0\ lb$		$0\ lb$	1.0 tributary width	1.0 tributary area	
$\Sigma(\text{Wind}) = 3,784\ lb$		$\Sigma(Smc) = 17,281\ lb$	2.0 total width	2.0 total area	
$v = 118\ PLF$		$v = 538\ PLF$	Height of Shearwall = 9.0 ft	Weight of Shearwall = 10.0 lbs	
Aspect Ratio OK					
3x framing required per IBC					
SDPWS, Table 4.3A →			$0.93 \times 595 = 553\ PLF$	Length of Shearwall = 9.0 ft	USE SW2
Use alternate R factor for seismic? No					

$$\begin{aligned} C_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = \boxed{} + 3387\ lbs &= 3387\ lbs && \text{Seismic controls} \\ T_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = \boxed{} + 4583\ lbs &= 4583\ lbs && \text{Load case 8 controls - Seismic} \end{aligned}$$

Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8: $E = 4839\ lbs$

USE SIMPSON DESIGNED HOLDOWN:
MST60
OR AT FOUNDATION / INTERIOR WALLS USE:
HDU8-SDS2.5

UPPER FL. FRONT (BDRM 3, ATTIC)		SHEARWALL	WIND	SEISMIC		
Floor Info						
Upper	Floor Level, e.g. Upper, Main, Lower		Tributary Width (Upper Floor)	Tributary Area (Upper Floor)		
Lt-Rt	Load Direction, e.g. Left-Right, Front-Rear (For Left Wall, Use Front-Rear Load Direction)		11.0 tributary width 50.0 total width	11.0 tributary area 50.0 total area		
CDX	Sheathing type Values in accordance with AF&PA SDPWS-2015		Tributary Width (Main Floor)	Tributary Area (Main Floor)		
Roof	Resisting Dead Load (e.g. Roof, Upper Floor, Main Floor)		1.0 tributary width 2.0 total width	1.0 tributary area 2.0 total area		
9.50 ft	Total Length of Shearwalls		Tributary Width (Lower Floor)	Tributary Area (Lower Floor)		
			1.0 tributary width 2.0 total width	1.0 tributary area 2.0 total area		
	$V_{(from\ upper)} = 3784\text{ lb}$	17281 lb	Height of Shearwall = 9.0 ft	Weight of Shearwall = 10.0 lbs		
	$V_{(from\ main)} = 0\text{ lb}$	0 lb	Length of Shearwall = 3.3 ft	Tributary width for dead load = 1.0 ft		
	$V_{(from\ lower)} = 0\text{ lb}$	0 lb	Aspect Ratio OK	Length of adjoining wall = 1.0 ft		
	$\Sigma(\text{Wind}) = 3,784\text{ lb}$	$\Sigma(Smc) = 17,281\text{ lb}$	Use alternate R factor for seismic? No			
	$v = 88\text{ PLF}$	$v = 400\text{ PLF}$				
3x framing required per IBC						
SDPWS, Table 4.3A →		(2w/h) x 0.93 x 595 = 406 PLF	USE SW2			
$C_{\text{TOTAL}} = (\text{floor above}) + (\text{this floor}) =$ <table border="1" style="display: inline-table; vertical-align: middle;"><tr><td></td></tr></table> + 2521 lbs = 2521 lbs Seismic controls $T_{\text{TOTAL}} = (\text{floor above}) + (\text{this floor}) =$ <table border="1" style="display: inline-table; vertical-align: middle;"><tr><td></td></tr></table> + 3478 lbs = 3478 lbs Load case 8 controls - Seismic						
Seismic controls holdown design Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8: E = 3602 lbs						
USE SIMPSON DESIGNED HOLDOWN: MST60 OR AT FOUNDATION / INTERIOR WALLS USE: STHD14/RJ						
UPPER FL. LEFT (BDRM 3, M. BATH)		SHEARWALL	WIND	SEISMIC		
Floor Info						
Upper	Floor Level, e.g. Upper, Main, Lower		Tributary Width (Upper Floor)	Tributary Area (Upper Floor)		
Ft-Rr	Load Direction, e.g. Left-Right, Front-Rear (For Left Wall, Use Front-Rear Load Direction)		6.0 tributary width 45.0 total width	6.0 tributary area 45.0 total area		
CDX	Sheathing type Values in accordance with AF&PA SDPWS-2015		Tributary Width (Main Floor)	Tributary Area (Main Floor)		
Roof	Resisting Dead Load (e.g. Roof, Upper Floor, Main Floor)		1.0 tributary width 2.0 total width	1.0 tributary area 2.0 total area		
23.50 ft	Total Length of Shearwalls		Tributary Width (Lower Floor)	Tributary Area (Lower Floor)		
			1.0 tributary width 2.0 total width	1.0 tributary area 2.0 total area		
	$V_{(from\ upper)} = 3307\text{ lb}$	17281 lb	Height of Shearwall = 9.0 ft	Weight of Shearwall = 10.0 lbs		
	$V_{(from\ main)} = 0\text{ lb}$	0 lb	Length of Shearwall = 3.0 ft	Tributary width for dead load = 1.0 ft		
	$V_{(from\ lower)} = 0\text{ lb}$	0 lb	Aspect Ratio OK	Length of adjoining wall = 1.0 ft		
	$\Sigma(\text{Wind}) = 3,307\text{ lb}$	$\Sigma(Smc) = 17,281\text{ lb}$	Use alternate R factor for seismic? No			
	$v = 19\text{ PLF}$	$v = 98\text{ PLF}$				
SDPWS, Table 4.3A →		(2w/h) x 0.93 x 242 = 150 PLF	USE SW6			
$C_{\text{TOTAL}} = (\text{floor above}) + (\text{this floor}) =$ <table border="1" style="display: inline-table; vertical-align: middle;"><tr><td></td></tr></table> + 618 lbs = 618 lbs Seismic controls $T_{\text{TOTAL}} = (\text{floor above}) + (\text{this floor}) =$ <table border="1" style="display: inline-table; vertical-align: middle;"><tr><td></td></tr></table> + 766 lbs = 766 lbs Load case 8 controls - Seismic						
Seismic controls holdown design Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8: E = 882 lbs						
USE SIMPSON DESIGNED HOLDOWN: CS14 OR AT FOUNDATION / INTERIOR WALLS USE: LSTHD8/RJ						
UPPER FL. MID 2 (ATTIC, M. SUITE)		SHEARWALL	WIND	SEISMIC		
Floor Info						
Upper	Floor Level, e.g. Upper, Main, Lower		Tributary Width (Upper Floor)	Tributary Area (Upper Floor)		
Ft-Rr	Load Direction, e.g. Left-Right, Front-Rear (For Left Wall, Use Front-Rear Load Direction)		17.0 tributary width 45.0 total width	17.0 tributary area 45.0 total area		
CDX	Sheathing type Values in accordance with AF&PA SDPWS-2015		Tributary Width (Main Floor)	Tributary Area (Main Floor)		
Roof	Resisting Dead Load (e.g. Roof, Upper Floor, Main Floor)		1.0 tributary width 2.0 total width	1.0 tributary area 2.0 total area		
23.00 ft	Total Length of Shearwalls		Tributary Width (Lower Floor)	Tributary Area (Lower Floor)		
			1.0 tributary width 2.0 total width	1.0 tributary area 2.0 total area		
	$V_{(from\ upper)} = 3307\text{ lb}$	17281 lb	Height of Shearwall = 9.0 ft	Weight of Shearwall = 10.0 lbs		
	$V_{(from\ main)} = 0\text{ lb}$	0 lb	Length of Shearwall = 8.0 ft	Tributary width for dead load = 1.0 ft		
	$V_{(from\ lower)} = 0\text{ lb}$	0 lb	Aspect Ratio OK	Length of adjoining wall = 1.0 ft		
	$\Sigma(\text{Wind}) = 3,307\text{ lb}$	$\Sigma(Smc) = 17,281\text{ lb}$	Use alternate R factor for seismic? No			
	$v = 54\text{ PLF}$	$v = 284\text{ PLF}$				
SDPWS, Table 4.3A →		0.93 x 353 = 328 PLF	USE SW4			
$C_{\text{TOTAL}} = (\text{floor above}) + (\text{this floor}) =$ <table border="1" style="display: inline-table; vertical-align: middle;"><tr><td></td></tr></table> + 1788 lbs = 1788 lbs Seismic controls $T_{\text{TOTAL}} = (\text{floor above}) + (\text{this floor}) =$ <table border="1" style="display: inline-table; vertical-align: middle;"><tr><td></td></tr></table> + 2322 lbs = 2322 lbs Load case 8 controls - Seismic						
Seismic controls holdown design Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8: E = 2555 lbs						
USE SIMPSON DESIGNED HOLDOWN: CS14 OR AT FOUNDATION / INTERIOR WALLS USE: STHD10/RJ						

UPPER FL. RIGHT (ATTIC)

SHEARWALL

WIND

SEISMIC

Floor Info

Upper Floor Level, e.g. Upper, Main, Lower
Ft-Rr Load Direction, e.g. Left-Right, Front-Rear
(For Left Wall, Use Front-Rear Load Direction)
CDX Sheathing type
Values in accordance with AF&PA SDPWS-2015
Roof Resisting Dead Load
(e.g. Roof, Upper Floor, Main Floor)
8.00 ft Total Length of Shearwalls

$$\begin{aligned} V(\text{from upper}) &= 3307 \text{ lb} & 17281 \text{ lb} \\ V(\text{from main}) &= 0 \text{ lb} & 0 \text{ lb} \\ V(\text{from lower}) &= 0 \text{ lb} & 0 \text{ lb} \\ \Sigma (\text{Wind}) &= 3,307 \text{ lb} & \Sigma (\text{Smc}) = 17,281 \text{ lb} \\ v &= 73 \text{ PLF} & v = 384 \text{ PLF} \end{aligned}$$

3x framing required per IBC

SDPWS, Table 4.3A →

0.93 x 456 = 424 PLF

Height of Shearwall = 9.0 ft

Length of Shearwall = 8.0 ft

Aspect Ratio OK

Use alternate R factor for seismic? No

→ USE SW3

$$\begin{array}{lll} C_{\text{TOTAL}} = & (\text{floor above}) + (\text{this floor}) = & 2419 \text{ lbs} \\ T_{\text{TOTAL}} = & (\text{floor above}) + (\text{this floor}) = & 3224 \text{ lbs} \end{array} \quad = \quad 2419 \text{ lbs} \quad \text{Seismic controls} \\ \quad + \quad 3224 \text{ lbs} \quad = \quad 3224 \text{ lbs} \quad \text{Load case 8 controls - Seismic}$$

Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8:

E = 3456 lbs

UPPER FL. MID 1 (WIC)

SHEARWALL

WIND

SEISMIC

Floor Info

Upper Floor Level, e.g. Upper, Main, Lower
Ft-Rr Load Direction, e.g. Left-Right, Front-Rear
(For Left Wall, Use Front-Rear Load Direction)
CDX Sheathing type
Values in accordance with AF&PA SDPWS-2015
Roof Resisting Dead Load
(e.g. Roof, Upper Floor, Main Floor)
12.00 ft Total Length of Shearwalls

$$\begin{aligned} V(\text{from upper}) &= 3307 \text{ lb} & 17281 \text{ lb} \\ V(\text{from main}) &= 0 \text{ lb} & 0 \text{ lb} \\ V(\text{from lower}) &= 0 \text{ lb} & 0 \text{ lb} \\ \Sigma (\text{Wind}) &= 3,307 \text{ lb} & \Sigma (\text{Smc}) = 17,281 \text{ lb} \\ v &= 92 \text{ PLF} & v = 480 \text{ PLF} \end{aligned}$$

3x framing required per IBC

SDPWS, Table 4.3A →

0.93 x 595 = 553 PLF

Height of Shearwall = 9.0 ft

Length of Shearwall = 12.0 ft

Aspect Ratio OK

Use alternate R factor for seismic? No

$$\begin{array}{lll} \text{Weight of Shearwall} = & 10.0 \text{ lbs} \\ \text{Tributary width for dead load} = & 1.0 \text{ ft} \\ \text{Length of adjoining wall} = & 1.0 \text{ ft} \end{array}$$

Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8:

E = 4320 lbs

MAIN FL. REAR (KITCHEN)

SHEARWALL

WIND

SEISMIC

Floor Info

Main Floor Level, e.g. Upper, Main, Lower
Lt-Rt Load Direction, e.g. Left-Right, Front-Rear
(For Left Wall, Use Front-Rear Load Direction)
CDX Sheathing type
Values in accordance with AF&PA SDPWS-2015
U/FL Resisting Dead Load
(e.g. Roof, Upper Floor, Main Floor)
5.50 ft Total Length of Shearwalls

$$\begin{aligned} V(\text{from upper}) &= 3784 \text{ lb} & 17281 \text{ lb} \\ V(\text{from main}) &= 6623 \text{ lb} & 12564 \text{ lb} \\ V(\text{from lower}) &= 0 \text{ lb} & 0 \text{ lb} \\ \Sigma (\text{Wind}) &= 10,407 \text{ lb} & \Sigma (\text{Smc}) = 29,845 \text{ lb} \\ v &= 329 \text{ PLF} & v = 954 \text{ PLF} \end{aligned}$$

3x framing required per IBC

SDPWS, Table 4.3A →

0.93 x 1190 = 1107 PLF

Height of Shearwall = 9.0 ft

Length of Shearwall = 5.5 ft

Aspect Ratio OK

Use alternate R factor for seismic? No

$$\begin{array}{lll} \text{Weight of Shearwall} = & 10.0 \text{ lbs} \\ \text{Tributary width for dead load} = & 6.0 \text{ ft} \\ \text{Length of adjoining wall} = & 2.0 \text{ ft} \end{array}$$

Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8:

E = 8585 lbs

Seismic controls shearwall design

$$\begin{array}{lll} C_{\text{TOTAL}} = & (\text{floor above}) + (\text{this floor}) = & 3563 \\ T_{\text{TOTAL}} = & (\text{floor above}) + (\text{this floor}) = & 4691 \end{array} \quad = \quad 9573 \text{ lbs} \quad \text{Seismic controls} \\ \quad + \quad 12897 \text{ lbs} \quad = \quad 12897 \text{ lbs} \quad \text{Load case 8 controls - Seismic}$$

Seismic controls holdown design

USE SIMPSON DESIGNED HOLDOWN: HD19 w/DF
OR AT FOUNDATION / INTERIOR WALLS USE: HHDQ14-SDS2.5

MAIN FL. MID 1 (DECK)		SHEARWALL	WIND	SEISMIC
Floor Info				
Main	Floor Level, e.g. Upper, Main, Lower		Tributary Width (Upper Floor)	Tributary Area (Upper Floor)
Lt-Rt	Load Direction, e.g. Left-Right, Front-Rear (For Left Wall, Use Front-Rear Load Direction)		14.5 tributary width 50.0 total width	14.5 tributary area 50.0 total area
CDX	Sheathing type		Tributary Width (Main Floor)	Tributary Area (Main Floor)
U/FL	Values in accordance with AF&PA SDPWS-2015		14.5 tributary width 50.0 total width	14.5 tributary area 50.0 total area
11.50 ft	Resisting Dead Load (e.g. Roof, Upper Floor, Main Floor)		Tributary Width (Lower Floor)	Tributary Area (Lower Floor)
	Total Length of Shearwalls		1.0 tributary width 2.0 total width	1.0 tributary area 2.0 total area
	V(from upper)= 3784 lb V(from main)= 6623 lb V(from lower)= 0 lb	17281 lb 12564 lb 0 lb	Height of Shearwall = 9.0 ft	Weight of Shearwall = 10.0 lbs
	Σ (Wind) = 10,407 lb Σ (Smc) = 29,845 lb	Σ (PLF) = 262 PLF Σ (PLF) = 753 PLF	Length of Shearwall = 11.5 ft	Tributary width for dead load = 1.0 ft
	3x framing required per IBC		Use alternate R factor for seismic? No	Length of adjoining wall = 1.0 ft
SDPWS, Table 4.3A →		0.93 x 911 = 847 PLF	USE (2)SW3	

$$\begin{array}{l} C_{\text{TOTAL}} = (\text{floor above}) + (\text{this floor}) = 2339 \\ T_{\text{TOTAL}} = (\text{floor above}) + (\text{this floor}) = 3220 \end{array} \quad + 4741 \text{ lbs} = 7080 \text{ lbs} \quad \text{Seismic controls}$$

$$+ 6459 \text{ lbs} = 9679 \text{ lbs} \quad \text{Load case 8 controls - Seismic}$$

HDU14

Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8: E = 6774 lbs	USE SIMPSON DESIGNED HOLDOWN: HD19 w/DF
--	---

OR AT FOUNDATION / INTERIOR WALLS USE: HHDQ14-SDS2.5

MAIN FL. MID 2 (DECK)		SHEARWALL	WIND	SEISMIC
Floor Info				
Main	Floor Level, e.g. Upper, Main, Lower		Tributary Width (Upper Floor)	Tributary Area (Upper Floor)
Lt-Rt	Load Direction, e.g. Left-Right, Front-Rear (For Left Wall, Use Front-Rear Load Direction)		14.0 tributary width 50.0 total width	14.0 tributary area 50.0 total area
CDX	Sheathing type		Tributary Width (Main Floor)	Tributary Area (Main Floor)
U/FL	Values in accordance with AF&PA SDPWS-2015		14.0 tributary width 50.0 total width	14.0 tributary area 50.0 total area
9.00 ft	Resisting Dead Load (e.g. Roof, Upper Floor, Main Floor)		Tributary Width (Lower Floor)	Tributary Area (Lower Floor)
	Total Length of Shearwalls		1.0 tributary width 2.0 total width	1.0 tributary area 2.0 total area
	V(from upper)= 3784 lb V(from main)= 6623 lb V(from lower)= 0 lb	17281 lb 12564 lb 0 lb	Height of Shearwall = 9.0 ft	Weight of Shearwall = 10.0 lbs
	Σ (Wind) = 10,407 lb Σ (Smc) = 29,845 lb	Σ (PLF) = 324 PLF Σ (PLF) = 929 PLF	Length of Shearwall = 9.0 ft	Tributary width for dead load = 1.0 ft
	3x framing required per IBC		Use alternate R factor for seismic? No	Length of adjoining wall = 1.0 ft
SDPWS, Table 4.3A →		0.93 x 1190 = 1107 PLF	USE (2)SW2	

$$\begin{array}{l} C_{\text{TOTAL}} = (\text{floor above}) + (\text{this floor}) = 3387 \\ T_{\text{TOTAL}} = (\text{floor above}) + (\text{this floor}) = 4583 \end{array} \quad + 5850 \text{ lbs} = 9237 \text{ lbs} \quad \text{Seismic controls}$$

$$+ 8101 \text{ lbs} = 12684 \text{ lbs} \quad \text{Load case 8 controls - Seismic}$$

HDU14

Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8: E = 8357 lbs	USE SIMPSON DESIGNED HOLDOWN: HD19 w/DF
--	---

OR AT FOUNDATION / INTERIOR WALLS USE: HHDQ14-SDS2.5

MAIN FL. FRONT (FOYER, GREAT RM)		SHEARWALL	WIND	SEISMIC
Floor Info				
Main	Floor Level, e.g. Upper, Main, Lower		Tributary Width (Upper Floor)	Tributary Area (Upper Floor)
Lt-Rt	Load Direction, e.g. Left-Right, Front-Rear (For Left Wall, Use Front-Rear Load Direction)		11.0 tributary width 50.0 total width	11.0 tributary area 50.0 total area
CDX	Sheathing type		Tributary Width (Main Floor)	Tributary Area (Main Floor)
U/FL	Values in accordance with AF&PA SDPWS-2015		11.0 tributary width 50.0 total width	11.0 tributary area 50.0 total area
10.50 ft	Resisting Dead Load (e.g. Roof, Upper Floor, Main Floor)		Tributary Width (Lower Floor)	Tributary Area (Lower Floor)
	Total Length of Shearwalls		1.0 tributary width 2.0 total width	1.0 tributary area 2.0 total area
	V(from upper)= 3784 lb V(from main)= 6623 lb V(from lower)= 0 lb	17281 lb 12564 lb 0 lb	Height of Shearwall = 9.0 ft	Weight of Shearwall = 10.0 lbs
	Σ (Wind) = 10,407 lb Σ (Smc) = 29,845 lb	Σ (PLF) = 218 PLF Σ (PLF) = 625 PLF	Length of Shearwall = 3.0 ft	Tributary width for dead load = 1.0 ft
	3x framing required per IBC		Use alternate R factor for seismic? No	Length of adjoining wall = 1.0 ft
SDPWS, Table 4.3A →		(2w/h) x 0.93 x 1190 = 738 PLF	USE (2)SW2	

$$\begin{array}{l} C_{\text{TOTAL}} = (\text{floor above}) + (\text{this floor}) = 2521 \\ T_{\text{TOTAL}} = (\text{floor above}) + (\text{this floor}) = 3478 \end{array} \quad + 3940 \text{ lbs} = 6461 \text{ lbs} \quad \text{Seismic controls}$$

$$+ 5512 \text{ lbs} = 8990 \text{ lbs} \quad \text{Load case 8 controls - Seismic}$$

Seismic controls holdown design

Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8: E = 5628 lbs	USE SIMPSON DESIGNED HOLDOWN: HDU11-SDS2.5
--	--

MAIN FL. RIGHT (GREAT RM)

SHEARWALL

WIND

SEISMIC

Floor Info

Main Floor Level, e.g. Upper, Main, Lower
 Ft-Rr Load Direction, e.g. Left-Right, Front-Rear
 (For Left Wall, Use Front-Rear Load Direction)
 CDX Sheathing type
 Values in accordance with AF&PA SDPWS-2015
 U/FL Resisting Dead Load
 (e.g. Roof, Upper Floor, Main Floor)
 4.00 ft Total Length of Shearwalls

$$\begin{aligned} V_{\text{from upper}} &= 3307 \text{ lb} & 17281 \text{ lb} \\ V_{\text{from main}} &= 5788 \text{ lb} & 12564 \text{ lb} \\ V_{\text{from lower}} &= 0 \text{ lb} & 0 \text{ lb} \\ \Sigma (\text{Wind}) &= 9,095 \text{ lb} & \Sigma (\text{Smc}) = 29,845 \text{ lb} \\ v &= 404 \text{ PLF} & v = 1326 \text{ PLF} \end{aligned}$$

3x framing required per IBC

SDPWS, Table 4.3A → $(2w/h) \times 0.93 \times 1432 = 444 \text{ PLF}$

Sucka! You'd better bust out your Simpson Catalog!

$$\begin{aligned} C_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = 2419 & + 11142 \text{ lbs} & = 13561 \text{ lbs} & \text{Seismic controls} \\ T_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = 3224 & + 15798 \text{ lbs} & = 19022 \text{ lbs} & \text{Load case 8 controls - Seismic} \end{aligned}$$

Seismic controls shearwall design

Seismic controls holdown design

Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8:

$E = 15917 \text{ lbs}$

USE SIMPSON DESIGNED HOLDOWN:

TOO BIG!!

LOWER FL. REAR (CRAWLSPACE, GARAGE)

SHEARWALL

WIND

SEISMIC

Floor Info

Lower Floor Level, e.g. Upper, Main, Lower
 Lt-Rt Load Direction, e.g. Left-Right, Front-Rear
 (For Left Wall, Use Front-Rear Load Direction)
 CDX Sheathing type
 Values in accordance with AF&PA SDPWS-2015
 M/FL Resisting Dead Load
 (e.g. Roof, Upper Floor, Main Floor)
 31.00 ft Total Length of Shearwalls

$$\begin{aligned} V_{\text{from upper}} &= 3784 \text{ lb} & 17281 \text{ lb} \\ V_{\text{from main}} &= 6623 \text{ lb} & 12564 \text{ lb} \\ V_{\text{from lower}} &= 4925 \text{ lb} & 4742 \text{ lb} \\ \Sigma (\text{Wind}) &= 15,331 \text{ lb} & \Sigma (\text{Smc}) = 34,587 \text{ lb} \\ v &= 85 \text{ PLF} & v = 195 \text{ PLF} \end{aligned}$$

SDPWS, Table 4.3A →

$(2w/h) \times 0.93 \times 353 = 219 \text{ PLF}$

$$\begin{aligned} C_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = & + 1230 \text{ lbs} & = 1230 \text{ lbs} & \text{Seismic controls} \\ T_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = & + 1641 \text{ lbs} & = 1641 \text{ lbs} & \text{Load case 8 controls - Seismic} \end{aligned}$$

Seismic controls shearwall design

Seismic controls holdown design

Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8:

$E = 1757 \text{ lbs}$

USE SIMPSON DESIGNED HOLDOWN:

CS14

LSTHD8/RJ

LOWER FL. MID (GARAGE)

SHEARWALL

WIND

SEISMIC

Floor Info

Lower Floor Level, e.g. Upper, Main, Lower
 Ft-Rr Load Direction, e.g. Left-Right, Front-Rear
 (For Left Wall, Use Front-Rear Load Direction)
 CDX Sheathing type
 Values in accordance with AF&PA SDPWS-2015
 M/FL Resisting Dead Load
 (e.g. Roof, Upper Floor, Main Floor)
 30.00 ft Total Length of Shearwalls

$$\begin{aligned} V_{\text{from upper}} &= 3307 \text{ lb} & 17281 \text{ lb} \\ V_{\text{from main}} &= 5788 \text{ lb} & 12564 \text{ lb} \\ V_{\text{from lower}} &= 4661 \text{ lb} & 4742 \text{ lb} \\ \Sigma (\text{Wind}) &= 13,757 \text{ lb} & \Sigma (\text{Smc}) = 34,587 \text{ lb} \\ v &= 173 \text{ PLF} & v = 436 \text{ PLF} \end{aligned}$$

3x framing required per IBC

SDPWS, Table 4.3A →

$0.93 \times 595 = 553 \text{ PLF}$

$$\begin{aligned} C_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = & + 2744 \text{ lbs} & = 2744 \text{ lbs} & \text{Seismic controls} \\ T_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = & + 3042 \text{ lbs} & = 3042 \text{ lbs} & \text{Load case 8 controls - Seismic} \end{aligned}$$

Seismic controls shearwall design

Seismic controls holdown design

Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8:

$E = 3920 \text{ lbs}$

USE SIMPSON DESIGNED HOLDOWN:

MST48

STHD14/RJ

LOW. FL. MID (GARAGE)

SHEARWALL

WIND

SEISMIC

Floor Info

- Lower** Floor Level, e.g. Upper, Main, Lower
Lt-Rt Load Direction, e.g. Left-Right, Front-Rear
(For Left Wall, Use Front-Rear Load Direction)
CDX Sheathing type
Values in accordance with AF&PA SDPWS-2015
M/FL Resisting Dead Load
(e.g. Roof, Upper Floor, Main Floor)
27.00 ft Total Length of Shearwalls

$$\begin{aligned} V(\text{from upper}) &= 3784 \text{ lb} & 17281 \text{ lb} \\ V(\text{from main}) &= 6623 \text{ lb} & 12564 \text{ lb} \\ V(\text{from lower}) &= 4925 \text{ lb} & 4742 \text{ lb} \\ \Sigma (\text{Wind}) &= 15,331 \text{ lb} & \Sigma (\text{Smc}) = 34,587 \text{ lb} \\ v &= 165 \text{ PLF} & v &= 371 \text{ PLF} \end{aligned}$$

3x framing required per IBC

SDPWS, Table 4.3A →

$$0.93 \times 456 = 424 \text{ PLF} \longrightarrow$$

Tributary Width (Upper Floor)		Tributary Area (Upper Floor)	
14.5	tributary width	14.5	tributary area
50.0	total width	50.0	total area
Tributary Width (Main Floor)		Tributary Area (Main Floor)	
14.5	tributary width	14.5	tributary area
50.0	total width	50.0	total area
Tributary Width (Lower Floor)		Tributary Area (Lower Floor)	
14.5	tributary width	14.5	tributary area
50.0	total width	50.0	total area

Height of Shearwall =	9.0 ft
Length of Shearwall =	16.0 ft

Aspect Ratio OK

Weight of Shearwall =	10.0 lbs
Tributary width for dead load =	1.0 ft
Length of adjoining wall =	1.0 ft

Use alternate R factor for seismic? No

$$\begin{aligned} C_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = \\ T_{\text{TOTAL}} &= (\text{floor above}) + (\text{this floor}) = \end{aligned} \quad \begin{aligned} &+ 2340 \text{ lbs} &= 2340 \text{ lbs} & \text{Seismic controls} \\ &+ 2925 \text{ lbs} &= 2925 \text{ lbs} & \text{Load case 8 controls - Seismic} \end{aligned}$$

Where overstrength factor is applicable, use this value for E in equations 5, 6, and 8:
E = 3343 lbs

USE SIMPSON DESIGNED HOLDOWN:

OR AT FOUNDATION / INTERIOR WALLS USE:

MST48

STHD14/RJ

Seismic controls holdown design

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: ROOF JOIST

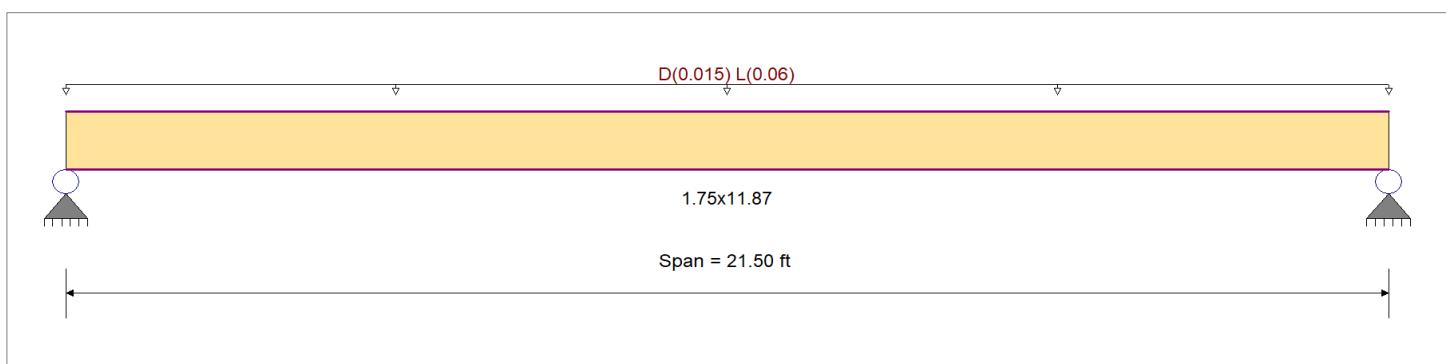
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,600.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	2,600.0 psi	Ebend - xx 1,900.0 ksi
		Fc - Prll	2,510.0 psi	Eminbend - xx 965.71 ksi
Wood Species	iLevel Truss Joist	Fc - Perp	750.0 psi	
Wood Grade	MicroLam LVL 1.9 E	Fv	285.0 psi	
Beam Bracing	Beam is Fully Braced against lateral-torsional buckling	Ft	1,555.0 psi	Density 42.010pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 1.0 ft, (ROOF DECK)

DESIGN SUMMARY

		Design OK	
Maximum Bending Stress Ratio	= 0.525 : 1	Maximum Shear Stress Ratio	= 0.201 : 1
Section used for this span	1.75x11.87	Section used for this span	1.75x11.87
fb: Actual	= 1,366.58psi	fv: Actual	= 57.39 psi
F'b	= 2,603.71psi	F'v	= 285.00 psi
Load Combination	+D+L	Load Combination	+D+L
Location of maximum on span	= 10.750ft	Location of maximum on span	= 20.558 ft
Span # where maximum occurs	= Span # 1	Span # where maximum occurs	= Span # 1
Maximum Deflection			
Max Downward Transient Deflection	0.625 in	Ratio = 412 >= 360	Span: 1 : L Only
Max Upward Transient Deflection	0 in	Ratio = 0 < 360	n/a
Max Downward Total Deflection	0.845 in	Ratio = 305 >= 240	Span: 1 : +D+L
Max Upward Total Deflection	0 in	Ratio = 0 < 240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios						Moment Values				Shear Values						
		Span #	M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	M	fb	F'b	V	fv	F'v	
D Only															0.0	0.00	0.0	0.0
Length = 21.50 ft	1	0.152	0.058	0.90	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	1.22	355.1	2,343.3	0.21	14.9	256.5
+D+L															0.0	0.00	0.0	0.0
Length = 21.50 ft	1	0.525	0.201	1.00	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	4.68	1,366.6	2,603.7	0.80	57.4	285.0
+D+0.750L															0.0	0.00	0.0	0.0
Length = 21.50 ft	1	0.342	0.131	1.25	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	3.82	1,113.7	3,254.6	0.65	46.8	356.3
+0.60D															0.0	0.00	0.0	0.0
Length = 21.50 ft	1	0.051	0.020	1.60	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	0.73	213.0	4,165.9	0.12	8.9	456.0

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: ROOF JOIST

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.8448	10.828		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.2195 in	10.828 ft	0.0000 in	0.000 ft
+D+L	1	0.8448 in	10.828 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.6885 in	10.828 ft	0.0000 in	0.000 ft
+0.60D	1	0.1317 in	10.828 ft	0.0000 in	0.000 ft
L Only	1	0.6253 in	10.828 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	0.871	0.871
Max Upward from Load Combinations	0.871	0.871
Max Upward from Load Cases	0.645	0.645
D Only	0.226	0.226
+D+L	0.871	0.871
+D+0.750L	0.710	0.710
+0.60D	0.136	0.136
L Only	0.645	0.645

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: ROOF JOIST 2

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.3825	8.310		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0940 in	8.310 ft	0.0000 in	0.000 ft
+D+L	1	0.3825 in	8.310 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.3104 in	8.310 ft	0.0000 in	0.000 ft
+0.60D	1	0.0564 in	8.310 ft	0.0000 in	0.000 ft
L Only	1	0.2885 in	8.310 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	0.873	0.873
Max Upward from Load Combinations	0.873	0.873
Max Upward from Load Cases	0.658	0.658
D Only	0.215	0.215
+D+L	0.873	0.873
+D+0.750L	0.708	0.708
+0.60D	0.129	0.129
L Only	0.658	0.658

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: UPPER FL. DECK JOIST 1

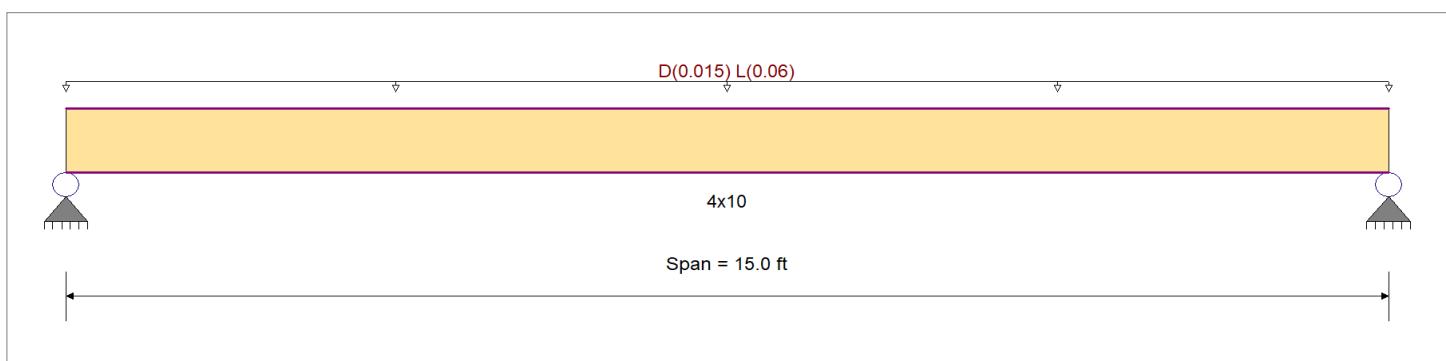
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	675.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	675.0 psi	Ebend - xx 1,100.0ksi
		Fc - Prll	475.0 psi	Eminbend - xx 400.0ksi
Wood Species	: Hem-Fir (North)	Fc - Perp	405.0 psi	
Wood Grade	: No.2	Fv	135.0 psi	
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	325.0 psi	Density 28.720pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 1.0 ft, (DECK)

DESIGN SUMMARY

Design OK			
Maximum Bending Stress Ratio	=	0.850 : 1	Maximum Shear Stress Ratio
Section used for this span		4x10	Section used for this span
fb: Actual	=	550.81psi	fv: Actual
F'b	=	648.00psi	F'v
Load Combination		+D+L	Load Combination
Location of maximum on span	=	7.500ft	Location of maximum on span
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs
Maximum Deflection			
Max Downward Transient Deflection	0.285 in	Ratio = 631 >= 360	Span: 1 : L Only
Max Upward Transient Deflection	0 in	Ratio = 0 < 360	n/a
Max Downward Total Deflection	0.387 in	Ratio = 465 >= 240	Span: 1 : +D+L
Max Upward Total Deflection	0 in	Ratio = 0 < 240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios								Moment Values				Shear Values				
		Span #	M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	fv	F'v
D Only														0.0	0.00	0.0	0.0	
Length = 15.0 ft	1	0.249	0.069	0.90	1.00	1.00	1.00	1.200	1.00	0.80	1.00	1.00	0.60	145.1	583.2	0.14	6.7	97.2
+D+L														0.0	0.00	0.0	0.0	
Length = 15.0 ft	1	0.850	0.235	1.00	1.00	1.00	1.00	1.200	1.00	0.80	1.00	1.00	2.29	550.8	648.0	0.55	25.4	108.0
+D+0.750L														0.0	0.00	0.0	0.0	
Length = 15.0 ft	1	0.555	0.154	1.25	1.00	1.00	1.00	1.200	1.00	0.80	1.00	1.00	1.87	449.4	810.0	0.45	20.7	135.0
+0.60D														0.0	0.00	0.0	0.0	
Length = 15.0 ft	1	0.084	0.023	1.60	1.00	1.00	1.00	1.200	1.00	0.80	1.00	1.00	0.36	87.1	1,036.8	0.09	4.0	172.8

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: UPPER FL. DECK JOIST 1

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.3869	7.555		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.1019 in	7.555 ft	0.0000 in	0.000 ft
+D+L	1	0.3869 in	7.555 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.3156 in	7.555 ft	0.0000 in	0.000 ft
+0.60D	1	0.0611 in	7.555 ft	0.0000 in	0.000 ft
L Only	1	0.2850 in	7.555 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	0.611	0.611
Max Upward from Load Combinations	0.611	0.611
Max Upward from Load Cases	0.450	0.450
D Only	0.161	0.161
+D+L	0.611	0.611
+D+0.750L	0.498	0.498
+0.60D	0.097	0.097
L Only	0.450	0.450

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: UPPER FL. DECK JOIST 2

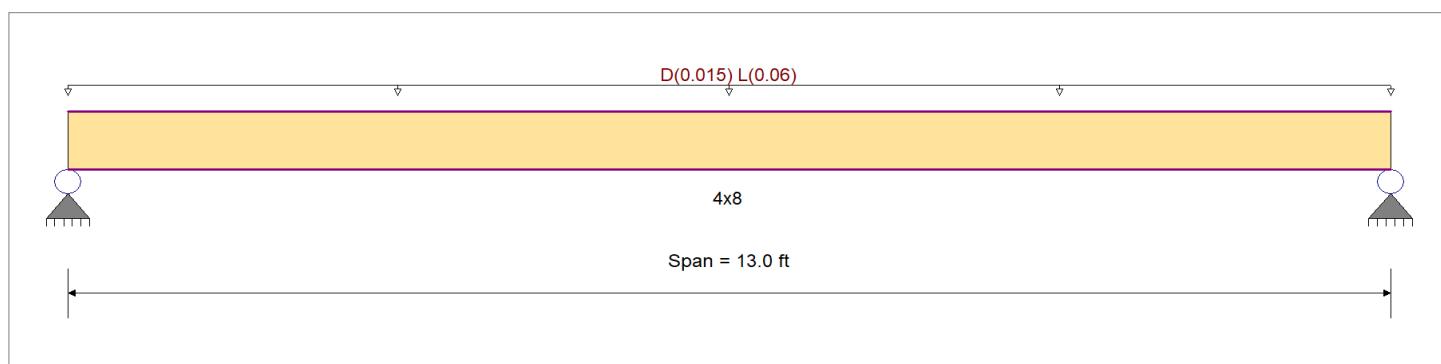
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	675.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	675.0 psi	Ebend - xx 1,100.0ksi
		Fc - Prll	475.0 psi	Eminbend - xx 400.0ksi
Wood Species	: Hem-Fir (North)	Fc - Perp	405.0 psi	
Wood Grade	: No.2	Fv	135.0 psi	
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	325.0 psi	Density 28.720pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 1.0 ft, (DECK JOIST)

DESIGN SUMMARY

Design OK			
Maximum Bending Stress Ratio	=	0.943 1	Maximum Shear Stress Ratio
Section used for this span		4x8	Section used for this span
fb: Actual	=	661.92psi	fv: Actual
F'b	=	702.00psi	F'v
Load Combination		+D+L	Load Combination
Location of maximum on span	=	6.500ft	Location of maximum on span
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs
Maximum Deflection			
Max Downward Transient Deflection	0.334 in	Ratio = 467 >=360	Span: 1 : L Only
Max Upward Transient Deflection	0 in	Ratio = 0 <360	n/a
Max Downward Total Deflection	0.446 in	Ratio = 350 >=240	Span: 1 : +D+L
Max Upward Total Deflection	0 in	Ratio = 0 <240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios								Moment Values				Shear Values				
		Span #	M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	fv	F'v
D Only														0.0	0.00	0.0	0.0	
Length = 13.0 ft	1	0.263	0.072	0.90	1.00	1.00	1.00	1.300	1.00	0.80	1.00	1.00	0.42	165.9	631.8	0.12	7.0	97.2
+D+L														0.0	0.00	0.0	0.0	
Length = 13.0 ft	1	0.943	0.260	1.00	1.00	1.00	1.00	1.300	1.00	0.80	1.00	1.00	1.69	661.9	702.0	0.47	28.1	108.0
+D+0.750L														0.0	0.00	0.0	0.0	
Length = 13.0 ft	1	0.613	0.169	1.25	1.00	1.00	1.00	1.300	1.00	0.80	1.00	1.00	1.37	537.9	877.5	0.39	22.8	135.0
+0.60D														0.0	0.00	0.0	0.0	
Length = 13.0 ft	1	0.089	0.024	1.60	1.00	1.00	1.00	1.300	1.00	0.80	1.00	1.00	0.25	99.5	1,123.2	0.07	4.2	172.8

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: UPPER FL. DECK JOIST 2

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.4455	6.547		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.1116 in	6.547 ft	0.0000 in	0.000 ft
+D+L	1	0.4455 in	6.547 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.3621 in	6.547 ft	0.0000 in	0.000 ft
+0.60D	1	0.0670 in	6.547 ft	0.0000 in	0.000 ft
L Only	1	0.3339 in	6.547 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	0.520	0.520
Max Upward from Load Combinations	0.520	0.520
Max Upward from Load Cases	0.390	0.390
D Only	0.130	0.130
+D+L	0.520	0.520
+D+0.750L	0.423	0.423
+0.60D	0.078	0.078
L Only	0.390	0.390

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: MAIN FL. DECK JOIST 1

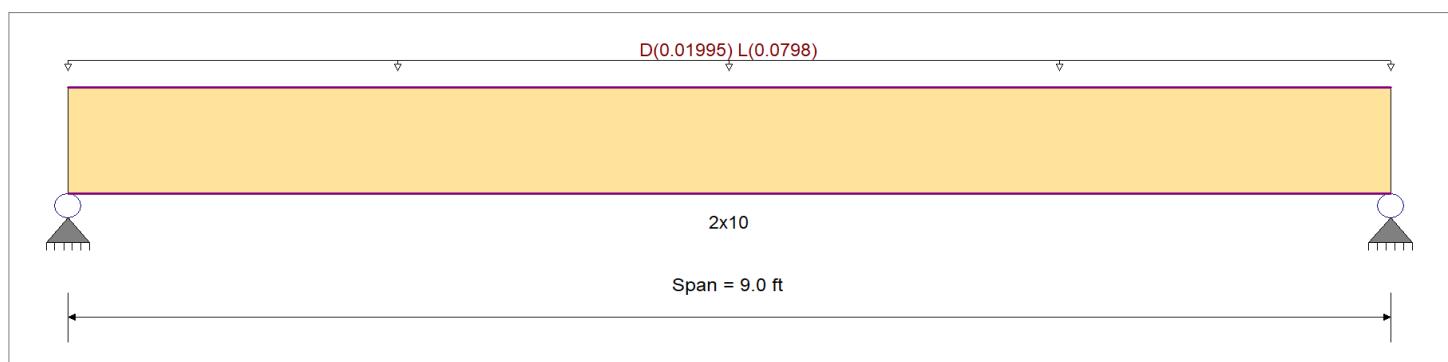
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	675.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	675.0 psi	Ebend- xx 1,100.0ksi
		Fc - Prll	475.0 psi	Eminbend - xx 400.0ksi
Wood Species	: Hem-Fir (North)	Fc - Perp	405.0 psi	
Wood Grade	: No.2	Fv	135.0 psi	
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	325.0 psi	Density 28.720pcf
				Repetitive Member Stress Increase



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
 Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 1.330 ft, (DECK JOIST)

DESIGN SUMMARY

Design OK				
Maximum Bending Stress Ratio	=	0.852 1	Maximum Shear Stress Ratio	= 0.384 : 1
Section used for this span		2x10	Section used for this span	2x10
fb: Actual	=	582.30psi	fv: Actual	= 41.50 psi
F'b	=	683.10psi	F'v	= 108.00 psi
Load Combination		+D+L	Load Combination	+D+L
Location of maximum on span	=	4.500ft	Location of maximum on span	= 8.245 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	= Span # 1
Maximum Deflection				
Max Downward Transient Deflection	0.115 in	Ratio = 942 >= 360	Span: 1 : L Only	
Max Upward Transient Deflection	0 in	Ratio = 0 < 360	n/a	
Max Downward Total Deflection	0.147 in	Ratio = 733 >= 240	Span: 1 : +D+L	
Max Upward Total Deflection	0 in	Ratio = 0 < 240	n/a	

Maximum Forces & Stresses for Load Combinations

Load Combination	Max Stress Ratios										Moment Values				Shear Values			
	Segment Length	Span #	M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only															0.0	0.00	0.0	0.0
Length = 9.0 ft	1	0.210	0.095	0.90	1.00	1.00	1.00	1.100	1.00	0.80	1.15		0.23	129.0	614.8	0.09	9.2	97.2
+D+L															0.0	0.00	0.0	0.0
Length = 9.0 ft	1	0.852	0.384	1.00	1.00	1.00	1.00	1.100	1.00	0.80	1.15		1.04	582.3	683.1	0.38	41.5	108.0
+D+0.750L															0.0	0.00	0.0	0.0
Length = 9.0 ft	1	0.549	0.248	1.25	1.00	1.00	1.00	1.100	1.00	0.80	1.15		0.84	469.0	853.9	0.31	33.4	135.0
+0.60D															0.0	0.00	0.0	0.0
Length = 9.0 ft	1	0.071	0.032	1.60	1.00	1.00	1.00	1.100	1.00	0.80	1.15		0.14	77.4	1,093.0	0.05	5.5	172.8

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: MAIN FL. DECK JOIST 1

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.1472	4.533		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0326 in	4.533 ft	0.0000 in	0.000 ft
+D+L	1	0.1472 in	4.533 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.1186 in	4.533 ft	0.0000 in	0.000 ft
+0.60D	1	0.0196 in	4.533 ft	0.0000 in	0.000 ft
L Only	1	0.1146 in	4.533 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	0.461	0.461
Max Upward from Load Combinations	0.461	0.461
Max Upward from Load Cases	0.359	0.359
D Only	0.102	0.102
+D+L	0.461	0.461
+D+0.750L	0.372	0.372
+0.60D	0.061	0.061
L Only	0.359	0.359

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#1

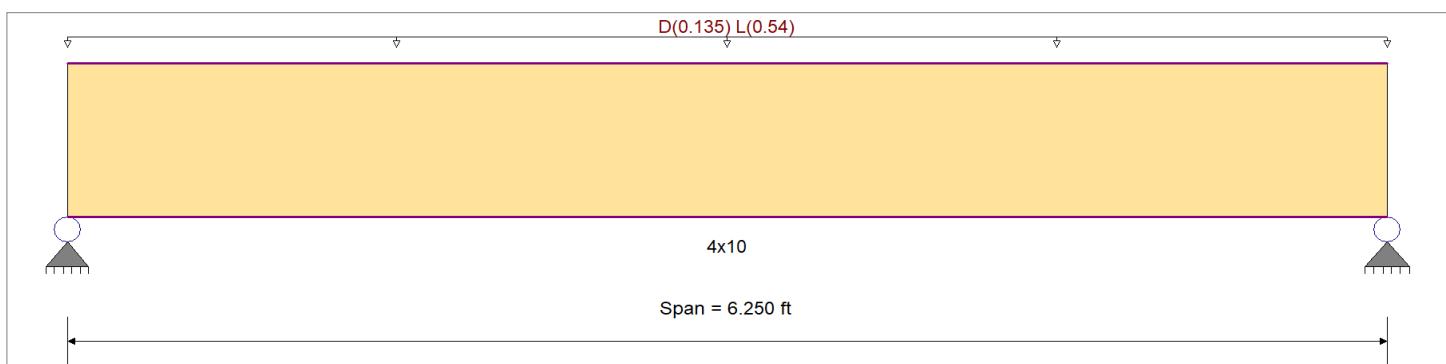
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	875.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	875.0 psi	Ebend - xx 1,300.0ksi
		Fc - Prll	600.0 psi	Eminbend - xx 470.0ksi
Wood Species	: Douglas Fir-Larch (North)	Fc - Perp	625.0 psi	
Wood Grade	: No.2	Fv	170.0 psi	
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	425.0 psi	Density 30.590pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 9.0 ft, (ROOF)

DESIGN SUMMARY

Design OK					
Maximum Bending Stress Ratio	=	0.762 1	Maximum Shear Stress Ratio	=	0.441 1
Section used for this span		4x10	Section used for this span		4x10
fb: Actual	=	800.49psi	fv: Actual	=	74.95 psi
F'b	=	1,050.00psi	F'v	=	170.00 psi
Load Combination		+D+L	Load Combination		+D+L
Location of maximum on span	=	3.125ft	Location of maximum on span	=	5.497 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
Maximum Deflection					
Max Downward Transient Deflection	0.062 in	Ratio = 1206 >=360	Span: 1 : L Only		
Max Upward Transient Deflection	0 in	Ratio = 0 <360	n/a		
Max Downward Total Deflection	0.078 in	Ratio = 955 >=240	Span: 1 : +D+L		
Max Upward Total Deflection	0 in	Ratio = 0 <240	n/a		

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios						Moment Values						Shear Values				
		Span #	M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only														0.0	0.00	0.0	0.0	
Length = 6.250 ft	1	0.176	0.102	0.90	1.00	1.00	1.00	1.200	1.00	1.00	1.00	1.00	0.69	166.6	945.0	0.34	15.6	153.0
+D+L									1.00	1.00	1.00	1.200	1.00	1.00	1.00	0.0	0.00	0.0
Length = 6.250 ft	1	0.762	0.441	1.00	1.00	1.00	1.00	1.200	1.00	1.00	1.00	1.00	3.33	800.5	1,050.0	1.62	74.9	170.0
+D+0.750L									1.00	1.00	1.00	1.200	1.00	1.00	1.00	0.0	0.00	0.0
Length = 6.250 ft	1	0.489	0.283	1.25	1.00	1.00	1.00	1.200	1.00	1.00	1.00	1.00	2.67	642.0	1,312.5	1.30	60.1	212.5
+0.60D									1.00	1.00	1.00	1.200	1.00	1.00	1.00	0.0	0.00	0.0
Length = 6.250 ft	1	0.059	0.034	1.60	1.00	1.00	1.00	1.200	1.00	1.00	1.00	1.00	0.42	99.9	1,680.0	0.20	9.4	272.0

Project Title:
Engineer:
Project ID:
Project Descr:

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#1

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.0785	3.148		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0163 in	3.148 ft	0.0000 in	0.000 ft
+D+L	1	0.0785 in	3.148 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.0629 in	3.148 ft	0.0000 in	0.000 ft
+0.60D	1	0.0098 in	3.148 ft	0.0000 in	0.000 ft
L Only	1	0.0621 in	3.148 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	2.131	2.131
Max Upward from Load Combinations	2.131	2.131
Max Upward from Load Cases	1.688	1.688
D Only	0.443	0.443
+D+L	2.131	2.131
+D+0.750L	1.709	1.709
+0.60D	0.266	0.266
L Only	1.688	1.688

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#2

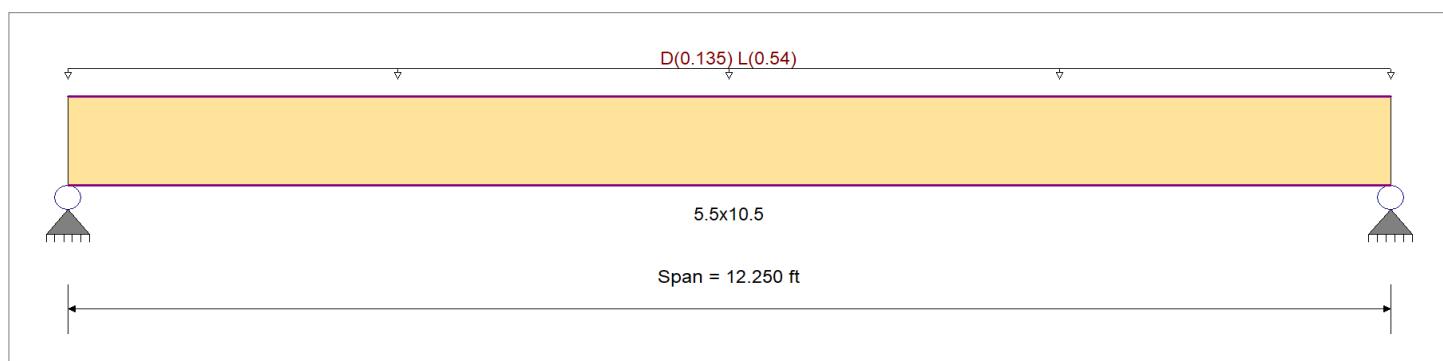
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	1,850.0 psi	Ebend- xx 1,800.0ksi
		Fc - Prll	1,650.0 psi	Eminbend - xx 950.0ksi
Wood Species	: DF/DF	Fc - Perp	650.0 psi	Ebend- yy 1,600.0ksi
Wood Grade	: 24F-V4	Fv	265.0 psi	Eminbend - yy 850.0ksi
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	1,100.0 psi	Density 31.210pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 9.0 ft, (ROOF)

DESIGN SUMMARY

				Design OK	
Maximum Bending Stress Ratio	=	0.638 : 1	Maximum Shear Stress Ratio	=	0.356 : 1
Section used for this span		5.5x10.5	Section used for this span		5.5x10.5
fb: Actual	=	1,531.29psi	fv: Actual	=	94.21 psi
F'b	=	2,400.00psi	F'v	=	265.00 psi
Load Combination		+D+L	Load Combination		+D+L
Location of maximum on span	=	6.125ft	Location of maximum on span	=	11.401 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
Maximum Deflection					
Max Downward Transient Deflection	0.288 in	Ratio = 510 >= 360	Span: 1 : L Only		
Max Upward Transient Deflection	0 in	Ratio = 0 < 360	n/a		
Max Downward Total Deflection	0.367 in	Ratio = 400 >= 240	Span: 1 : +D+L		
Max Upward Total Deflection	0 in	Ratio = 0 < 240	n/a		

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios						Moment Values				Shear Values						
		Span #	M	V	CD	CM	C _t	CLx	C _y	C _f	C _i	C _r	M	fb	F'b	V	fv	F'v
D Only															0.0	0.00	0.0	0.0
Length = 12.250 ft	1	0.152	0.085	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	2.77	328.6	2,160.0	0.78	20.2	238.5
+D+L															0.0	0.00	0.0	0.0
Length = 12.250 ft	1	0.638	0.356	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	12.90	1,531.3	2,400.0	3.63	94.2	265.0
+D+0.750L															0.0	0.00	0.0	0.0
Length = 12.250 ft	1	0.410	0.229	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	10.36	1,230.6	3,000.0	2.91	75.7	331.3
+0.60D															0.0	0.00	0.0	0.0
Length = 12.250 ft	1	0.051	0.029	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	1.66	197.1	3,840.0	0.47	12.1	424.0

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#2

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.3669	6.170		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0787 in	6.170 ft	0.0000 in	0.000 ft
+D+L	1	0.3669 in	6.170 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.2948 in	6.170 ft	0.0000 in	0.000 ft
+0.60D	1	0.0472 in	6.170 ft	0.0000 in	0.000 ft
L Only	1	0.2882 in	6.170 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	4.211	4.211
Max Upward from Load Combinations	4.211	4.211
Max Upward from Load Cases	3.308	3.308
D Only	0.904	0.904
+D+L	4.211	4.211
+D+0.750L	3.384	3.384
+0.60D	0.542	0.542
L Only	3.308	3.308

Project Title:
Engineer:
Project ID:
Project Descr:

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#3

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.2633	6.170		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0599 in	6.170 ft	0.0000 in	0.000 ft
+D+L	1	0.2633 in	6.170 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.2125 in	6.170 ft	0.0000 in	0.000 ft
+0.60D	1	0.0360 in	6.170 ft	0.0000 in	0.000 ft
L Only	1	0.2034 in	6.170 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	1.903	1.903
Max Upward from Load Combinations	1.903	1.903
Max Upward from Load Cases	1.470	1.470
D Only	0.433	0.433
+D+L	1.903	1.903
+D+0.750L	1.536	1.536
+0.60D	0.260	0.260
L Only	1.470	1.470

Project Title:
Engineer:
Project ID:
Project Descr:

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#4

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.1025	3.651		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0214 in	3.651 ft	0.0000 in	0.000 ft
+D+L	1	0.1025 in	3.651 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.0822 in	3.651 ft	0.0000 in	0.000 ft
+0.60D	1	0.0128 in	3.651 ft	0.0000 in	0.000 ft
L Only	1	0.0811 in	3.651 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	3.573	3.573
Max Upward from Load Combinations	3.573	3.573
Max Upward from Load Cases	2.828	2.828
D Only	0.746	0.746
+D+L	3.573	3.573
+D+0.750L	2.866	2.866
+0.60D	0.447	0.447
L Only	2.828	2.828

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#5

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.0730	3.148		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0156 in	3.148 ft	0.0000 in	0.000 ft
+D+L	1	0.0730 in	3.148 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.0586 in	3.148 ft	0.0000 in	0.000 ft
+0.60D	1	0.0094 in	3.148 ft	0.0000 in	0.000 ft
L Only	1	0.0574 in	3.148 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	0.954	0.954
Max Upward from Load Combinations	0.954	0.954
Max Upward from Load Cases	0.750	0.750
D Only	0.204	0.204
+D+L	0.954	0.954
+D+0.750L	0.767	0.767
+0.60D	0.123	0.123
L Only	0.750	0.750

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#6

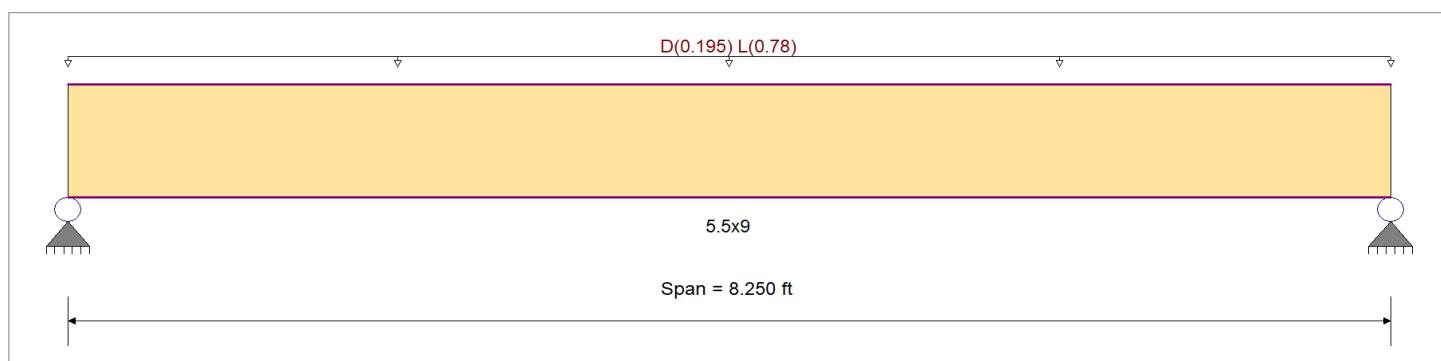
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	1,850.0 psi	Ebend- xx 1,800.0ksi
		Fc - Prll	1,650.0 psi	Eminbend - xx 950.0ksi
Wood Species	: DF/DF	Fc - Perp	650.0 psi	Ebend- yy 1,600.0ksi
Wood Grade	: 24F-V4	Fv	265.0 psi	Eminbend - yy 850.0ksi
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	1,100.0 psi	Density 31.210pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 13.0 ft, (ROOF)

DESIGN SUMMARY

Design OK			
Maximum Bending Stress Ratio	=	0.565 1	Maximum Shear Stress Ratio
Section used for this span		5.5x9	Section used for this span
fb: Actual	=	1,355.38psi	fv: Actual
F'b	=	2,400.00psi	F'v
Load Combination		+D+L	Load Combination
Location of maximum on span	=	4.125ft	Location of maximum on span
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs
Maximum Deflection			
Max Downward Transient Deflection	0.136 in	Ratio = 728 >= 360	Span: 1 : L Only
Max Upward Transient Deflection	0 in	Ratio = 0 < 360	n/a
Max Downward Total Deflection	0.172 in	Ratio = 576 >= 240	Span: 1 : +D+L
Max Upward Total Deflection	0 in	Ratio = 0 < 240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios								Moment Values				Shear Values				
		Span #	M	V	CD	CM	C _t	CLx	C _y	C _f	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only															0.0	0.00	0.0	0.0
Length = 8.250 ft	1	0.131	0.089	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	1.75	282.9	2,160.0	0.70	21.2	238.5
+D+L															0.0	0.00	0.0	0.0
Length = 8.250 ft	1	0.565	0.384	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	8.39	1,355.4	2,400.0	3.35	101.6	265.0
+D+0.750L															0.0	0.00	0.0	0.0
Length = 8.250 ft	1	0.362	0.246	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	6.73	1,087.3	3,000.0	2.69	81.5	331.3
+0.60D															0.0	0.00	0.0	0.0
Length = 8.250 ft	1	0.044	0.030	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	1.05	169.7	3,840.0	0.42	12.7	424.0

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#6

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.1718	4.155		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0359 in	4.155 ft	0.0000 in	0.000 ft
+D+L	1	0.1718 in	4.155 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.1378 in	4.155 ft	0.0000 in	0.000 ft
+0.60D	1	0.0215 in	4.155 ft	0.0000 in	0.000 ft
L Only	1	0.1360 in	4.155 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	4.066	4.066
Max Upward from Load Combinations	4.066	4.066
Max Upward from Load Cases	3.218	3.218
D Only	0.849	0.849
+D+L	4.066	4.066
+D+0.750L	3.262	3.262
+0.60D	0.509	0.509
L Only	3.218	3.218

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#9

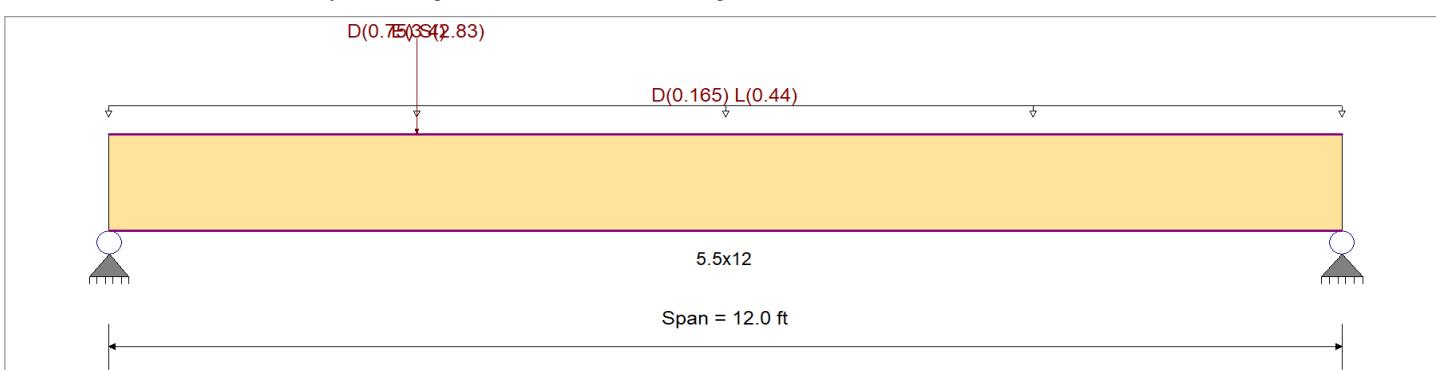
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	1,850.0 psi	Ebend- xx 1,800.0 ksi
Wood Species	DF/DF	Fc - Prll	1,650.0 psi	Eminbend - xx 950.0 ksi
Wood Grade	24F-V4	Fc - Perp	650.0 psi	Ebend- yy 1,600.0 ksi
Beam Bracing	Beam is Fully Braced against lateral-torsional buckling	Fv	265.0 psi	Eminbend - yy 850.0 ksi
		Ft	1,100.0 psi	Density 31.210 pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.0150, L = 0.040 ksf, Tributary Width = 11.0 ft, (FLOOR)

Point Load : E = 3.40 k @ 3.0 ft, (SW2)

Point Load : D = 0.750, S = 2.830 k @ 3.0 ft, (HDR#4)

DESIGN SUMMARY

Maximum Bending Stress Ratio	=	0.944 : 1	Maximum Shear Stress Ratio	=	0.729 : 1
Section used for this span	=	5.5x12	Section used for this span	=	5.5x12
fb: Actual	=	3,625.68 psi	fv: Actual	=	308.95 psi
F'b	=	3,840.00 psi	F'v	=	424.00 psi
Load Combination	=	+1.118D+0.750L+0.750S+3.413E	Load Combination	=	+1.118D+0.750L+0.750S+3.413E
Location of maximum on span	=	3.022 ft	Location of maximum on span	=	0.000 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
Maximum Deflection					
Max Downward Transient Deflection		0.145 in	Ratio =	994 >= 360	Span: 1 : L Only
Max Upward Transient Deflection		0 in	Ratio =	0 < 360	n/a
Max Downward Total Deflection		0.309 in	Ratio =	465 >= 240	Span: 1 : +D+0.750L+0.750S+0.5250E
Max Upward Total Deflection		0 in	Ratio =	0 < 240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios						Moment Values				Shear Values					
			M	V	CD	CM	C _t	CLx	C _y	C _f u	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only															0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.187	0.140	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	4.45	404.6	2,160.0	1.47	33.3	238.5
+D+L															0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.466	0.316	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	12.30	1,118.3	2,400.0	3.68	83.7	265.0
+D+S															0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.345	0.268	1.15	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	10.47	951.6	2,760.0	3.59	81.5	304.8
+D+0.750L															0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.313	0.215	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	10.33	938.8	3,000.0	3.13	71.1	331.3
+D+0.750L+0.750S															0.0	0.00	0.0	0.0

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#9

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios									Moment Values			Shear Values		
			M	V	CD	CM	C _t	CLx	C _V	C _{fu}	C _i	M	f _b	F' _b	V	f _v	F' _v
Length = 12.0 ft	1	0.461	0.352	1.15	1.00	1.00	1.00	1.000	1.00	1.00	1.00	13.98	1,271.1	2,760.0	4.72	107.3	304.8
+1.157D+4.550E					1.00	1.00	1.00	1.000	1.00	1.00	1.00			0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.935	0.713	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	39.48	3,589.4	3,840.0	13.30	302.2	424.0
+1.118D+0.750L+0.750S+3.4					1.00	1.00	1.00	1.000	1.00	1.00	1.00			0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.944	0.729	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	39.88	3,625.7	3,840.0	13.59	308.9	424.0
+0.60D					1.00	1.00	1.00	1.000	1.00	1.00	1.00			0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.063	0.047	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	2.67	242.8	3,840.0	0.88	20.0	424.0
+0.4432D+4.550E					1.00	1.00	1.00	1.000	1.00	1.00	1.00			0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.865	0.657	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	36.55	3,322.4	3,840.0	12.25	278.5	424.0

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+0.750L+0.750S+0.5250E	1	0.3094	5.693		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0818	in	5.825 ft	0.0000 in
+D+L	1	0.2266	in	5.956 ft	0.0000 in
+D+S	1	0.1683	in	5.562 ft	0.0000 in
+D+0.750L	1	0.1904	in	5.956 ft	0.0000 in
+D+0.750L+0.750S	1	0.2549	in	5.781 ft	0.0000 in
+D+0.70E	1	0.1545	in	5.606 ft	0.0000 in
+D+0.750L+0.750S+0.5250E	1	0.3094	in	5.693 ft	0.0000 in
+0.60D	1	0.0491	in	5.825 ft	0.0000 in
+0.60D+0.70E	1	0.1219	in	5.518 ft	0.0000 in
L Only	1	0.1448	in	6.044 ft	0.0000 in
S Only	1	0.0869	in	5.299 ft	0.0000 in
E Only	1	0.1044	in	5.299 ft	0.0000 in

Vertical Reactions

Load Combination	Support 1	Support 2	Support notation : Far left is #1	Values in KIPS
Max Upward from all Load Conditions	6.549	4.220		
Max Upward from Load Combinations	6.549	4.220		
Max Upward from Load Cases	2.640	2.640		
D Only	1.638	1.263		
+D+L	4.278	3.903		
+D+S	3.761	1.971		
+D+0.750L	3.618	3.243		
+D+0.750L+0.750S	5.210	3.774		
+D+0.70E	3.423	1.858		
+D+0.750L+0.750S+0.5250E	6.549	4.220		
+0.60D	0.983	0.758		
+0.60D+0.70E	2.768	1.353		
L Only	2.640	2.640		
S Only	2.123	0.708		
E Only	2.550	0.850		

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#10

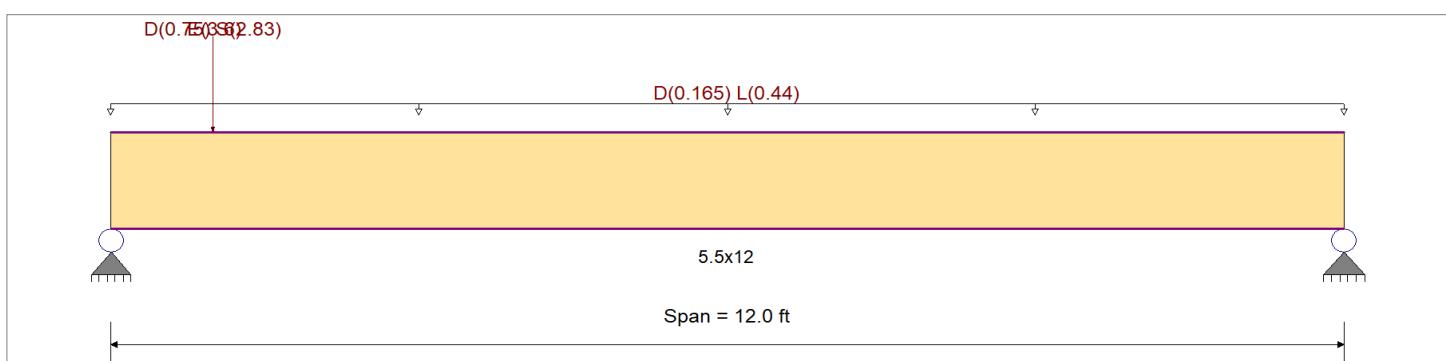
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	1,850.0 psi	Ebend- xx 1,800.0 ksi
		Fc - Prll	1,650.0 psi	Eminbend - xx 950.0 ksi
Wood Species	: DF/DF	Fc - Perp	650.0 psi	Ebend- yy 1,600.0 ksi
Wood Grade	: 24F-V4	Fv	265.0 psi	Eminbend - yy 850.0 ksi
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	1,100.0 psi	Density 31.210 pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.0150, L = 0.040 ksf, Tributary Width = 11.0 ft, (FLOOR)

Point Load : E = 3.60 k @ 1.0 ft, (SW2)

Point Load : D = 0.750, S = 2.830 k @ 1.0 ft, (HDR#4)

DESIGN SUMMARY

Maximum Bending Stress Ratio		=	0.443 1	Maximum Shear Stress Ratio		=	0.903 : 1	Design OK	
Section used for this span			5.5x12	Section used for this span			5.5x12		
fb: Actual	=	1,699.22psi		fv: Actual			383.07 psi		
F'b	=	3,840.00psi		F'v			424.00 psi		
Load Combination	+1.118D+0.750L+0.750S+3.413E			Load Combination			+1.157D+4.550E		
Location of maximum on span	=	3.591ft		Location of maximum on span			0.000 ft		
Span # where maximum occurs	=	Span # 1		Span # where maximum occurs			Span # 1		
Maximum Deflection									
Max Downward Transient Deflection	0.145 in	Ratio =	994 >=360	Span: 1 : L Only					
Max Upward Transient Deflection	0 in	Ratio =	0 <360	n/a					
Max Downward Total Deflection	0.220 in	Ratio =	654 >=240	Span: 1 : +D+0.750L+0.750S+0.5250E					
Max Upward Total Deflection	0 in	Ratio =	0 <240	n/a					

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios							Moment Values			Shear Values					
			M	V	CD	CM	C _t	CLx	C _y	C _f	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only														0.0	0.00	0.0	0.0	
Length = 12.0 ft	1	0.152	0.152	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	3.61	328.5	2,160.0	1.59	36.1	238.5
+D+L					1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00		0.0	0.00	0.0	0.0	0.0
Length = 12.0 ft	1	0.437	0.326	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	11.53	1,047.8	2,400.0	3.81	86.5	265.0
+D+S					1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00		0.0	0.00	0.0	0.0	0.0
Length = 12.0 ft	1	0.173	0.312	1.15	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	5.27	478.7	2,760.0	4.18	95.1	304.8
+D+0.750L					1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00		0.0	0.00	0.0	0.0	0.0
Length = 12.0 ft	1	0.289	0.223	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	9.55	867.8	3,000.0	3.25	73.9	331.3
+D+0.750L+0.750S					1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00		0.0	0.00	0.0	0.0	0.0

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#10

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios										Moment Values			Shear Values		
			M	V	CD	CM	C _t	CLx	C _v	C _{fu}	C _i	C _r	M	f _b	F' _b	V	f _v	F' _v
Length = 12.0 ft	1	0.351	0.388	1.15	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	10.66	969.1	2,760.0	5.20	118.1	304.8
+1.157D+4.550E					1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00			0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.401	0.903	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	16.95	1,540.7	3,840.0	16.85	383.1	424.0
+1.118D+0.750L+0.750S+3.4					1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00			0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.443	0.892	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	18.69	1,699.2	3,840.0	16.65	378.3	424.0
+0.60D					1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00			0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.051	0.051	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	2.17	197.1	3,840.0	0.95	21.7	424.0
+0.4432D+4.550E					1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00			0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.373	0.843	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	15.75	1,431.8	3,840.0	15.72	357.3	424.0

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+0.750L+0.750S+0.5250E	1	0.2199	5.825		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0672	in	5.912 ft	0.0000 in
+D+L	1	0.2121	in	6.000 ft	0.0000 in
+D+S	1	0.0984	in	5.693 ft	0.0000 in
+D+0.750L	1	0.1758	in	6.000 ft	0.0000 in
+D+0.750L+0.750S	1	0.1991	in	5.869 ft	0.0000 in
+D+0.70E	1	0.0950	in	5.693 ft	0.0000 in
+D+0.750L+0.750S+0.5250E	1	0.2199	in	5.825 ft	0.0000 in
+0.60D	1	0.0403	in	5.912 ft	0.0000 in
+0.60D+0.70E	1	0.0682	in	5.606 ft	0.0000 in
L Only	1	0.1448	in	6.044 ft	0.0000 in
S Only	1	0.0316	in	5.124 ft	0.0000 in
E Only	1	0.0402	in	5.124 ft	0.0000 in

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	7.421	3.778
Max Upward from Load Combinations	7.421	3.778
Max Upward from Load Cases	3.300	2.640
D Only	1.763	1.138
+D+L	4.403	3.778
+D+S	4.357	1.374
+D+0.750L	3.743	3.118
+D+0.750L+0.750S	5.689	3.295
+D+0.70E	4.073	1.348
+D+0.750L+0.750S+0.5250E	7.421	3.453
+0.60D	1.058	0.683
+0.60D+0.70E	3.368	0.893
L Only	2.640	2.640
S Only	2.594	0.236
E Only	3.300	0.300

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#11

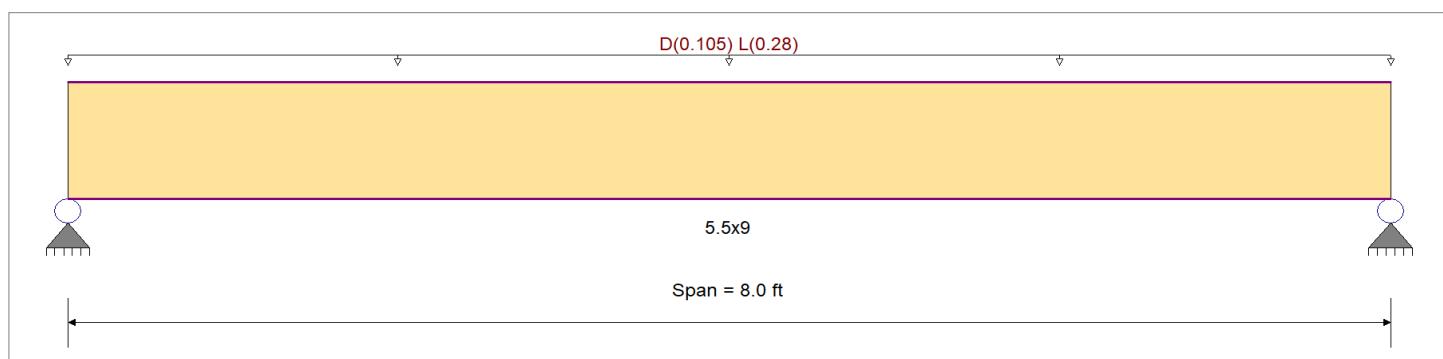
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	1,850.0 psi	Ebend- xx 1,800.0ksi
		Fc - Prll	1,650.0 psi	Eminbend - xx 950.0ksi
Wood Species	: DF/DF	Fc - Perp	650.0 psi	Ebend- yy 1,600.0ksi
Wood Grade	: 24F-V4	Fv	265.0 psi	Eminbend - yy 850.0ksi
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	1,100.0 psi	Density 31.210pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load : D = 0.0150, L = 0.040 ksf, Tributary Width = 7.0 ft, (FLOOR)

DESIGN SUMMARY

Design OK									
Maximum Bending Stress Ratio	=	0.213 1	Maximum Shear Stress Ratio	=	0.148 1				
Section used for this span		5.5x9	Section used for this span		5.5x9				
fb: Actual	=	511.65psi	fv: Actual	=	39.21 psi				
F'b	=	2,400.00psi	F'v	=	265.00 psi				
Load Combination		+D+L	Load Combination		+D+L				
Location of maximum on span	=	4.000ft	Location of maximum on span	=	7.270 ft				
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1				
Maximum Deflection									
Max Downward Transient Deflection		0.043 in	Ratio =	2224 >=360	Span: 1 : L Only				
Max Upward Transient Deflection		0 in	Ratio =	0 <360	n/a				
Max Downward Total Deflection		0.061 in	Ratio =	1573 >=240	Span: 1 : +D+L				
Max Upward Total Deflection		0 in	Ratio =	0 <240	n/a				

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios								Moment Values				Shear Values				
		Span #	M	V	CD	CM	C _t	CLx	C _y	C _f	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only														0.0	0.00	0.0	0.0	
Length = 8.0 ft	1	0.069	0.048	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	0.93	149.6	2,160.0	0.38	11.5	238.5
+D+L														0.0	0.00	0.0	0.0	
Length = 8.0 ft	1	0.213	0.148	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	3.17	511.6	2,400.0	1.29	39.2	265.0
+D+0.750L														0.0	0.00	0.0	0.0	
Length = 8.0 ft	1	0.140	0.097	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	2.61	421.1	3,000.0	1.07	32.3	331.3
+1.157D														0.0	0.00	0.0	0.0	
Length = 8.0 ft	1	0.045	0.031	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	1.07	173.1	3,840.0	0.44	13.3	424.0
+1.118D+0.750L														0.0	0.00	0.0	0.0	
Length = 8.0 ft	1	0.114	0.079	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	2.71	438.7	3,840.0	1.11	33.6	424.0

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: HDR#11

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios								Moment Values			Shear Values				
			M	V	CD	CM	C _t	CLx	C _v	C _{fu}	C _i	C _r	M	f _b	F' _b	V	f _v	F' _v
+0.60D					1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00		0.0	0.00	0.0	0.0	0.0
Length = 8.0 ft	1	0.023	0.016	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	0.56	89.8	3,840.0	0.23	6.9	424.0
+0.4432D					1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00		0.0	0.00	0.0	0.0	0.0
Length = 8.0 ft	1	0.017	0.012	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	0.41	66.3	3,840.0	0.17	5.1	424.0

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.0610	4.029		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0178 in	4.029 ft	0.0000 in	0.000 ft
+D+L	1	0.0610 in	4.029 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.0502 in	4.029 ft	0.0000 in	0.000 ft
+0.60D	1	0.0107 in	4.029 ft	0.0000 in	0.000 ft
L Only	1	0.0432 in	4.029 ft	0.0000 in	0.000 ft

Vertical Reactions

Load Combination	Support 1	Support 2	Support notation : Far left is #1	Values in KIPS
Max Upward from all Load Conditions	1.583	1.583		
Max Upward from Load Combinations	1.583	1.583		
Max Upward from Load Cases	1.120	1.120		
D Only	0.463	0.463		
+D+L	1.583	1.583		
+D+0.750L	1.303	1.303		
+0.60D	0.278	0.278		
L Only	1.120	1.120		

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#0.1

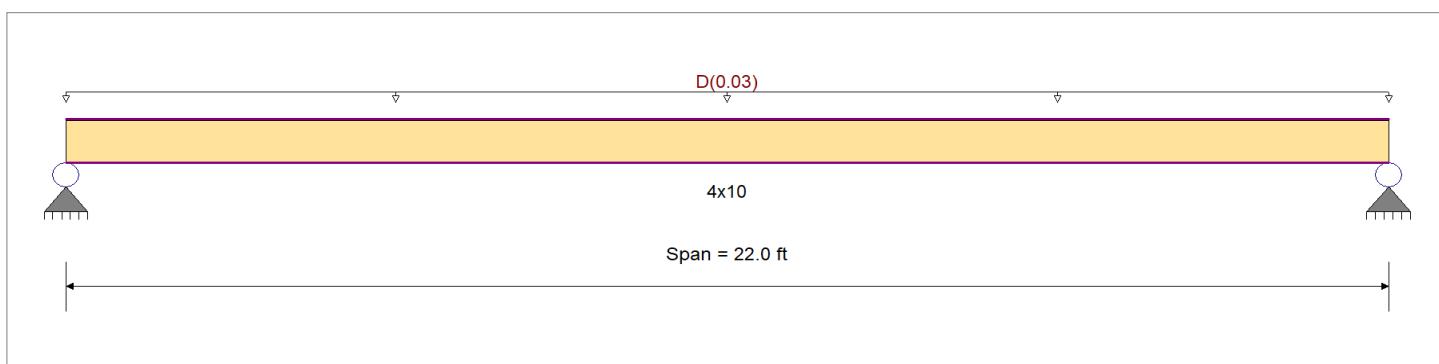
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	875.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	875.0 psi	Ebend - xx 1,300.0ksi
		Fc - Prll	600.0 psi	Eminbend - xx 470.0ksi
Wood Species	: Douglas Fir-Larch (North)	Fc - Perp	625.0 psi	
Wood Grade	: No.2	Fv	170.0 psi	
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	425.0 psi	Density 30.590pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.0150 ksf, Tributary Width = 2.0 ft, (ROOF)

DESIGN SUMMARY

				Design OK			
Maximum Bending Stress Ratio	=	0.710 : 1	Maximum Shear Stress Ratio	=	0.143 : 1		
Section used for this span		4x10	Section used for this span		4x10		
fb: Actual	=	536.41 psi	fv: Actual	=	17.56 psi		
F'b	=	756.00 psi	F'v	=	122.40 psi		
Load Combination		D Only	Load Combination		D Only		
Location of maximum on span	=	11.000ft	Location of maximum on span	=	21.277 ft		
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1		
Maximum Deflection							
Max Downward Transient Deflection		0 in	Ratio =	0 < 360	n/a		
Max Upward Transient Deflection		0 in	Ratio =	0 < 360	n/a		
Max Downward Total Deflection		0.686 in	Ratio =	384 >= 240	Span: 1 : D Only		
Max Upward Total Deflection		0 in	Ratio =	0 < 240	n/a		

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios						Moment Values				Shear Values							
		Span #	M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	fv	F'v	
D Only														0.0	0.00	0.0	0.0		
Length = 22.0 ft	1	0.710	0.143	0.90	1.00	1.00	1.00	1.200	1.00	0.80	1.00	1.00	2.23	536.4	756.0	0.38	17.6	122.4	
+0.60D									1.00	1.00	1.00	1.200	1.00	0.80	1.00		0.0	0.00	0.0
Length = 22.0 ft	1	0.239	0.048	1.60	1.00	1.00	1.00	1.200	1.00	0.80	1.00	1.00	1.34	321.8	1,344.0	0.23	10.5	217.6	

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
D Only	1	0.6858	11.080		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.6858 in	11.080 ft	0.0000 in	0.000 ft
+0.60D	1	0.4115 in	11.080 ft	0.0000 in	0.000 ft

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#0.1

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	0.406	0.406
Max Upward from Load Combinations	0.243	0.243
Max Upward from Load Cases	0.406	0.406
D Only	0.406	0.406
+0.60D	0.243	0.243

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#0.2

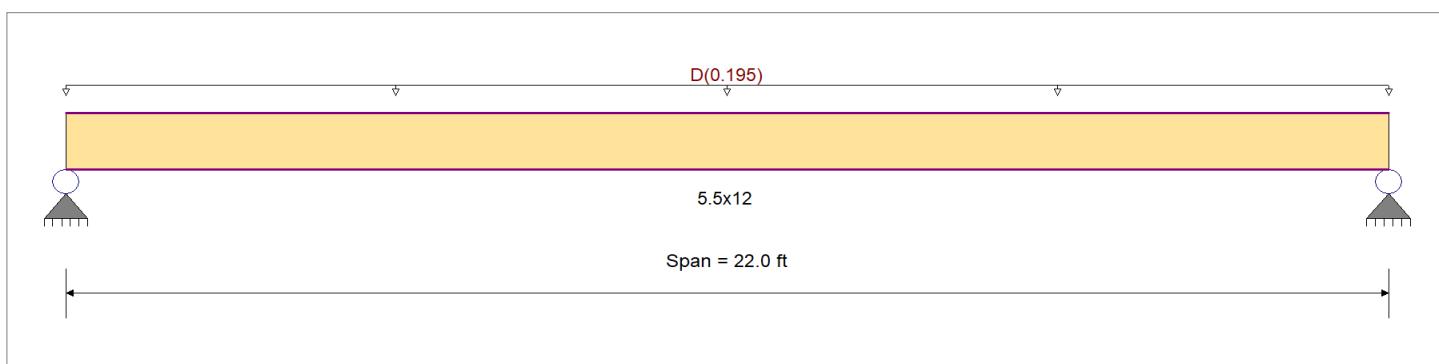
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	1,850.0 psi	Ebend - xx 1,800.0ksi
		Fc - Prll	1,650.0 psi	Eminbend - xx 950.0ksi
Wood Species	: DF/DF	Fc - Perp	650.0 psi	Ebend - yy 1,600.0ksi
Wood Grade	: 24F-V4	Fv	265.0 psi	Eminbend - yy 850.0ksi
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	1,100.0 psi	Density 31.210pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load : D = 0.0150 ksf, Tributary Width = 13.0 ft, (ROOF)

DESIGN SUMMARY

		Design OK	
Maximum Bending Stress Ratio	= 0.539 : 1	Maximum Shear Stress Ratio	= 0.200 : 1
Section used for this span	5.5x12	Section used for this span	5.5x12
fb: Actual	= 1,151.18psi	fv: Actual	= 47.74 psi
F'b	= 2,134.85psi	F'v	= 238.50 psi
Load Combination	D Only	Load Combination	D Only
Location of maximum on span	= 11.000ft	Location of maximum on span	= 21.036 ft
Span # where maximum occurs	= Span # 1	Span # where maximum occurs	= Span # 1
Maximum Deflection			
Max Downward Transient Deflection	0 in	Ratio = 0 < 360	n/a
Max Upward Transient Deflection	0 in	Ratio = 0 < 360	n/a
Max Downward Total Deflection	0.778 in	Ratio = 339 >= 240	Span: 1 : D Only
Max Upward Total Deflection	0 in	Ratio = 0 < 240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Max Stress Ratios								Moment Values				Shear Values					
	Segment Length	Span #	M	V	CD	CM	C _t	CLx	C _y	Cfu	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only															0.0	0.00	0.0	0.0
Length = 22.0 ft	1	0.539	0.200	0.90	1.00	1.00	1.00	0.988	1.00	1.00	1.00	1.00	12.66	1,151.2	2,134.8	2.10	47.7	238.5
+0.60D															0.0	0.00	0.0	0.0
Length = 22.0 ft	1	0.182	0.068	1.60	1.00	1.00	1.00	0.988	1.00	1.00	1.00	1.00	7.60	690.7	3,795.3	1.26	28.6	424.0

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
D Only	1	0.7784	11.080		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.7784 in	11.080 ft	0.0000 in	0.000 ft
+0.60D	1	0.4670 in	11.080 ft	0.0000 in	0.000 ft

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#0.2

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	2.302	2.302
Max Upward from Load Combinations	1.381	1.381
Max Upward from Load Cases	2.302	2.302
D Only	2.302	2.302
+0.60D	1.381	1.381

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#0.3

CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

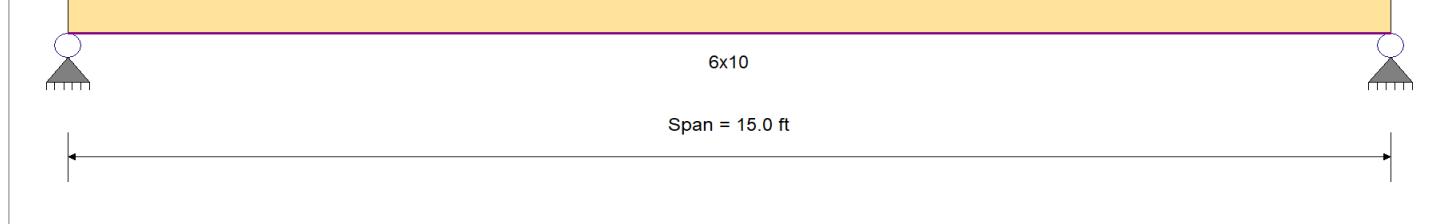
Material Properties

Analysis Method : Allowable Stress Design
Load Combination IBC 2018

Wood Species : Douglas Fir-Larch (North)
Wood Grade : No.2

Beam Bracing : Beam is Fully Braced against lateral-torsional buckling

Fb +	875.0 psi	E : Modulus of Elasticity
Fb -	875.0 psi	Ebend- xx 1,300.0ksi
Fc - Prl	600.0 psi	Eminbend - xx 470.0ksi
Fc - Perp	625.0 psi	
Fv	170.0 psi	
Ft	425.0 psi	Density 30.590pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.0150 ksf, Tributary Width = 6.0 ft, (ROOF)

DESIGN SUMMARY

Design OK							
Maximum Bending Stress Ratio	=	0.655 1	Maximum Shear Stress Ratio	=	0.160 : 1		
Section used for this span		6x10	Section used for this span		6x10		
fb: Actual	=	412.44psi	fv: Actual	=	19.54 psi		
F'b	=	630.00psi	F'v	=	122.40 psi		
Load Combination		D Only	Load Combination		D Only		
Location of maximum on span	=	7.500ft	Location of maximum on span	=	14.234 ft		
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1		
Maximum Deflection							
Max Downward Transient Deflection		0 in	Ratio =	0 < 360	n/a		
Max Upward Transient Deflection		0 in	Ratio =	0 < 360	n/a		
Max Downward Total Deflection		0.239 in	Ratio =	754 >= 240	Span: 1 : D Only		
Max Upward Total Deflection		0 in	Ratio =	0 < 240	n/a		

Maximum Forces & Stresses for Load Combinations

Load Combination	Max Stress Ratios							Moment Values			Shear Values						
	Segment Length	Span #	M	V	CD	CM	C _t	CLx	C _F	Cfu	C _i	C _r	M	fb	F'b	V	f _v
D Only													0.0	0.00	0.0	0.0	0.0
Length = 15.0 ft	1	0.655	0.160	0.90	1.00	1.00	1.00	1.000	1.00	0.80	1.00	2.84	412.4	630.0	0.68	19.5	122.4
+0.60D					1.00	1.00	1.00	1.000	1.00	0.80	1.00		0.0	0.00	0.0	0.0	0.0
Length = 15.0 ft	1	0.221	0.054	1.60	1.00	1.00	1.00	1.000	1.00	0.80	1.00	1.71	247.5	1,120.0	0.41	11.7	217.6

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
D Only	1	0.2387	7.555		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.2387 in	7.555 ft	0.0000 in	0.000 ft
+0.60D	1	0.1432 in	7.555 ft	0.0000 in	0.000 ft

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#0.3

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	0.758	0.758
Max Upward from Load Combinations	0.455	0.455
Max Upward from Load Cases	0.758	0.758
D Only	0.758	0.758
+0.60D	0.455	0.455

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#1

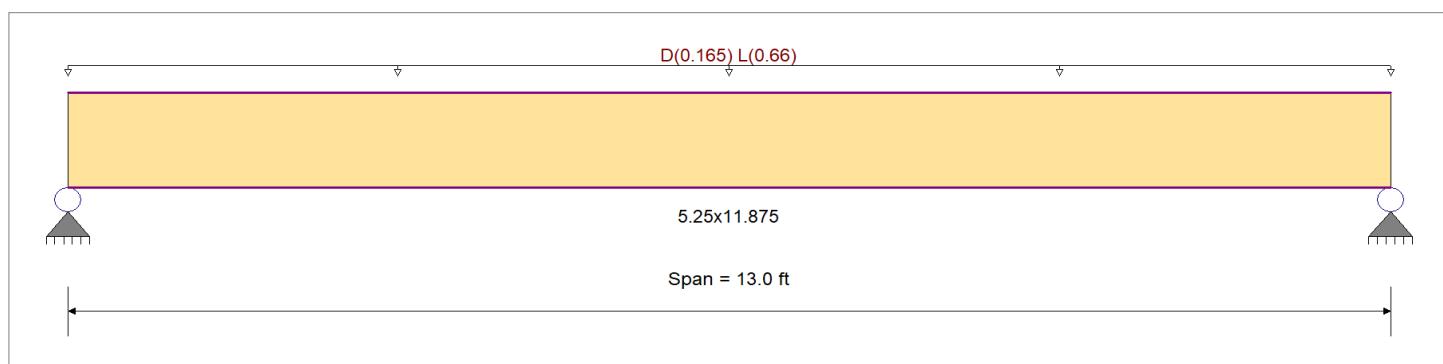
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,900.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	2,900.0 psi	Ebend- xx 2,000.0ksi
		Fc - Prll	2,900.0 psi	Eminbend - xx 1,016.54ksi
Wood Species	iLevel Truss Joist	Fc - Perp	750.0 psi	
Wood Grade	Parallam PSL 2.0E	Fv	290.0 psi	
Beam Bracing	Beam is Fully Braced against lateral-torsional buckling	Ft	2,025.0 psi	Density 45.070pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 11.0 ft, (ROOF)

DESIGN SUMMARY

Design OK			
Maximum Bending Stress Ratio	=	0.598 : 1	Maximum Shear Stress Ratio
Section used for this span		5.25x11.875	Section used for this span
fb: Actual	=	1,735.04psi	fv: Actual
F'b	=	2,903.37psi	F'v
Load Combination		+D+L	Load Combination
Location of maximum on span	=	6.500ft	Location of maximum on span
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs
Maximum Deflection			
Max Downward Transient Deflection		0.291 in	Ratio = 535 >=360 Span: 1 : L Only
Max Upward Transient Deflection		0 in	Ratio = 0 <360 n/a
Max Downward Total Deflection		0.373 in	Ratio = 418 >=240 Span: 1 : +D+L
Max Upward Total Deflection		0 in	Ratio = 0 <240 n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios							Moment Values				Shear Values				
			M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.145	0.094	0.90	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	3.90	379.1	2,613.0	1.02	24.6	261.0
+D+L															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.598	0.389	1.00	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	17.84	1,735.0	2,903.4	4.69	112.8	290.0
+D+0.750L															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.385	0.250	1.25	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	14.35	1,396.0	3,629.2	3.77	90.8	362.5
+0.60D															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.049	0.032	1.60	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	2.34	227.4	4,645.4	0.61	14.8	464.0

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#1

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.3725	6.547		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0814 in	6.547 ft	0.0000 in	0.000 ft
+D+L	1	0.3725 in	6.547 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.2998 in	6.547 ft	0.0000 in	0.000 ft
+0.60D	1	0.0488 in	6.547 ft	0.0000 in	0.000 ft
L Only	1	0.2912 in	6.547 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	5.489	5.489
Max Upward from Load Combinations	5.489	5.489
Max Upward from Load Cases	4.290	4.290
D Only	1.199	1.199
+D+L	5.489	5.489
+D+0.750L	4.417	4.417
+0.60D	0.720	0.720
L Only	4.290	4.290

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#2

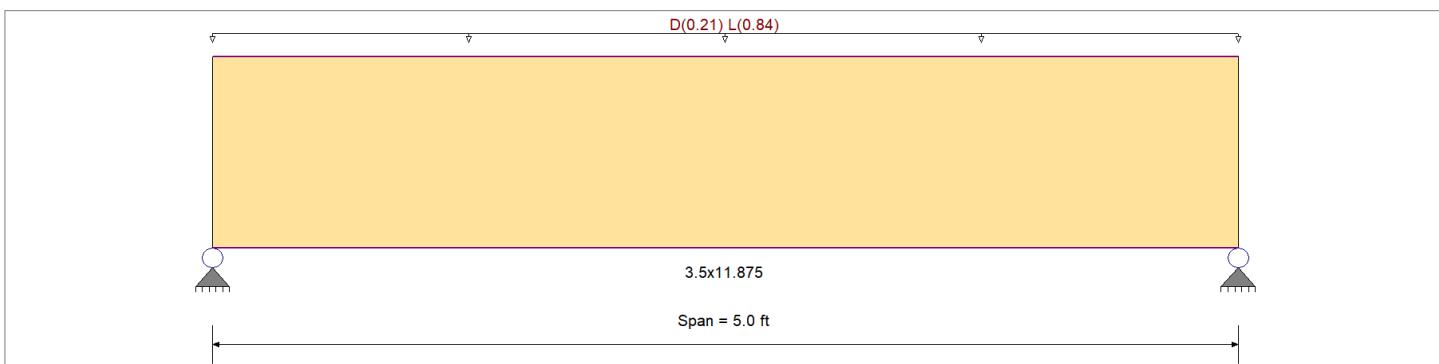
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,900.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	2,900.0 psi	Ebend - xx 2,000.0ksi
		Fc - Prl	2,900.0 psi	Eminbend - xx 1,016.54ksi
Wood Species	iLevel Truss Joist	Fc - Perp	750.0 psi	
Wood Grade	Parallam PSL 2.0E	Fv	290.0 psi	
Beam Bracing	Beam is Fully Braced against lateral-torsional buckling	Ft	2,025.0 psi	Density 45.070pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 14.0 ft, (ROOF)

DESIGN SUMMARY

Design OK				
Maximum Bending Stress Ratio	=	0.167 : 1	Maximum Shear Stress Ratio	= 0.200 : 1
Section used for this span		3.5x11.875	Section used for this span	3.5x11.875
fb: Actual	=	484.60psi	fv: Actual	58.11 psi
F'b	=	2,903.37psi	F'v	290.00 psi
Load Combination		+D+L	Load Combination	+D+L
Location of maximum on span	=	2.500ft	Location of maximum on span	0.000 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	Span # 1
Maximum Deflection				
Max Downward Transient Deflection		0.012 in	Ratio = 4932 >= 360	Span: 1 : L Only
Max Upward Transient Deflection		0 in	Ratio = 0 < 360	n/a
Max Downward Total Deflection		0.015 in	Ratio = 3897 >= 240	Span: 1 : +D+L
Max Upward Total Deflection		0 in	Ratio = 0 < 240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios							Moment Values					Shear Values				
		Span #	M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	fv	F'v
D Only														0.0	0.00	0.0	0.0	
Length = 5.0 ft	1	0.039	0.047	0.90	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	0.70	101.7	2,613.0	0.34	12.2	261.0
+D+L														0.0	0.00	0.0	0.0	
Length = 5.0 ft	1	0.167	0.200	1.00	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	3.32	484.6	2,903.4	1.61	58.1	290.0
+D+0.750L														0.0	0.00	0.0	0.0	
Length = 5.0 ft	1	0.107	0.129	1.25	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	2.67	388.9	3,629.2	1.29	46.6	362.5
+0.60D														0.0	0.00	0.0	0.0	
Length = 5.0 ft	1	0.013	0.016	1.60	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	0.42	61.0	4,645.4	0.20	7.3	464.0

Project Title:
Engineer:
Project ID:
Project Descr:

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#2

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.0154	2.518		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0032 in	2.518 ft	0.0000 in	0.000 ft
+D+L	1	0.0154 in	2.518 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.0124 in	2.518 ft	0.0000 in	0.000 ft
+0.60D	1	0.0019 in	2.518 ft	0.0000 in	0.000 ft
L Only	1	0.0122 in	2.518 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	2.658	2.658
Max Upward from Load Combinations	2.658	2.658
Max Upward from Load Cases	2.100	2.100
D Only	0.558	0.558
+D+L	2.658	2.658
+D+0.750L	2.133	2.133
+0.60D	0.335	0.335
L Only	2.100	2.100

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#3

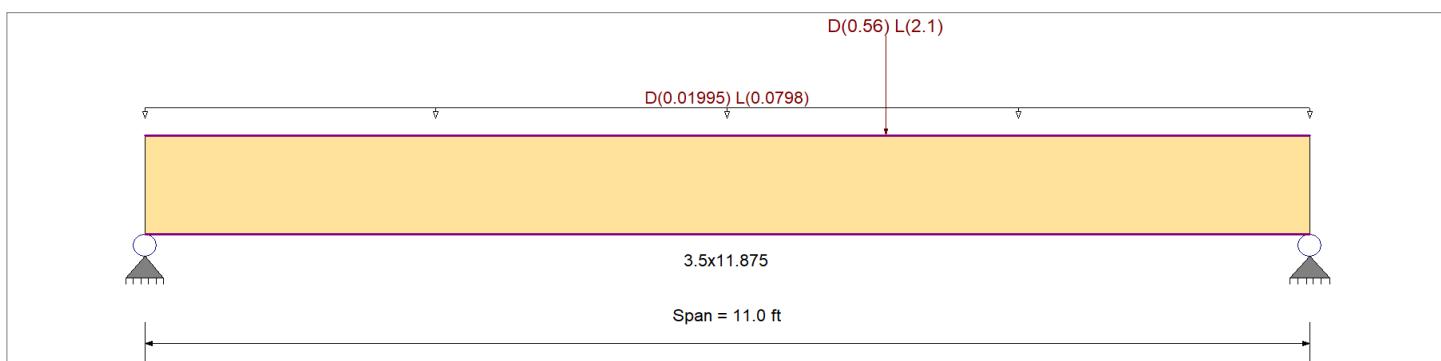
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,900.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	2,900.0 psi	Ebend - xx 2,000.0ksi
		Fc - Prll	2,900.0 psi	Eminbend - xx 1,016.54ksi
Wood Species	iLevel Truss Joist	Fc - Perp	750.0 psi	
Wood Grade	Parallam PSL 2.0E	Fv	290.0 psi	
Beam Bracing	Beam is Fully Braced against lateral-torsional buckling	Ft	2,025.0 psi	Density 45.070pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 1.330 ft, (ROOF)

Point Load : D = 0.560, L = 2.10 k @ 7.0 ft, (BM#2)

DESIGN SUMMARY

				Design OK
Maximum Bending Stress Ratio	=	0.419 : 1	Maximum Shear Stress Ratio	=
Section used for this span		3.5x11.875	Section used for this span	=
fb: Actual	=	1,216.33psi	fv: Actual	=
F'b	=	2,903.37psi	F'v	=
Load Combination		+D+L	Load Combination	
Location of maximum on span	=	6.985ft	Location of maximum on span	=
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=
Maximum Deflection				
Max Downward Transient Deflection		0.121 in	Ratio = 1094 >= 360	Span: 1 : L Only
Max Upward Transient Deflection		0 in	Ratio = 0 < 360	n/a
Max Downward Total Deflection		0.157 in	Ratio = 842 >= 240	Span: 1 : +D+L
Max Upward Total Deflection		0 in	Ratio = 0 < 240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios						Moment Values			Shear Values						
			M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	fv	F'v
D Only															0.0	0.00	0.0	0.0
Length = 11.0 ft	1	0.105	0.070	0.90	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.88	274.9	2,613.0	0.51	18.3	261.0
+D+L															0.0	0.00	0.0	0.0
Length = 11.0 ft	1	0.419	0.274	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	8.34	1,216.3	2,903.4	2.20	79.6	290.0
+D+0.750L															0.0	0.00	0.0	0.0
Length = 11.0 ft	1	0.270	0.177	1.25	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	6.72	981.0	3,629.2	1.78	64.2	362.5
+0.60D															0.0	0.00	0.0	0.0
Length = 11.0 ft	1	0.036	0.024	1.60	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.13	165.0	4,645.4	0.30	11.0	464.0

Project Title:
Engineer:
Project ID:
Project Descr:

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#3

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.1567	5.821		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0361 in	5.821 ft	0.0000 in	0.000 ft
+D+L	1	0.1567 in	5.821 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.1266 in	5.821 ft	0.0000 in	0.000 ft
+0.60D	1	0.0217 in	5.821 ft	0.0000 in	0.000 ft
L Only	1	0.1206 in	5.861 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	1.587	2.313
Max Upward from Load Combinations	1.587	2.313
Max Upward from Load Cases	1.203	1.775
D Only	0.385	0.538
+D+L	1.587	2.313
+D+0.750L	1.287	1.869
+0.60D	0.231	0.323
L Only	1.203	1.775

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#4

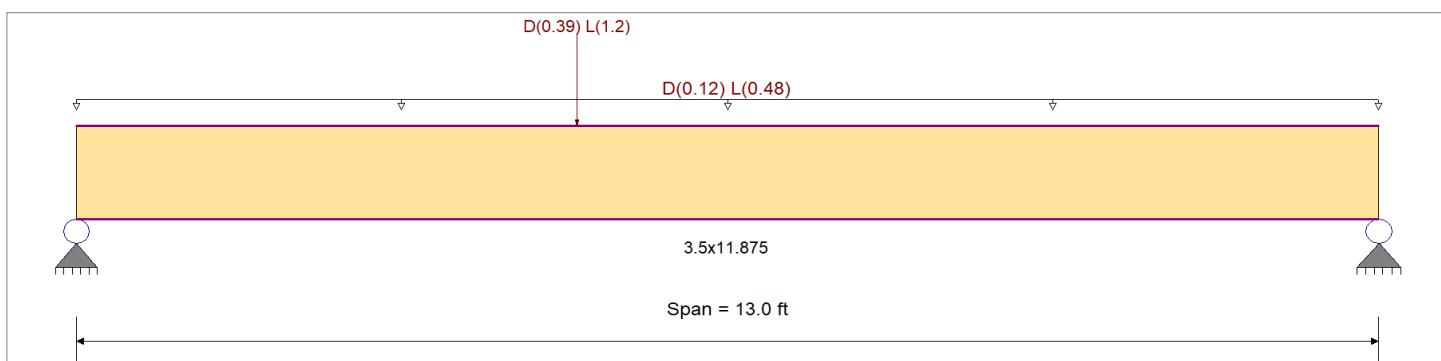
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,900.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	2,900.0 psi	Ebend - xx 2,000.0ksi
		Fc - Prll	2,900.0 psi	Eminbend - xx 1,016.54ksi
Wood Species	iLevel Truss Joist	Fc - Perp	750.0 psi	
Wood Grade	Parallam PSL 2.0E	Fv	290.0 psi	
Beam Bracing	Beam is Fully Braced against lateral-torsional buckling	Ft	2,025.0 psi	Density 45.070pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 8.0 ft, (ROOF)

Point Load : D = 0.390, L = 1.20 k @ 5.0 ft, (BM#3)

DESIGN SUMMARY

		Design OK	
Maximum Bending Stress Ratio	= 0.866 1	Maximum Shear Stress Ratio	= 0.545 : 1
Section used for this span	3.5x11.875	Section used for this span	3.5x11.875
fb: Actual	= 2,513.50psi	fv: Actual	= 158.12 psi
F'b	= 2,903.37psi	F'v	= 290.00 psi
Load Combination	+D+L	Load Combination	+D+L
Location of maximum on span	= 5.504ft	Location of maximum on span	= 0.000 ft
Span # where maximum occurs	= Span # 1	Span # where maximum occurs	= Span # 1
Maximum Deflection			
Max Downward Transient Deflection	0.408 in	Ratio = 382 >= 360	Span: 1 : L Only
Max Upward Transient Deflection	0 in	Ratio = 0 < 360	n/a
Max Downward Total Deflection	0.526 in	Ratio = 296 >= 240	Span: 1 : +D+L
Max Upward Total Deflection	0 in	Ratio = 0 < 240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios						Moment Values				Shear Values					
			M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.216	0.135	0.90	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	3.87	564.5	2,613.0	0.98	35.3	261.0
+D+L															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.866	0.545	1.00	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	17.23	2,513.5	2,903.4	4.38	158.1	290.0
+D+0.750L															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.558	0.352	1.25	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	13.89	2,026.2	3,629.2	3.53	127.4	362.5
+0.60D															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.073	0.046	1.60	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	2.32	338.7	4,645.4	0.59	21.2	464.0

Project Title:
Engineer:
Project ID:
Project Descr:

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#4

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.5258	6.405		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.1175 in	6.405 ft	0.0000 in	0.000 ft
+D+L	1	0.5258 in	6.405 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.4237 in	6.405 ft	0.0000 in	0.000 ft
+0.60D	1	0.0705 in	6.405 ft	0.0000 in	0.000 ft
L Only	1	0.4083 in	6.405 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	4.963	4.596
Max Upward from Load Combinations	4.963	4.596
Max Upward from Load Cases	3.858	3.582
D Only	1.105	1.015
+D+L	4.963	4.596
+D+0.750L	3.998	3.701
+0.60D	0.663	0.609
L Only	3.858	3.582

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#5

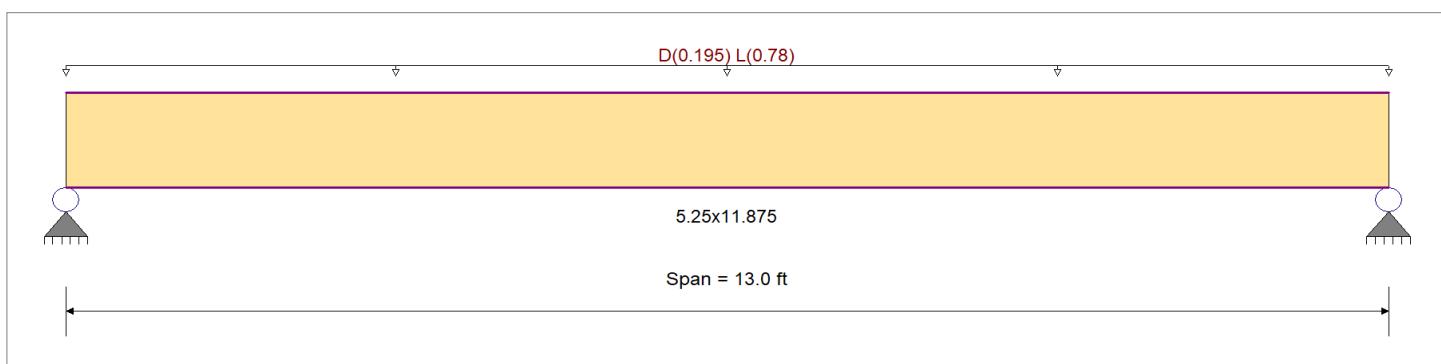
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,900.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	2,900.0 psi	Ebend- xx 2,000.0ksi
		Fc - Prll	2,900.0 psi	Eminbend - xx 1,016.54ksi
Wood Species	iLevel Truss Joist	Fc - Perp	750.0 psi	
Wood Grade	Parallam PSL 2.0E	Fv	290.0 psi	
Beam Bracing	Beam is Fully Braced against lateral-torsional buckling	Ft	2,025.0 psi	Density 45.070pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 13.0 ft, (ROOF)

DESIGN SUMMARY

		Design OK	
Maximum Bending Stress Ratio	= 0.704 : 1	Maximum Shear Stress Ratio	= 0.458 : 1
Section used for this span	5.25x11.875	Section used for this span	5.25x11.875
fb: Actual	= 2,043.21psi	fv: Actual	= 132.83 psi
F'b	= 2,903.37psi	F'v	= 290.00 psi
Load Combination	+D+L	Load Combination	+D+L
Location of maximum on span	= 6.500ft	Location of maximum on span	= 12.051 ft
Span # where maximum occurs	= Span # 1	Span # where maximum occurs	= Span # 1
Maximum Deflection			
Max Downward Transient Deflection	0.344 in	Ratio = 453 >= 360	Span: 1 : L Only
Max Upward Transient Deflection	0 in	Ratio = 0 < 360	n/a
Max Downward Total Deflection	0.439 in	Ratio = 355 >= 240	Span: 1 : +D+L
Max Upward Total Deflection	0 in	Ratio = 0 < 240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios								Moment Values				Shear Values				
		Span #	M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.169	0.110	0.90	1.00	1.00	1.00	1.001	1.00	1.00	1.00	1.00	4.53	440.7	2,613.0	1.19	28.7	261.0
+D+L															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.704	0.458	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	1.00	21.01	2,043.2	2,903.4	5.52	132.8	290.0
+D+0.750L															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.453	0.295	1.25	1.00	1.00	1.00	1.001	1.00	1.00	1.00	1.00	16.89	1,642.6	3,629.2	4.44	106.8	362.5
+0.60D															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.057	0.037	1.60	1.00	1.00	1.00	1.001	1.00	1.00	1.00	1.00	2.72	264.4	4,645.4	0.71	17.2	464.0

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#5

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.4387	6.547		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0946 in	6.547 ft	0.0000 in	0.000 ft
+D+L	1	0.4387 in	6.547 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.3527 in	6.547 ft	0.0000 in	0.000 ft
+0.60D	1	0.0568 in	6.547 ft	0.0000 in	0.000 ft
L Only	1	0.3441 in	6.547 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	6.464	6.464
Max Upward from Load Combinations	6.464	6.464
Max Upward from Load Cases	5.070	5.070
D Only	1.394	1.394
+D+L	6.464	6.464
+D+0.750L	5.197	5.197
+0.60D	0.837	0.837
L Only	5.070	5.070

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#6

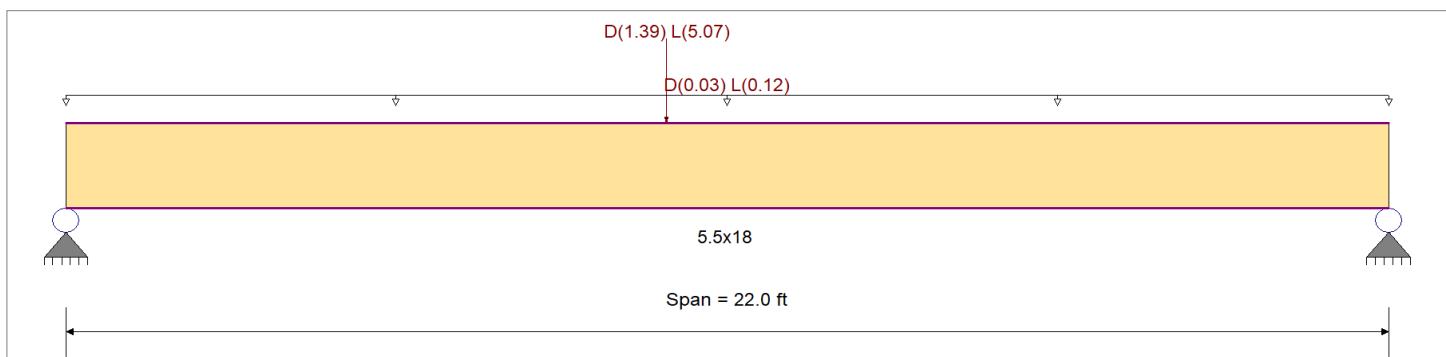
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	1,850.0 psi	Ebend - xx 1,800.0ksi
		Fc - Prll	1,650.0 psi	Eminbend - xx 950.0ksi
Wood Species	: DF/DF	Fc - Perp	650.0 psi	Ebend - yy 1,600.0ksi
Wood Grade	: 24F-V4	Fv	265.0 psi	Eminbend - yy 850.0ksi
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	1,100.0 psi	Density 31.210pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : $D = 0.0150$, $L = 0.060$ ksf, Tributary Width = 2.0 ft, (ROOF)

Point Load : $D = 1.390$, $L = 5.070$ k @ 10.0 ft, (BM#5)

DESIGN SUMMARY

			Design OK		
Maximum Bending Stress Ratio	=	0.806 1	Maximum Shear Stress Ratio	=	0.295 : 1
Section used for this span		5.5x18	Section used for this span		5.5x18
fb: Actual	=	1,835.26psi	fv: Actual	=	78.21 psi
F'b	=	2,277.80psi	F'v	=	265.00 psi
Load Combination		+D+L	Load Combination		+D+L
Location of maximum on span	=	10.036ft	Location of maximum on span	=	0.000 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
Maximum Deflection					
Max Downward Transient Deflection		0.534 in	Ratio =	494 >=360	Span: 1 : L Only
Max Upward Transient Deflection		0 in	Ratio =	0 <360	n/a
Max Downward Total Deflection		0.701 in	Ratio =	376 >=240	Span: 1 : +D+L
Max Upward Total Deflection		0 in	Ratio =	0 <240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios							Moment Values				Shear Values				
			M	V	CD	CM	C _t	CLx	C _y	C _f	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only															0.0	0.00	0.0	0.0
Length = 22.0 ft	1	0.210	0.079	0.90	1.00	1.00	1.00	0.949	1.00	1.00	1.00	1.00	10.65	430.2	2,050.0	1.25	18.9	238.5
+D+L															0.0	0.00	0.0	0.0
Length = 22.0 ft	1	0.806	0.295	1.00	1.00	1.00	1.00	0.949	1.00	1.00	1.00	1.00	45.42	1,835.3	2,277.8	5.16	78.2	265.0
+D+0.750L															0.0	0.00	0.0	0.0
Length = 22.0 ft	1	0.521	0.191	1.25	1.00	1.00	1.00	0.949	1.00	1.00	1.00	1.00	36.73	1,484.0	2,847.2	4.18	63.4	331.3
+0.60D															0.0	0.00	0.0	0.0
Length = 22.0 ft	1	0.071	0.027	1.60	1.00	1.00	1.00	0.949	1.00	1.00	1.00	1.00	6.39	258.1	3,644.5	0.75	11.4	424.0

Project Title:
Engineer:
Project ID:
Project Descr:

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#6

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.7007	10.839		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.1668 in	10.839 ft	0.0000 in	0.000 ft
+D+L	1	0.7007 in	10.839 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.5672 in	10.839 ft	0.0000 in	0.000 ft
+0.60D	1	0.1001 in	10.839 ft	0.0000 in	0.000 ft
L Only	1	0.5339 in	10.759 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	5.410	4.822
Max Upward from Load Combinations	5.410	4.822
Max Upward from Load Cases	4.085	3.625
D Only	1.324	1.198
+D+L	5.410	4.822
+D+0.750L	4.388	3.916
+0.60D	0.795	0.719
L Only	4.085	3.625

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#7

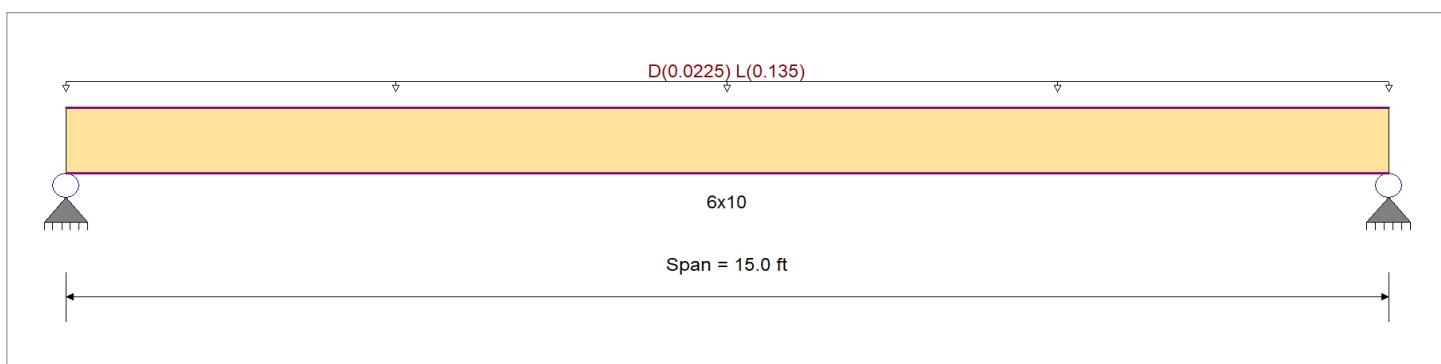
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	875.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	875.0 psi	Ebend- xx 1,300.0ksi
		Fc - Prll	600.0 psi	Eminbend - xx 470.0ksi
Wood Species	: Douglas Fir-Larch (North)	Fc - Perp	625.0 psi	
Wood Grade	: No.2	Fv	170.0 psi	
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	425.0 psi	Density 30.590pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load : D = 0.010, L = 0.060 ksf, Tributary Width = 2.250 ft, (DECK)

DESIGN SUMMARY

Design OK			
Maximum Bending Stress Ratio	=	0.983 1	Maximum Shear Stress Ratio
Section used for this span		6x10	Section used for this span
fb: Actual	=	687.81psi	fv: Actual
F'b	=	700.00psi	F'v
Load Combination		+D+L	Load Combination
Location of maximum on span	=	7.500ft	Location of maximum on span
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs
Maximum Deflection			
Max Downward Transient Deflection		0.319 in	Ratio = 564 >=360 Span: 1 : L Only
Max Upward Transient Deflection		0 in	Ratio = 0 <360 n/a
Max Downward Total Deflection		0.398 in	Ratio = 452 >=240 Span: 1 : +D+L
Max Upward Total Deflection		0 in	Ratio = 0 <240 n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios								Moment Values				Shear Values			
		Span #	M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	f _v
D Only														0.0	0.00	0.0	0.0
Length = 15.0 ft	1	0.218	0.053	0.90	1.00	1.00	1.00	1.000	1.00	0.80	1.00	0.94	137.1	630.0	0.23	6.5	122.4
+D+L														0.0	0.00	0.0	0.0
Length = 15.0 ft	1	0.983	0.240	1.00	1.00	1.00	1.00	1.000	1.00	0.80	1.00	4.74	687.8	700.0	1.14	32.6	136.0
+D+0.750L														0.0	0.00	0.0	0.0
Length = 15.0 ft	1	0.629	0.153	1.25	1.00	1.00	1.00	1.000	1.00	0.80	1.00	3.79	550.1	875.0	0.91	26.1	170.0
+0.60D														0.0	0.00	0.0	0.0
Length = 15.0 ft	1	0.073	0.018	1.60	1.00	1.00	1.00	1.000	1.00	0.80	1.00	0.57	82.2	1,120.0	0.14	3.9	217.6

Project Title:
Engineer:
Project ID:
Project Descr:

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#7

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.3980	7.555		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0793 in	7.555 ft	0.0000 in	0.000 ft
+D+L	1	0.3980 in	7.555 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.3184 in	7.555 ft	0.0000 in	0.000 ft
+0.60D	1	0.0476 in	7.555 ft	0.0000 in	0.000 ft
L Only	1	0.3187 in	7.555 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	1.264	1.264
Max Upward from Load Combinations	1.264	1.264
Max Upward from Load Cases	1.013	1.013
D Only	0.252	0.252
+D+L	1.264	1.264
+D+0.750L	1.011	1.011
+0.60D	0.151	0.151
L Only	1.013	1.013

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#7.1

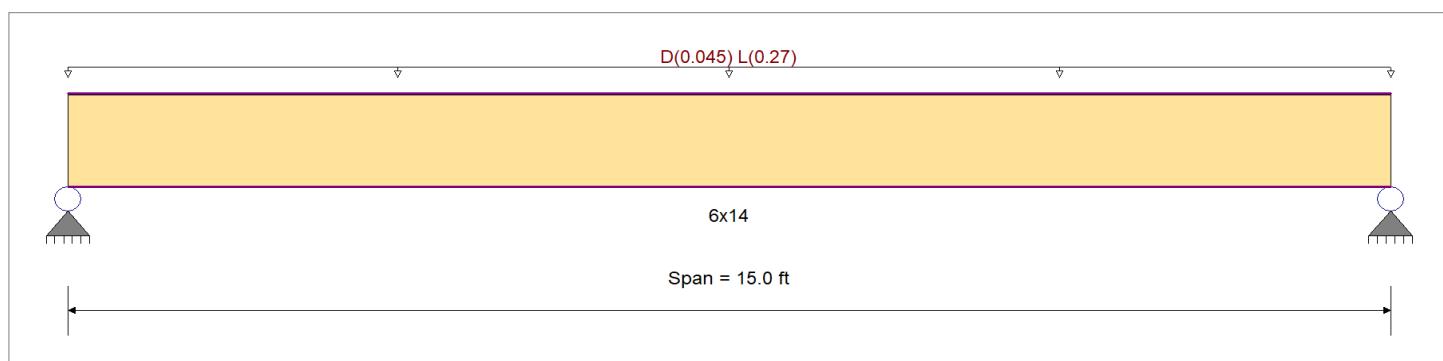
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	875.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	875.0 psi	Ebend- xx 1,300.0ksi
		Fc - Prll	600.0 psi	Eminbend - xx 470.0ksi
Wood Species	: Douglas Fir-Larch (North)	Fc - Perp	625.0 psi	
Wood Grade	: No.2	Fv	170.0 psi	
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	425.0 psi	Density 30.590pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load : D = 0.010, L = 0.060 ksf, Tributary Width = 4.50 ft, (DECK)

DESIGN SUMMARY

Design OK			
Maximum Bending Stress Ratio	=	0.967. 1	Maximum Shear Stress Ratio
Section used for this span	=	6x14	Section used for this span
fb: Actual	=	668.23psi	fv: Actual
F'b	=	690.90psi	F'v
Load Combination	=	+D+L	Load Combination
Location of maximum on span	=	7.500ft	Location of maximum on span
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs
Maximum Deflection			
Max Downward Transient Deflection		0.222 in	Ratio = 810 >=360 Span: 1 : L Only
Max Upward Transient Deflection		0 in	Ratio = 0 <360 n/a
Max Downward Total Deflection		0.272 in	Ratio = 661 >=240 Span: 1 : +D+L
Max Upward Total Deflection		0 in	Ratio = 0 <240 n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios							Moment Values				Shear Values				
			M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only														0.0	0.00	0.0	0.0	
Length = 15.0 ft	1	0.197	0.064	0.90	1.00	1.00	1.00	0.987	1.00	0.80	1.00	1.00	1.71	122.8	621.8	0.39	7.9	122.4
+D+L														0.0	0.00	0.0	0.0	
Length = 15.0 ft	1	0.967	0.315	1.00	1.00	1.00	1.00	0.987	1.00	0.80	1.00	1.00	9.30	668.2	690.9	2.12	42.8	136.0
+D+0.750L														0.0	0.00	0.0	0.0	
Length = 15.0 ft	1	0.616	0.200	1.25	1.00	1.00	1.00	0.987	1.00	0.80	1.00	1.00	7.40	531.9	863.6	1.69	34.1	170.0
+0.60D														0.0	0.00	0.0	0.0	
Length = 15.0 ft	1	0.067	0.022	1.60	1.00	1.00	1.00	0.987	1.00	0.80	1.00	1.00	1.03	73.7	1,105.4	0.23	4.7	217.6

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#7.1

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.2721	7.555		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0500 in	7.555 ft	0.0000 in	0.000 ft
+D+L	1	0.2721 in	7.555 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.2166 in	7.555 ft	0.0000 in	0.000 ft
+0.60D	1	0.0300 in	7.555 ft	0.0000 in	0.000 ft
L Only	1	0.2221 in	7.555 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	2.481	2.481
Max Upward from Load Combinations	2.481	2.481
Max Upward from Load Cases	2.025	2.025
D Only	0.456	0.456
+D+L	2.481	2.481
+D+0.750L	1.975	1.975
+0.60D	0.273	0.273
L Only	2.025	2.025

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#8

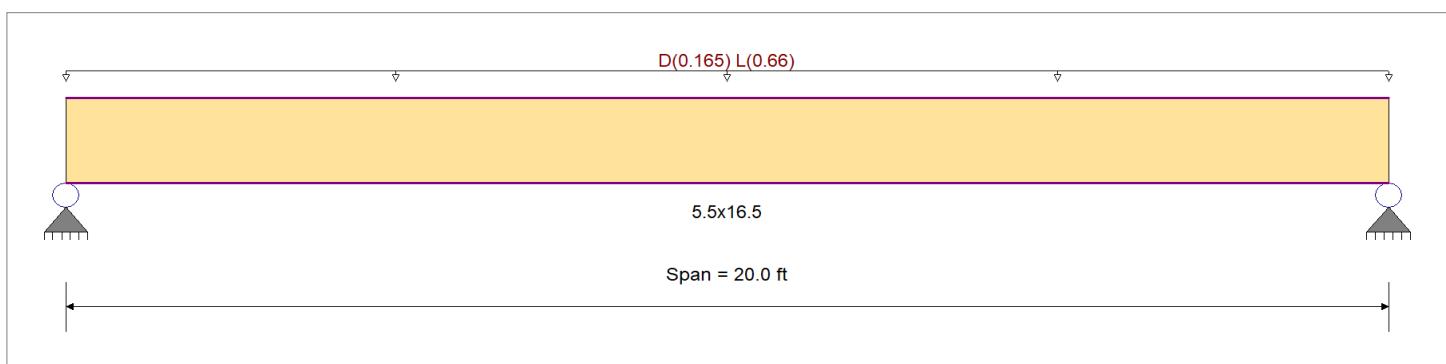
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	1,850.0 psi	Ebend- xx 1,800.0ksi
		Fc - Prll	1,650.0 psi	Eminbend - xx 950.0ksi
Wood Species	: DF/DF	Fc - Perp	650.0 psi	Ebend- yy 1,600.0ksi
Wood Grade	: 24F-V4	Fv	265.0 psi	Eminbend - yy 850.0ksi
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	1,100.0 psi	Density 31.210pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 11.0 ft, (DECK)

DESIGN SUMMARY

				Design OK	
Maximum Bending Stress Ratio	=	0.875	1	Maximum Shear Stress Ratio	= 0.458 : 1
Section used for this span		5.5x16.5		Section used for this span	= 5.5x16.5
fb: Actual	=	2,030.76psi		fv: Actual	= 121.27 psi
F'b	=	2,319.71psi		F'v	= 265.00 psi
Load Combination		+D+L		Load Combination	+D+L
Location of maximum on span	=	10.000ft		Location of maximum on span	= 0.000 ft
Span # where maximum occurs	=	Span # 1		Span # where maximum occurs	= Span # 1
Maximum Deflection					
Max Downward Transient Deflection		0.645 in	Ratio =	372 >=360	Span: 1 : L Only
Max Upward Transient Deflection		0 in	Ratio =	0 <360	n/a
Max Downward Total Deflection		0.825 in	Ratio =	290 >=240	Span: 1 : +D+L
Max Upward Total Deflection		0 in	Ratio =	0 <240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios								Moment Values				Shear Values				
		Span #	M	V	CD	CM	C _t	CLx	C _y	C _f	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only														0.0	0.00	0.0	0.0	
Length = 20.0 ft	1	0.213	0.111	0.90	1.00	1.00	1.00	0.967	1.00	1.00	1.00	1.00	9.23	444.0	2,087.7	1.60	26.5	238.5
+D+L														0.0	0.00	0.0	0.0	
Length = 20.0 ft	1	0.875	0.458	1.00	1.00	1.00	1.00	0.967	1.00	1.00	1.00	1.00	42.23	2,030.8	2,319.7	7.34	121.3	265.0
+D+0.750L														0.0	0.00	0.0	0.0	
Length = 20.0 ft	1	0.564	0.295	1.25	1.00	1.00	1.00	0.967	1.00	1.00	1.00	1.00	33.98	1,634.1	2,899.6	5.90	97.6	331.3
+0.60D														0.0	0.00	0.0	0.0	
Length = 20.0 ft	1	0.072	0.038	1.60	1.00	1.00	1.00	0.967	1.00	1.00	1.00	1.00	5.54	266.4	3,711.5	0.96	15.9	424.0

Project Title:
Engineer:
Project ID:
Project Descr:

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#8

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.8253	10.073		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.1804 in	10.073 ft	0.0000 in	0.000 ft
+D+L	1	0.8253 in	10.073 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.6641 in	10.073 ft	0.0000 in	0.000 ft
+0.60D	1	0.1083 in	10.073 ft	0.0000 in	0.000 ft
L Only	1	0.6449 in	10.073 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	8.447	8.447
Max Upward from Load Combinations	8.447	8.447
Max Upward from Load Cases	6.600	6.600
D Only	1.847	1.847
+D+L	8.447	8.447
+D+0.750L	6.797	6.797
+0.60D	1.108	1.108
L Only	6.600	6.600

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#9

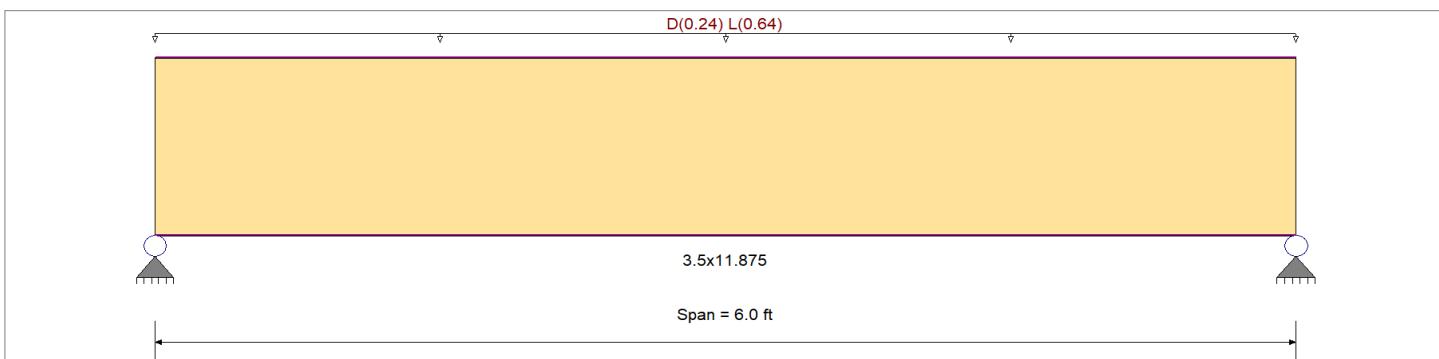
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,900.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	2,900.0 psi	Ebend- xx 2,000.0ksi
		Fc - Prll	2,900.0 psi	Eminbend - xx 1,016.54ksi
Wood Species	iLevel Truss Joist	Fc - Perp	750.0 psi	
Wood Grade	Parallam PSL 2.0E	Fv	290.0 psi	
Beam Bracing	Beam is Fully Braced against lateral-torsional buckling	Ft	2,025.0 psi	Density 45.070pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.0150, L = 0.040 ksf, Tributary Width = 16.0 ft, (FLOOR)

DESIGN SUMMARY

Design OK			
Maximum Bending Stress Ratio	=	0.202 1	Maximum Shear Stress Ratio
Section used for this span	=	3.5x11.875	Section used for this span
fb: Actual	=	586.23psi	fv: Actual
F'b	=	2,903.37psi	F'v
Load Combination	=	+D+L	Load Combination
Location of maximum on span	=	3.000ft	Location of maximum on span
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs
Maximum Deflection			
Max Downward Transient Deflection		0.019 in	Ratio = 3746 >= 360 Span: 1 : L Only
Max Upward Transient Deflection		0 in	Ratio = 0 < 360 n/a
Max Downward Total Deflection		0.027 in	Ratio = 2685 >= 240 Span: 1 : +D+L
Max Upward Total Deflection		0 in	Ratio = 0 < 240 n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Max Stress Ratios								Moment Values				Shear Values					
	Segment Length	Span #	M	V	CD	CM	C _t	C _{Lx}	C _F	C _f	C _i	C _r	M	fb	F'b	V	fv	F'v
D Only															0.0	0.00	0.0	0.0
Length = 6.0 ft	1	0.064	0.070	0.90	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	1.14	166.1	2,613.0	0.51	18.4	261.0
+D+L															0.0	0.00	0.0	0.0
Length = 6.0 ft	1	0.202	0.224	1.00	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	4.02	586.2	2,903.4	1.80	64.9	290.0
+D+0.750L															0.0	0.00	0.0	0.0
Length = 6.0 ft	1	0.133	0.147	1.25	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	3.30	481.2	3,629.2	1.48	53.3	362.5
+0.60D															0.0	0.00	0.0	0.0
Length = 6.0 ft	1	0.021	0.024	1.60	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	0.68	99.7	4,645.4	0.31	11.0	464.0

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#9

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.0268	3.022		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0076 in	3.022 ft	0.0000 in	0.000 ft
+D+L	1	0.0268 in	3.022 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.0220 in	3.022 ft	0.0000 in	0.000 ft
+0.60D	1	0.0046 in	3.022 ft	0.0000 in	0.000 ft
L Only	1	0.0192 in	3.022 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	2.679	2.679
Max Upward from Load Combinations	2.679	2.679
Max Upward from Load Cases	1.920	1.920
D Only	0.759	0.759
+D+L	2.679	2.679
+D+0.750L	2.199	2.199
+0.60D	0.455	0.455
L Only	1.920	1.920

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#10

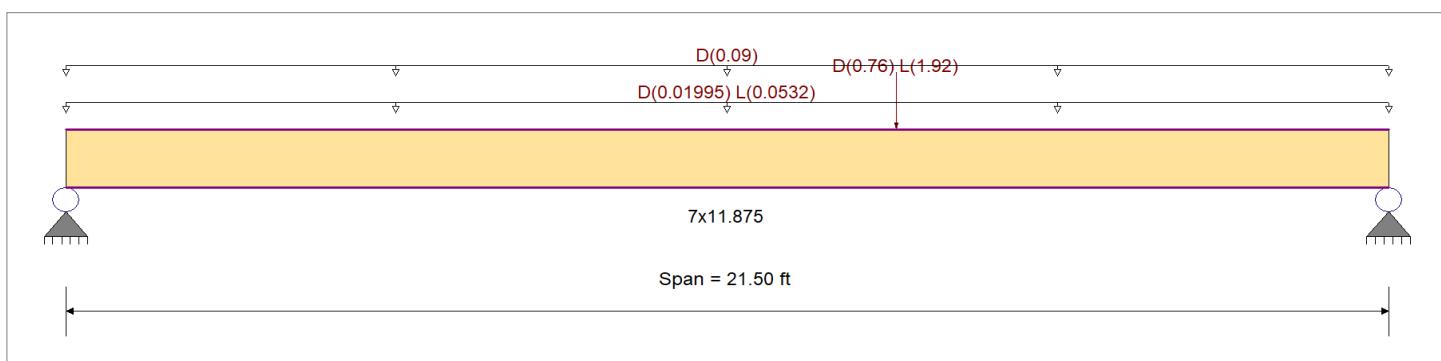
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,900.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	2,900.0 psi	Ebend- xx 2,000.0ksi
		Fc - Prll	2,900.0 psi	Eminbend - xx 1,016.54ksi
Wood Species	iLevel Truss Joist	Fc - Perp	750.0 psi	
Wood Grade	Parallam PSL 2.0E	Fv	290.0 psi	
Beam Bracing	Beam is Fully Braced against lateral-torsional buckling	Ft	2,025.0 psi	Density 45.070pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.0150, L = 0.040 ksf, Tributary Width = 1.330 ft, (FLOOR)

Uniform Load : D = 0.010 ksf, Tributary Width = 9.0 ft, (WALL)

Point Load : D = 0.760, L = 1.920 k @ 13.50 ft, (BM#9)

DESIGN SUMMARY

Design OK			
Maximum Bending Stress Ratio	=	0.595 : 1	Maximum Shear Stress Ratio
Section used for this span	=	7x11.875	Section used for this span
fb: Actual	=	1,726.90psi	fv: Actual
F'b	=	2,903.37psi	F'v
Load Combination	=	+D+L	Load Combination
Location of maximum on span	=	13.496ft	Location of maximum on span
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs
Maximum Deflection			
Max Downward Transient Deflection	0.455 in	Ratio = 567 >=360	Span: 1 : L Only
Max Upward Transient Deflection	0 in	Ratio = 0 <360	n/a
Max Downward Total Deflection	0.919 in	Ratio = 280 >=240	Span: 1 : +D+L
Max Upward Total Deflection	0 in	Ratio = 0 <240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios								Moment Values			Shear Values				
			M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only															0.0	0.00	0.0	0.0
Length = 21.50 ft	1	0.312	0.125	0.90	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	11.19	816.2	2,613.0	1.81	32.7	261.0
+D+L															0.0	0.00	0.0	0.0
Length = 21.50 ft	1	0.595	0.220	1.00	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	23.68	1,726.9	2,903.4	3.54	63.8	290.0
+D+0.750L															0.0	0.00	0.0	0.0
Length = 21.50 ft	1	0.413	0.155	1.25	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	20.55	1,498.7	3,629.2	3.11	56.1	362.5
+0.60D															0.0	0.00	0.0	0.0
Length = 21.50 ft	1	0.105	0.042	1.60	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	6.71	489.7	4,645.4	1.09	19.6	464.0

Project Title:
Engineer:
Project ID:
Project Descr:

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#10

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.9187	11.221		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.4641 in	10.985 ft	0.0000 in	0.000 ft
+D+L	1	0.9187 in	11.221 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.8051 in	11.142 ft	0.0000 in	0.000 ft
+0.60D	1	0.2785 in	10.985 ft	0.0000 in	0.000 ft
L Only	1	0.4549 in	11.378 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	3.031	3.716
Max Upward from Load Combinations	3.031	3.716
Max Upward from Load Cases	1.744	1.939
D Only	1.744	1.939
+D+L	3.031	3.716
+D+0.750L	2.709	3.272
+0.60D	1.047	1.163
L Only	1.286	1.777

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#11

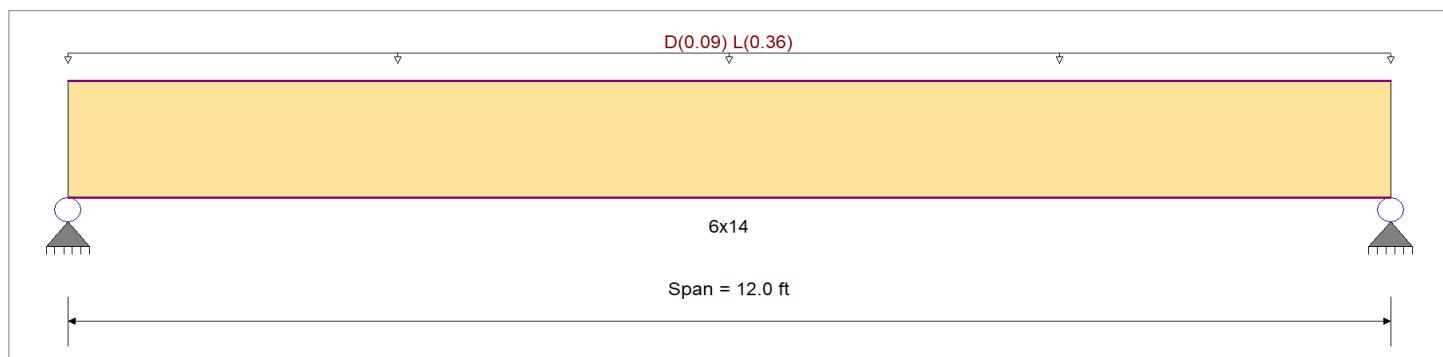
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	875 psi	E : Modulus of Elasticity	
Load Combination	IBC 2018	Fb -	875 psi	Ebend - xx	1300ksi
		Fc - Prll	600 psi	Eminbend - xx	470ksi
Wood Species	: Douglas Fir-Larch (North)	Fc - Perp	625 psi		
Wood Grade	: No.2	Fv	170 psi		
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Ft	425 psi	Density	30.59pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading
Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 6.0 ft, (DECK)

DESIGN SUMMARY

Design OK					
Maximum Bending Stress Ratio	=	0.872 1	Maximum Shear Stress Ratio	=	0.339 : 1
Section used for this span		6x14	Section used for this span		6x14
fb: Actual	=	602.21psi	fv: Actual	=	46.15 psi
F'b	=	690.90psi	F'v	=	136.00 psi
Load Combination		+D+L	Load Combination		+D+L
Location of maximum on span	=	6.000ft	Location of maximum on span	=	0.000 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
Maximum Deflection					
Max Downward Transient Deflection		0.121 in	Ratio =	1187 >= 360	Span: 1 : L Only
Max Upward Transient Deflection		0 in	Ratio =	0 < 360	n/a
Max Downward Total Deflection		0.157 in	Ratio =	917 >= 240	Span: 1 : +D+L
Max Upward Total Deflection		0 in	Ratio =	0 < 240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios						Moment Values				Shear Values						
		Span #	M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	M	fb	F'b	V	f _v	F'v	
D Only															0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.220	0.086	0.90	1.00	1.00	1.00	0.987	1.00	0.80	1.00	1.90	136.8	621.8	0.52	10.5	122.4	
+D+L															0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.872	0.339	1.00	1.00	1.00	1.00	0.987	1.00	0.80	1.00	8.38	602.2	690.9	2.28	46.2	136.0	
+D+0.750L															0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.563	0.219	1.25	1.00	1.00	1.00	0.987	1.00	0.80	1.00	6.76	485.8	863.6	1.84	37.2	170.0	
+0.60D															0.0	0.00	0.0	0.0
Length = 12.0 ft	1	0.074	0.029	1.60	1.00	1.00	1.00	0.987	1.00	0.80	1.00	1.14	82.1	1,105.4	0.31	6.3	217.6	

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#11

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.1570	6.044		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0356 in	6.044 ft	0.0000 in	0.000 ft
+D+L	1	0.1570 in	6.044 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.1266 in	6.044 ft	0.0000 in	0.000 ft
+0.60D	1	0.0214 in	6.044 ft	0.0000 in	0.000 ft
L Only	1	0.1213 in	6.044 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	2.795	2.795
Max Upward from Load Combinations	2.795	2.795
Max Upward from Load Cases	2.160	2.160
D Only	0.635	0.635
+D+L	2.795	2.795
+D+0.750L	2.255	2.255
+0.60D	0.381	0.381
L Only	2.160	2.160

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#12

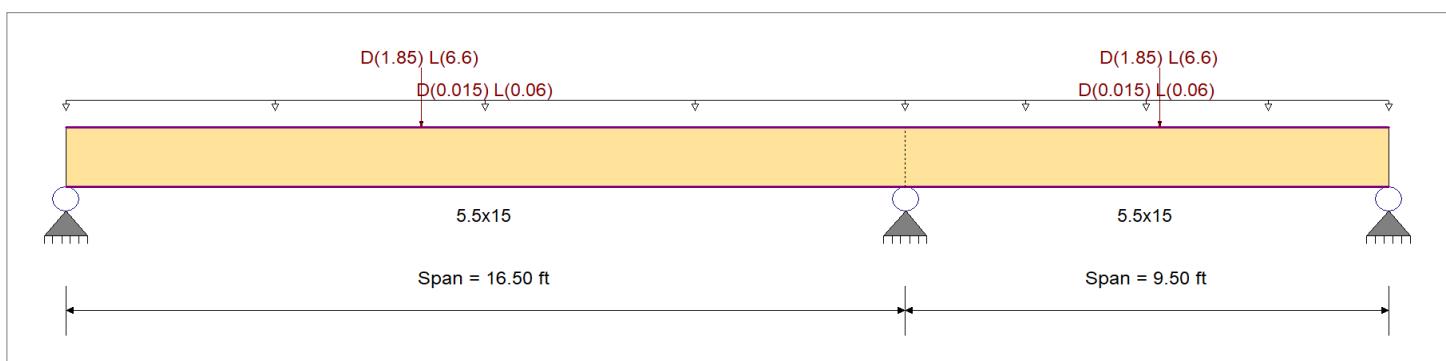
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	1,850.0 psi	Ebend - xx 1,800.0ksi
Wood Species	: DF/DF	Fc - Prll	1,650.0 psi	Eminbend - xx 950.0ksi
Wood Grade	: 24F-V4	Fc - Perp	650.0 psi	Ebend - yy 1,600.0ksi
Beam Bracing	: Beam is Fully Braced against lateral-torsional buckling	Fv	265.0 psi	Eminbend - yy 850.0ksi
		Ft	1,100.0 psi	Density 31.210pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Load for Span Number 1

Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 1.0 ft, (DECK)

Point Load : D = 1.850, L = 6.60 k @ 7.0 ft, (BM#8)

Load for Span Number 2

Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 1.0 ft, (DECK)

Point Load : D = 1.850, L = 6.60 k @ 5.0 ft, (BM#8)

DESIGN SUMMARY

Design OK			
Maximum Bending Stress Ratio	=	0.729 : 1	Maximum Shear Stress Ratio
Section used for this span	=	5.5x15	Section used for this span
fb: Actual	=	1,347.94psi	fv: Actual
F'b	=	1,850.00psi	F'v
Load Combination		+D+L	Load Combination
Location of maximum on span	=	0.000ft	Location of maximum on span
Span # where maximum occurs	=	Span # 2	Span # where maximum occurs
Maximum Deflection			
Max Downward Transient Deflection	0.229 in	Ratio = 864 >= 360	Span: 2 : L Only
Max Upward Transient Deflection	-0.006 in	Ratio = 17681 >= 360	Span: 2 : L Only
Max Downward Total Deflection	0.299 in	Ratio = 663 >= 240	Span: 2 : +D+L
Max Upward Total Deflection	-0.009 in	Ratio = 13172 >= 240	Span: 2 : +D+L

Maximum Forces & Stresses for Load Combinations

Load Combination	Max Stress Ratios										Moment Values				Shear Values			
	Segment Length	Span #	M	V	CD	CM	C _t	C _{Lx}	C _y	C _f	C _i	C _r	M	fb	F'b	V	fv	F'v
D Only															0.0	0.00	0.0	0.0
Length = 16.50 ft	1	0.169	0.119	0.90	1.00	1.00	1.00	0.995	1.00	1.00	1.00	1.00	6.25	363.9	2,148.7	1.56	28.4	238.5
Length = 9.50 ft	2	0.189	0.119	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	5.39	313.9	1,665.0	1.56	28.4	238.5
+D+L															0.0	0.00	0.0	0.0
Length = 16.50 ft	1	0.665	0.464	1.00	1.00	1.00	1.00	0.995	1.00	1.00	1.00	1.00	27.29	1,587.7	2,387.4	6.77	123.1	265.0
Length = 9.50 ft	2	0.729	0.464	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	23.17	1,347.9	1,850.0	6.77	123.1	265.0

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#12

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios								Moment Values			Shear Values					
			M	V	CD	CM	C _t	CLx	C _v	C _{fu}	C _i	C _r	M	f _b	F' _b	V	f _v	F' _v	
+D+0.750L					1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00				0.0	0.00	0.0	0.0
Length = 16.50 ft	1	0.430	0.300	1.25	1.00	1.00	1.00	0.995	1.00	1.00	1.00	1.00	22.03	1,281.7	2,984.3	5.47	99.4	331.3	
Length = 9.50 ft	2	0.471	0.300	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	18.72	1,089.4	2,312.5	5.47	99.4	331.3	
+0.60D					1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00				0.0	0.00	0.0	0.0
Length = 16.50 ft	1	0.057	0.040	1.60	1.00	1.00	1.00	0.995	1.00	1.00	1.00	1.00	3.75	218.3	3,819.9	0.94	17.0	424.0	
Length = 9.50 ft	2	0.064	0.040	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	3.24	188.3	2,960.0	0.94	17.0	424.0	

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.2986	7.190		0.0000	0.000
+D+L	2	0.0217	5.944	+D+L	-0.0087	1.274

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0696	in	7.190 ft	0.0000 in
D Only	2	0.0045	in	5.997 ft	-0.0022 in
+D+L	1	0.2986	in	7.190 ft	0.0000 in
+D+L	2	0.0217	in	5.944 ft	-0.0087 in
+D+0.750L	1	0.2414	in	7.190 ft	0.0000 in
+D+0.750L	2	0.0174	in	5.944 ft	-0.0070 in
+0.60D	1	0.0417	in	7.190 ft	0.0000 in
+0.60D	2	0.0027	in	5.997 ft	-0.0013 in
L Only	1	0.2291	in	7.190 ft	0.0000 in
L Only	2	0.0172	in	5.944 ft	-0.0064 in

Vertical Reactions

Load Combination	Support 1	Support 2	Support 3	Support notation : Far left is #1	Values in KIPS
Max Upward from all Load Conditions	4.227	12.638	2.450		
Max Upward from Load Combinations	4.227	12.638	2.450		
Max Upward from Load Cases	3.218	9.654	1.888		
D Only	1.009	2.983	0.562		
+D+L	4.227	12.638	2.450		
+D+0.750L	3.423	10.224	1.978		
+0.60D	0.606	1.790	0.337		
L Only	3.218	9.654	1.888		

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#13

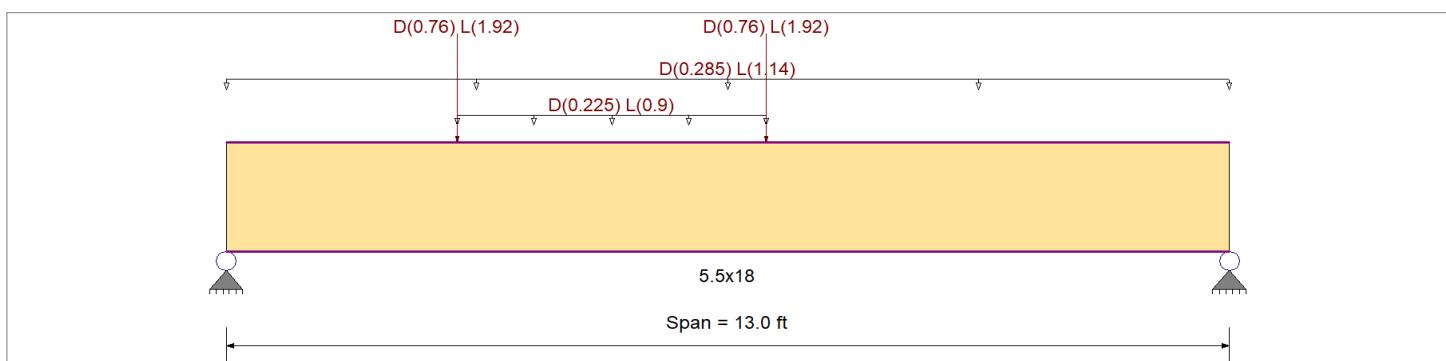
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2,400.0 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	1,850.0 psi	Ebend- xx 1,800.0ksi
Wood Species	DF/DF	Fc - Prll	1,650.0 psi	Eminbend - xx 950.0ksi
Wood Grade	24F-V4	Fc - Perp	650.0 psi	Ebend- yy 1,600.0ksi
		Fv	265.0 psi	Eminbend - yy 850.0ksi
		Ft	1,100.0 psi	Density 31.210pcf
Beam Bracing	Beam is Fully Braced against lateral-torsional buckling			



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Load for Span Number 1

Uniform Load : D = 0.0150, L = 0.060 ksf, Extent = 3.0 --> 7.0 ft, Tributary Width = 15.0 ft, (UPPER FLOOR)

Point Load : D = 0.760, L = 1.920 k @ 3.0 ft, (BM#9)

Point Load : D = 0.760, L = 1.920 k @ 7.0 ft, (BM#9)

Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 19.0 ft, (MAIN FLOOR)

DESIGN SUMMARY

Design OK			
Maximum Bending Stress Ratio	=	0.905 1	Maximum Shear Stress Ratio
Section used for this span		5.5x18	Section used for this span
fb: Actual	=	2,173.08psi	fv: Actual
F'b	=	2,400.00psi	F'v
Load Combination		+D+L	Load Combination
Location of maximum on span	=	6.263ft	Location of maximum on span
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs
Maximum Deflection			
Max Downward Transient Deflection	0.258 in	Ratio = 604 >=360	Span: 1 : L Only
Max Upward Transient Deflection	0 in	Ratio = 0 <360	n/a
Max Downward Total Deflection	0.333 in	Ratio = 468 >=240	Span: 1 : +D+L
Max Upward Total Deflection	0 in	Ratio = 0 <240	n/a

Maximum Forces & Stresses for Load Combinations

Load Combination	Max Stress Ratios								Moment Values				Shear Values					
	Segment Length	Span #	M	V	CD	CM	C _t	CLx	C _y	C _f	C _i	C _r	M	fb	F'b	V	fv	F'v
D Only															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.227	0.193	0.90	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	12.12	489.7	2,160.0	3.03	45.9	238.5
+D+L															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.905	0.763	1.00	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	53.78	2,173.1	2,400.0	13.34	202.2	265.0
+D+0.750L															0.0	0.00	0.0	0.0
Length = 13.0 ft	1	0.584	0.492	1.25	1.00	1.00	1.00	1.000	1.00	1.00	1.00	1.00	43.37	1,752.2	3,000.0	10.76	163.1	331.3
+0.60D															0.0	0.00	0.0	0.0

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#13

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Span #	Max Stress Ratios								Moment Values			Shear Values				
			M	V	CD	CM	C _t	CLx	C _v	C _f	C _i	C _r	M	f _b	F' _b	V	f _v	F' _v
Length = 13.0 ft		1	0.077	0.065	1.60	1.00	1.00	1.00	1.000	1.00	1.00	1.00	7.27	293.8	3,840.0	1.82	27.5	424.0

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.3331	6.405		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0750 in	6.405 ft	0.0000 in	0.000 ft
+D+L	1	0.3331 in	6.405 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.2686 in	6.405 ft	0.0000 in	0.000 ft
+0.60D	1	0.0450 in	6.405 ft	0.0000 in	0.000 ft
L Only	1	0.2581 in	6.405 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	15.470	13.194
Max Upward from Load Combinations	15.470	13.194
Max Upward from Load Cases	11.988	10.272
D Only	3.481	2.923
+D+L	15.470	13.194
+D+0.750L	12.473	10.626
+0.60D	2.089	1.754
L Only	11.988	10.272

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#14

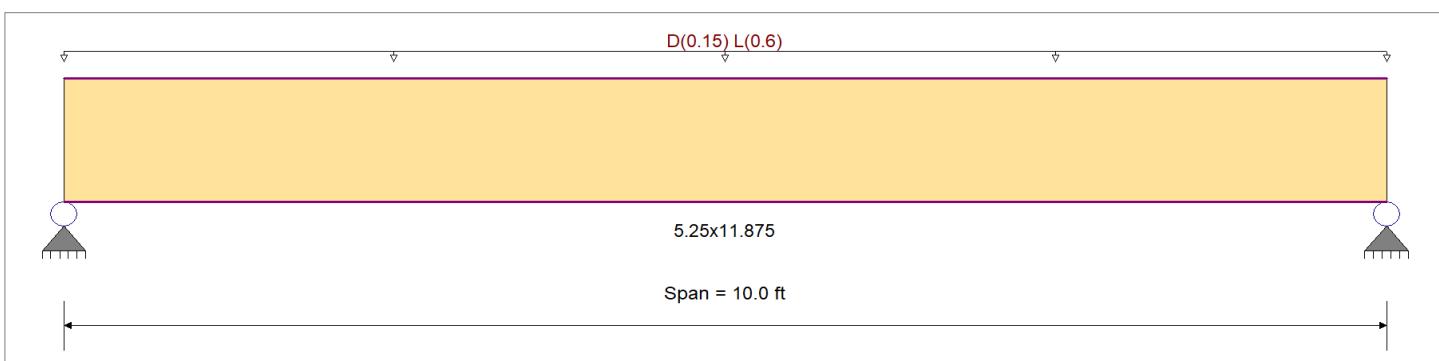
CODE REFERENCES

Calculations per NDS 2018, IBC 2021, ASCE 7-16

Load Combination Set : IBC 2018

Material Properties

Analysis Method :	Allowable Stress Design	Fb +	2900 psi	E : Modulus of Elasticity
Load Combination	IBC 2018	Fb -	2900 psi	Ebend - xx 2000ksi
		Fc - Prll	2900 psi	Eminbend - xx 1016.535ksi
Wood Species	iLevel Truss Joist	Fc - Perp	750 psi	
Wood Grade	Parallam PSL 2.0E	Fv	290 psi	
Beam Bracing	Beam is Fully Braced against lateral-torsional buckling	Ft	2025 psi	Density 45.07 pcf



Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Beam self weight calculated and added to loading

Uniform Load : D = 0.0150, L = 0.060 ksf, Tributary Width = 10.0 ft, (FLOOR)

DESIGN SUMMARY

Design OK					
Maximum Bending Stress Ratio	=	0.322 1	Maximum Shear Stress Ratio	=	0.256 : 1
Section used for this span		5.25x11.875	Section used for this span		5.25x11.875
fb: Actual	=	935.47psi	fv: Actual	=	74.33 psi
F'b	=	2,903.37psi	F'v	=	290.00 psi
Load Combination		+D+L	Load Combination		+D+L
Location of maximum on span	=	5.000ft	Location of maximum on span	=	0.000 ft
Span # where maximum occurs	=	Span # 1	Span # where maximum occurs	=	Span # 1
Maximum Deflection					
Max Downward Transient Deflection	0.093 in	Ratio = 1294 >= 360	Span: 1 : L Only		
Max Upward Transient Deflection	0 in	Ratio = 0 < 360	n/a		
Max Downward Total Deflection	0.119 in	Ratio = 1009 >= 240	Span: 1 : +D+L		
Max Upward Total Deflection	0 in	Ratio = 0 < 240	n/a		

Maximum Forces & Stresses for Load Combinations

Load Combination	Segment Length	Max Stress Ratios								Moment Values				Shear Values				
		Span #	M	V	CD	CM	C _t	CLx	C _F	C _f	C _i	C _r	M	fb	F'b	V	f _v	F'v
D Only															0.0	0.00	0.0	0.0
Length = 10.0 ft	1	0.079	0.063	0.90	1.00	1.00	1.00	1.001	1.00	1.00	1.00	1.00	2.12	206.1	2,613.0	0.68	16.4	261.0
+D+L															0.0	0.00	0.0	0.0
Length = 10.0 ft	1	0.322	0.256	1.00	1.00	1.00	1.00	1.001	1.00	1.00	1.00	1.00	9.62	935.5	2,903.4	3.09	74.3	290.0
+D+0.750L															0.0	0.00	0.0	0.0
Length = 10.0 ft	1	0.208	0.165	1.25	1.00	1.00	1.00	1.001	1.00	1.00	1.00	1.00	7.74	753.1	3,629.2	2.49	59.8	362.5
+0.60D															0.0	0.00	0.0	0.0
Length = 10.0 ft	1	0.027	0.021	1.60	1.00	1.00	1.00	1.001	1.00	1.00	1.00	1.00	1.27	123.6	4,645.4	0.41	9.8	464.0

Wood Beam

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: BM#14

Overall Maximum Deflections

Load Combination	Span	Max. "-" Defl	Location in Span	Load Combination	Max. "+" Defl	Location in Span
+D+L	1	0.1189	5.036		0.0000	0.000

Maximum Deflections for Load Combinations

Load Combination	Span	Max. Downward Defl	Location in Span	Max. Upward Defl	Location in Span
D Only	1	0.0262 in	5.036 ft	0.0000 in	0.000 ft
+D+L	1	0.1189 in	5.036 ft	0.0000 in	0.000 ft
+D+0.750L	1	0.0957 in	5.036 ft	0.0000 in	0.000 ft
+0.60D	1	0.0157 in	5.036 ft	0.0000 in	0.000 ft
L Only	1	0.0927 in	5.036 ft	0.0000 in	0.000 ft

Vertical Reactions

Support notation : Far left is #1

Values in KIPS

Load Combination	Support 1	Support 2
Max Upward from all Load Conditions	3.848	3.848
Max Upward from Load Combinations	3.848	3.848
Max Upward from Load Cases	3.000	3.000
D Only	0.848	0.848
+D+L	3.848	3.848
+D+0.750L	3.098	3.098
+0.60D	0.509	0.509
L Only	3.000	3.000

General Footing

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: FTNG#1

Code References

Calculations per ACI 318-19, IBC 2021, ASCE 7-16

Load Combinations Used : IBC 2018

General Information

Material Properties

f'c : Concrete 28 day strength	=	2.50 ksi
fy : Rebar Yield	=	40.0 ksi
Ec : Concrete Elastic Modulus	=	3,122.0 ksi
Concrete Density	=	145.0 pcf
φ Values	Flexure	= 0.90
	Shear	= 0.750

Analysis Settings

Min Steel % Bending Reinf.	=	
Min Allow % Temp Reinf.	=	0.00180
Min. Overturning Safety Factor	=	1.0 : 1
Min. Sliding Safety Factor	=	1.0 : 1
Add Ftg Wt for Soil Pressure	:	Yes
Use ftg wt for stability, moments & shears	:	Yes
Add Pedestal Wt for Soil Pressure	:	No
Use Pedestal wt for stability, mom & shear	:	No

Soil Design Values

Allowable Soil Bearing	=	1.50 ksf
Soil Density	=	110.0 pcf
Increase Bearing By Footing Weight	=	No
Soil Passive Resistance (for Sliding)	=	150.0 pcf
Soil/Concrete Friction Coeff.	=	0.250

Increases based on footing Depth

Footing base depth below soil surface	=	ft
Allow press. increase per foot of depth	=	ksf
when footing base is below	=	ft

Increases based on footing plan dimension

Allowable pressure increase per foot of depth	=	ksf
when max. length or width is greater than	=	ft
	=	ft

Dimensions

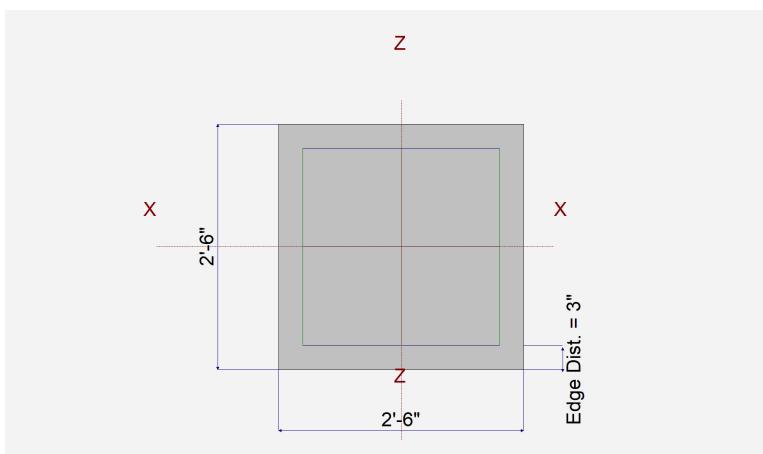
Width parallel to X-X Axis	=	2.50 ft
Length parallel to Z-Z Axis	=	2.50 ft
Footing Thickness	=	10.0 in

Pedestal dimensions...

px : parallel to X-X Axis	=	in
pz : parallel to Z-Z Axis	=	in
Height	=	in

Rebar Centerline to Edge of Concrete... at Bottom of footing

3.0 in



Reinforcing

Bars parallel to X-X Axis	=	3.0
Number of Bars	=	# 4

Bars parallel to Z-Z Axis	=	3.0
Number of Bars	=	# 4

Bandwidth Distribution Check (ACI 15.4.4.2)

Direction Requiring Closer Separation

n/a

Bars required within zone

n/a

Bars required on each side of zone

n/a

Applied Loads

	D	Lr	L	S	W	E	H
P : Column Load	=	1.50		6.20			k ksf
OB : Overburden	=						
M-xx	=						k-ft
M-zz	=						k-ft
V-x	=						k
V-z	=						k

General Footing

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: FTNG#1

DESIGN SUMMARY

Design OK

Min. Ratio	Item	Applied	Capacity	Governing Load Combination
PASS	0.9020 Soil Bearing	1.353 ksf	1.50 ksf	+D+L about Z-Z axis
PASS	n/a Overturning - X-X	0.0 k-ft	0.0 k-ft	No Overturning
PASS	n/a Overturning - Z-Z	0.0 k-ft	0.0 k-ft	No Overturning
PASS	n/a Sliding - X-X	0.0 k	0.0 k	No Sliding
PASS	n/a Sliding - Z-Z	0.0 k	0.0 k	No Sliding
PASS	n/a Uplift	0.0 k	0.0 k	No Uplift
PASS	0.2987 Z Flexure (+X)	1.465 k-ft/ft	4.904 k-ft/ft	+1.20D+1.60L
PASS	0.2987 Z Flexure (-X)	1.465 k-ft/ft	4.904 k-ft/ft	+1.20D+1.60L
PASS	0.2987 X Flexure (+Z)	1.465 k-ft/ft	4.904 k-ft/ft	+1.20D+1.60L
PASS	0.2987 X Flexure (-Z)	1.465 k-ft/ft	4.904 k-ft/ft	+1.20D+1.60L
PASS	0.2009 1-way Shear (+X)	15.069 psi	75.0 psi	+1.20D+1.60L
PASS	0.2009 1-way Shear (-X)	15.069 psi	75.0 psi	+1.20D+1.60L
PASS	0.2009 1-way Shear (+Z)	15.069 psi	75.0 psi	+1.20D+1.60L
PASS	0.2009 1-way Shear (-Z)	15.069 psi	75.0 psi	+1.20D+1.60L
PASS	0.3757 2-way Punching	56.352 psi	150.0 psi	+1.20D+1.60L

Detailed Results

Soil Bearing

Rotation Axis & Load Combination...	Gross Allowable	Xecc	Zecc (in)	Actual Soil Bearing Stress @ Location	Bottom, -Z	Top, +Z	Left, -X	Right, +X	Actual / Allow Ratio
X-X, D Only	1.50	n/a	0.0	0.3608	0.3608	n/a	n/a	n/a	0.241
X-X, +D+L	1.50	n/a	0.0	1.353	1.353	n/a	n/a	n/a	0.902
X-X, +D+0.750L	1.50	n/a	0.0	1.105	1.105	n/a	n/a	n/a	0.737
X-X, +0.60D	1.50	n/a	0.0	0.2165	0.2165	n/a	n/a	n/a	0.144
Z-Z, D Only	1.50	0.0	n/a	n/a	n/a	0.3608	0.3608	0.3608	0.241
Z-Z, +D+L	1.50	0.0	n/a	n/a	n/a	1.353	1.353	1.353	0.902
Z-Z, +D+0.750L	1.50	0.0	n/a	n/a	n/a	1.105	1.105	1.105	0.737
Z-Z, +0.60D	1.50	0.0	n/a	n/a	n/a	0.2165	0.2165	0.2165	0.144

Overturning Stability

Rotation Axis & Load Combination...	Overspin Moment	Resisting Moment	Stability Ratio	Status
Footing Has NO Overturning				All units k

Sliding Stability

Force Application Axis Load Combination...	Sliding Force	Resisting Force	Stability Ratio	Status
Footing Has NO Sliding				

Footing Flexure

Flexure Axis & Load Combination	Mu k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
X-X, +1.40D	0.2625	+Z	Bottom	0.2160	AsMin	0.240	4.904	OK
X-X, +1.40D	0.2625	-Z	Bottom	0.2160	AsMin	0.240	4.904	OK
X-X, +1.20D+1.60L	1.465	+Z	Bottom	0.2160	AsMin	0.240	4.904	OK
X-X, +1.20D+1.60L	1.465	-Z	Bottom	0.2160	AsMin	0.240	4.904	OK
X-X, +1.20D+0.50L	0.6125	+Z	Bottom	0.2160	AsMin	0.240	4.904	OK
X-X, +1.20D+0.50L	0.6125	-Z	Bottom	0.2160	AsMin	0.240	4.904	OK
X-X, +1.20D	0.2250	+Z	Bottom	0.2160	AsMin	0.240	4.904	OK
X-X, +1.20D	0.2250	-Z	Bottom	0.2160	AsMin	0.240	4.904	OK
X-X, +0.90D	0.1688	+Z	Bottom	0.2160	AsMin	0.240	4.904	OK
X-X, +0.90D	0.1688	-Z	Bottom	0.2160	AsMin	0.240	4.904	OK
Z-Z, +1.40D	0.2625	-X	Bottom	0.2160	AsMin	0.240	4.904	OK
Z-Z, +1.40D	0.2625	+X	Bottom	0.2160	AsMin	0.240	4.904	OK
Z-Z, +1.20D+1.60L	1.465	-X	Bottom	0.2160	AsMin	0.240	4.904	OK
Z-Z, +1.20D+1.60L	1.465	+X	Bottom	0.2160	AsMin	0.240	4.904	OK
Z-Z, +1.20D+0.50L	0.6125	-X	Bottom	0.2160	AsMin	0.240	4.904	OK
Z-Z, +1.20D+0.50L	0.6125	+X	Bottom	0.2160	AsMin	0.240	4.904	OK
Z-Z, +1.20D	0.2250	-X	Bottom	0.2160	AsMin	0.240	4.904	OK

General Footing

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: FTNG#1

Footing Flexure

Flexure Axis & Load Combination	Mu k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
Z-Z, +1.20D	0.2250	+X	Bottom	0.2160	AsMin	0.240	4.904	OK
Z-Z, +0.90D	0.1688	-X	Bottom	0.2160	AsMin	0.240	4.904	OK
Z-Z, +0.90D	0.1688	+X	Bottom	0.2160	AsMin	0.240	4.904	OK

One Way Shear

Load Combination...	Vu @ -X	Vu @ +X	Vu @ -Z	Vu @ +Z	Vu:Max	Phi Vn	Vu / Phi*Vn	Status
+1.40D	2.70 psi	75.00 psi	0.04	OK				
+1.20D+1.60L	15.07 psi	75.00 psi	0.20	OK				
+1.20D+0.50L	6.30 psi	75.00 psi	0.08	OK				
+1.20D	2.31 psi	75.00 psi	0.03	OK				
+0.90D	1.74 psi	75.00 psi	0.02	OK				

Two-Way "Punching" Shear

Load Combination...	Vu	Phi*Vn	Vu / Phi*Vn	Status
+1.40D	10.10 psi	150.00psi	0.06731	OK
+1.20D+1.60L	56.35 psi	150.00psi	0.3757	OK
+1.20D+0.50L	23.56 psi	150.00psi	0.1571	OK
+1.20D	8.66 psi	150.00psi	0.0577	OK
+0.90D	6.49 psi	150.00psi	0.04327	OK

All units k

General Footing

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: FTNG#2

Code References

Calculations per ACI 318-19, IBC 2021, ASCE 7-16

Load Combinations Used : IBC 2018

General Information

Material Properties

f'c : Concrete 28 day strength	=	2.50 ksi
fy : Rebar Yield	=	40.0 ksi
Ec : Concrete Elastic Modulus	=	3,122.0 ksi
Concrete Density	=	145.0 pcf
φ Values Flexure	=	0.90
Shear	=	0.750

Analysis Settings

Min Steel % Bending Reinf.	=	
Min Allow % Temp Reinf.	=	0.00180
Min. Overturning Safety Factor	=	1.0 : 1
Min. Sliding Safety Factor	=	1.0 : 1
Add Ftg Wt for Soil Pressure	:	Yes
Use ftg wt for stability, moments & shears	:	Yes
Add Pedestal Wt for Soil Pressure	:	No
Use Pedestal wt for stability, mom & shear	:	No

Soil Design Values

Allowable Soil Bearing	=	1.50 ksf
Soil Density	=	110.0 pcf
Increase Bearing By Footing Weight	=	No
Soil Passive Resistance (for Sliding)	=	150.0 pcf
Soil/Concrete Friction Coeff.	=	0.250

Increases based on footing Depth

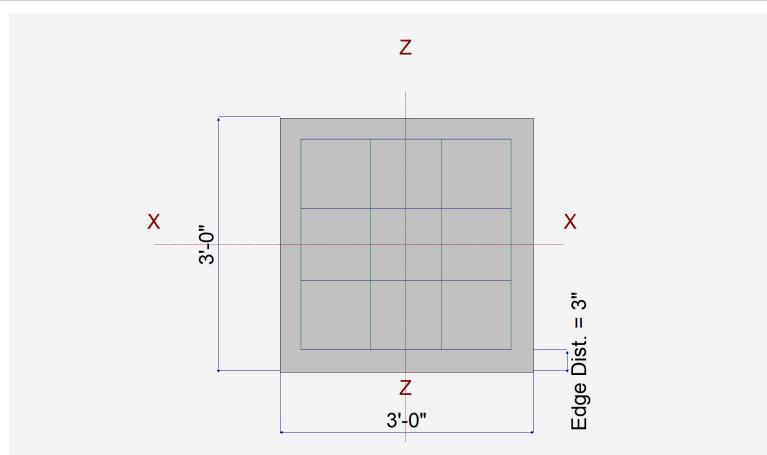
Footing base depth below soil surface	=	ft
Allow press. increase per foot of depth when footing base is below	=	ksf
	=	ft

Increases based on footing plan dimension

Allowable pressure increase per foot of depth when max. length or width is greater than	=	ksf
	=	ft

Dimensions

Width parallel to X-X Axis	=	3.0 ft
Length parallel to Z-Z Axis	=	3.0 ft
Footing Thickness	=	10.0 in



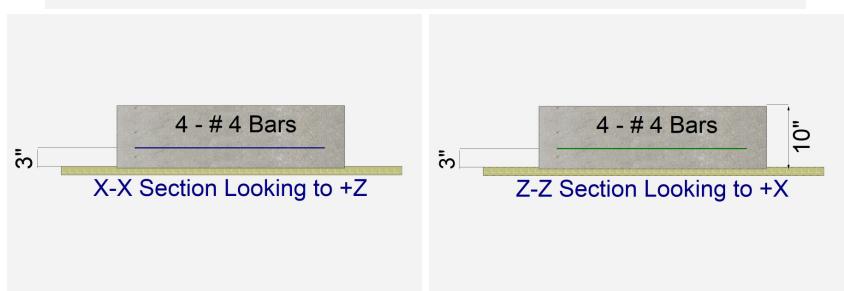
Reinforcing

Bars parallel to X-X Axis	=	
Number of Bars	=	4
Reinforcing Bar Size	=	# 4
Bars parallel to Z-Z Axis	=	
Number of Bars	=	4
Reinforcing Bar Size	=	# 4

Bandwidth Distribution Check (ACI 15.4.4.2)

Direction Requiring Closer Separation

# Bars required within zone	n/a
# Bars required on each side of zone	n/a



Applied Loads

	D	Lr	L	S	W	E	H
P : Column Load	=	2.750		6.60	3.310		k ksf
OB : Overburden	=						
M-xx	=						k-ft
M-zz	=						k-ft
V-x	=						k
V-z	=						k

General Footing

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: FTNG#2

DESIGN SUMMARY

Design OK

Min. Ratio	Item	Applied	Capacity	Governing Load Combination
PASS	0.8347	Soil Bearing	1.252 ksf	1.50 ksf +D+0.750L+0.750S about Z-Z axis
PASS	n/a	Overturning - X-X	0.0 k-ft	0.0 k-ft No Overturning
PASS	n/a	Overturning - Z-Z	0.0 k-ft	0.0 k-ft No Overturning
PASS	n/a	Sliding - X-X	0.0 k	0.0 k No Sliding
PASS	n/a	Sliding - Z-Z	0.0 k	0.0 k No Sliding
PASS	n/a	Uplift	0.0 k	0.0 k No Uplift
PASS	0.3570	Z Flexure (+X)	1.939 k-ft/ft	5.433 k-ft/ft +1.20D+1.60L+0.50S
PASS	0.3570	Z Flexure (-X)	1.939 k-ft/ft	5.433 k-ft/ft +1.20D+1.60L+0.50S
PASS	0.3570	X Flexure (+Z)	1.939 k-ft/ft	5.433 k-ft/ft +1.20D+1.60L+0.50S
PASS	0.3570	X Flexure (-Z)	1.939 k-ft/ft	5.433 k-ft/ft +1.20D+1.60L+0.50S
PASS	0.2545	1-way Shear (+X)	19.086 psi	75.0 psi +1.20D+1.60L+0.50S
PASS	0.2545	1-way Shear (-X)	19.086 psi	75.0 psi +1.20D+1.60L+0.50S
PASS	0.2545	1-way Shear (+Z)	19.086 psi	75.0 psi +1.20D+1.60L+0.50S
PASS	0.2545	1-way Shear (-Z)	19.086 psi	75.0 psi +1.20D+1.60L+0.50S
PASS	0.5066	2-way Punching	75.992 psi	150.0 psi +1.20D+1.60L+0.50S

Detailed Results

Soil Bearing

Rotation Axis & Load Combination...	Gross Allowable	Xecc (in)	Zecc (in)	Actual Soil Bearing Stress @ Location	Bottom, -Z	Top, +Z	Left, -X	Right, +X	Actual / Allow Ratio
X-X, D Only	1.50	n/a	0.0	0.4264	0.4264	n/a	n/a	n/a	0.284
X-X, +D+L	1.50	n/a	0.0	1.160	1.160	n/a	n/a	n/a	0.773
X-X, +D+S	1.50	n/a	0.0	0.7942	0.7942	n/a	n/a	n/a	0.530
X-X, +D+0.750L	1.50	n/a	0.0	0.9764	0.9764	n/a	n/a	n/a	0.651
X-X, +D+0.750L+0.750S	1.50	n/a	0.0	1.252	1.252	n/a	n/a	n/a	0.835
X-X, +0.60D	1.50	n/a	0.0	0.2558	0.2558	n/a	n/a	n/a	0.171
Z-Z, D Only	1.50	0.0	n/a	n/a	n/a	0.4264	0.4264	0.4264	0.284
Z-Z, +D+L	1.50	0.0	n/a	n/a	n/a	1.160	1.160	1.160	0.773
Z-Z, +D+S	1.50	0.0	n/a	n/a	n/a	0.7942	0.7942	0.7942	0.530
Z-Z, +D+0.750L	1.50	0.0	n/a	n/a	n/a	0.9764	0.9764	0.9764	0.651
Z-Z, +D+0.750L+0.750S	1.50	0.0	n/a	n/a	n/a	1.252	1.252	1.252	0.835
Z-Z, +0.60D	1.50	0.0	n/a	n/a	n/a	0.2558	0.2558	0.2558	0.171

Overturning Stability

Rotation Axis & Load Combination...	Overspin Moment	Resisting Moment	Stability Ratio	Status
Footing Has NO Overturning				All units k

Sliding Stability

Force Application Axis Load Combination...	Sliding Force	Resisting Force	Stability Ratio	Status
Footing Has NO Sliding				

Footing Flexure

Flexure Axis & Load Combination	Mu k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
X-X, +1.40D	0.4813	+Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.40D	0.4813	-Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D+1.60L	1.733	+Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D+1.60L	1.733	-Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D+1.60L+0.50S	1.939	+Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D+1.60L+0.50S	1.939	-Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D+0.50L	0.8250	+Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D+0.50L	0.8250	-Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D	0.4125	+Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D	0.4125	-Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D+0.50L+1.60S	1.487	+Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D+0.50L+1.60S	1.487	-Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D+1.60S	1.075	+Z	Bottom	0.2160	AsMin	0.2667	5.433	OK

General Footing

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: FTNG#2

Footing Flexure

Flexure Axis & Load Combination	Mu k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
X-X, +1.20D+1.60S	1.075	-Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D+0.50L+0.50S	1.032	+Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D+0.50L+0.50S	1.032	-Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D+0.50L+0.70S	1.115	+Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +1.20D+0.50L+0.70S	1.115	-Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +0.90D	0.3094	+Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
X-X, +0.90D	0.3094	-Z	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.40D	0.4813	-X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.40D	0.4813	+X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+1.60L	1.733	-X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+1.60L	1.733	+X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+1.60L+0.50S	1.939	-X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+1.60L+0.50S	1.939	+X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+0.50L	0.8250	-X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+0.50L	0.8250	+X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D	0.4125	-X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D	0.4125	+X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+0.50L+1.60S	1.487	-X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+0.50L+1.60S	1.487	+X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+1.60S	1.075	-X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+1.60S	1.075	+X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+0.50L+0.50S	1.032	-X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+0.50L+0.50S	1.032	+X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+0.50L+0.70S	1.115	-X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +1.20D+0.50L+0.70S	1.115	+X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +0.90D	0.3094	-X	Bottom	0.2160	AsMin	0.2667	5.433	OK
Z-Z, +0.90D	0.3094	+X	Bottom	0.2160	AsMin	0.2667	5.433	OK

One Way Shear

Load Combination...	Vu @ -X	Vu @ +X	Vu @ -Z	Vu @ +Z	Vu:Max	Phi Vn	Vu / Phi*Vn	Status
+1.40D	4.74 psi	75.00 psi	0.06	OK				
+1.20D+1.60L	17.05 psi	75.00 psi	0.23	OK				
+1.20D+1.60L+0.50S	19.09 psi	75.00 psi	0.25	OK				
+1.20D+0.50L	8.12 psi	75.00 psi	0.11	OK				
+1.20D	4.06 psi	75.00 psi	0.05	OK				
+1.20D+0.50L+1.60S	14.63 psi	75.00 psi	0.20	OK				
+1.20D+1.60S	10.57 psi	75.00 psi	0.14	OK				
+1.20D+0.50L+0.50S	10.16 psi	75.00 psi	0.14	OK				
+1.20D+0.50L+0.70S	10.97 psi	75.00 psi	0.15	OK				
+0.90D	3.05 psi	75.00 psi	0.04	OK				

Two-Way "Punching" Shear

Load Combination...	Vu	Phi*Vn	Vu / Phi*Vn	Status
+1.40D	18.86 psi	150.00psi	0.1257	OK
+1.20D+1.60L	67.89 psi	150.00psi	0.4526	OK
+1.20D+1.60L+0.50S	75.99 psi	150.00psi	0.5066	OK
+1.20D+0.50L	32.33 psi	150.00psi	0.2155	OK
+1.20D	16.16 psi	150.00psi	0.1078	OK
+1.20D+0.50L+1.60S	58.27 psi	150.00psi	0.3884	OK
+1.20D+1.60S	42.10 psi	150.00psi	0.2807	OK
+1.20D+0.50L+0.50S	40.43 psi	150.00psi	0.2696	OK
+1.20D+0.50L+0.70S	43.68 psi	150.00psi	0.2912	OK
+0.90D	12.12 psi	150.00psi	0.08082	OK

All units k

General Footing

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: FTNG#3

Code References

Calculations per ACI 318-19, IBC 2021, ASCE 7-16

Load Combinations Used : IBC 2018

General Information

Material Properties

f'c : Concrete 28 day strength	=	2.50 ksi
fy : Rebar Yield	=	40.0 ksi
Ec : Concrete Elastic Modulus	=	3,122.0 ksi
Concrete Density	=	145.0 pcf
φ Values Flexure	=	0.90
Shear	=	0.750

Analysis Settings

Min Steel % Bending Reinf.	=	
Min Allow % Temp Reinf.	=	0.00180
Min. Overturning Safety Factor	=	1.0 : 1
Min. Sliding Safety Factor	=	1.0 : 1
Add Ftg Wt for Soil Pressure	:	Yes
Use ftg wt for stability, moments & shears	:	Yes
Add Pedestal Wt for Soil Pressure	:	No
Use Pedestal wt for stability, mom & shear	:	No

Soil Design Values

Allowable Soil Bearing	=	1.50 ksf
Soil Density	=	110.0 pcf
Increase Bearing By Footing Weight	=	No
Soil Passive Resistance (for Sliding)	=	150.0 pcf
Soil/Concrete Friction Coeff.	=	0.250

Increases based on footing Depth

Footing base depth below soil surface	=	ft
Allow press. increase per foot of depth when footing base is below	=	ksf
	=	ft

Increases based on footing plan dimension

Allowable pressure increase per foot of depth when max. length or width is greater than	=	ksf
	=	ft

Dimensions

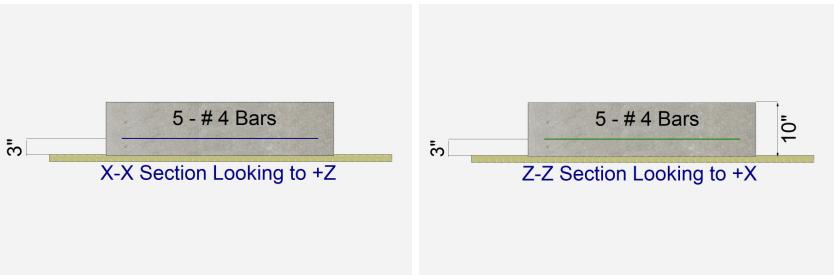
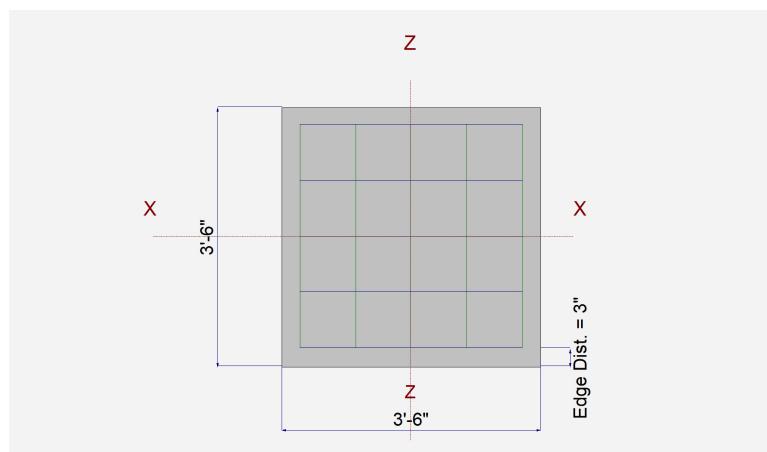
Width parallel to X-X Axis	=	3.50 ft
Length parallel to Z-Z Axis	=	3.50 ft
Footing Thickness	=	10.0 in

Pedestal dimensions...

px : parallel to X-X Axis	=	in
pz : parallel to Z-Z Axis	=	in
Height	=	in

Rebar Centerline to Edge of Concrete... at Bottom of footing

3.0 in



Reinforcing

Bars parallel to X-X Axis	=	
Number of Bars	=	5
Reinforcing Bar Size	=	# 4
Bars parallel to Z-Z Axis	=	
Number of Bars	=	5
Reinforcing Bar Size	=	# 4

Bandwidth Distribution Check (ACI 15.4.4.2)

Direction Requiring Closer Separation

n/a

Bars required within zone

n/a

Bars required on each side of zone

n/a

Applied Loads

	D	Lr	L	S	W	E	H
P : Column Load	=	3.0		9.650	0.0		k ksf
OB : Overburden	=						
M-xx	=						k-ft
M-zz	=						k-ft
V-x	=						k
V-z	=						k

General Footing

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: FTNG#3

DESIGN SUMMARY

Design OK

Min. Ratio	Item	Applied	Capacity	Governing Load Combination
PASS	0.7687 Soil Bearing	1.153 ksf	1.50 ksf	+D+L about Z-Z axis
PASS	n/a Overturning - X-X	0.0 k-ft	0.0 k-ft	No Overturning
PASS	n/a Overturning - Z-Z	0.0 k-ft	0.0 k-ft	No Overturning
PASS	n/a Sliding - X-X	0.0 k	0.0 k	No Sliding
PASS	n/a Sliding - Z-Z	0.0 k	0.0 k	No Sliding
PASS	n/a Uplift	0.0 k	0.0 k	No Uplift
PASS	0.4098 Z Flexure (+X)	2.380 k-ft/ft	5.808 k-ft/ft	+1.20D+1.60L
PASS	0.4098 Z Flexure (-X)	2.380 k-ft/ft	5.808 k-ft/ft	+1.20D+1.60L
PASS	0.4098 X Flexure (+Z)	2.380 k-ft/ft	5.808 k-ft/ft	+1.20D+1.60L
PASS	0.4098 X Flexure (-Z)	2.380 k-ft/ft	5.808 k-ft/ft	+1.20D+1.60L
PASS	0.2850 1-way Shear (+X)	21.371 psi	75.0 psi	+1.20D+1.60L
PASS	0.2850 1-way Shear (-X)	21.371 psi	75.0 psi	+1.20D+1.60L
PASS	0.2850 1-way Shear (+Z)	21.371 psi	75.0 psi	+1.20D+1.60L
PASS	0.2850 1-way Shear (-Z)	21.371 psi	75.0 psi	+1.20D+1.60L
PASS	0.6310 2-way Punching	94.656 psi	150.0 psi	+1.20D+1.60L

Detailed Results

Soil Bearing

Rotation Axis & Load Combination...	Gross Allowable	Xecc (in)	Zecc (in)	Actual Soil Bearing Stress @ Location	Bottom, -Z	Top, +Z	Left, -X	Right, +X	Actual / Allow Ratio
X-X, D Only	1.50	n/a	0.0	0.3657	0.3657	n/a	n/a	n/a	0.244
X-X, +D+L	1.50	n/a	0.0	1.153	1.153	n/a	n/a	n/a	0.769
X-X, +D+0.750L	1.50	n/a	0.0	0.9565	0.9565	n/a	n/a	n/a	0.638
X-X, +0.60D	1.50	n/a	0.0	0.2194	0.2194	n/a	n/a	n/a	0.146
Z-Z, D Only	1.50	0.0	n/a	n/a	n/a	0.3657	0.3657	0.3657	0.244
Z-Z, +D+L	1.50	0.0	n/a	n/a	n/a	1.153	1.153	1.153	0.769
Z-Z, +D+0.750L	1.50	0.0	n/a	n/a	n/a	0.9565	0.9565	0.9565	0.638
Z-Z, +0.60D	1.50	0.0	n/a	n/a	n/a	0.2194	0.2194	0.2194	0.146

Overturning Stability

Rotation Axis & Load Combination...	Overspin Moment	Resisting Moment	Stability Ratio	Status
Footing Has NO Overturning				All units k

Sliding Stability

Force Application Axis Load Combination...	Sliding Force	Resisting Force	Stability Ratio	Status
Footing Has NO Sliding				

Footing Flexure

Flexure Axis & Load Combination	Mu k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
X-X, +1.40D	0.5250	+Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.40D	0.5250	-Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.20D+1.60L	2.380	+Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.20D+1.60L	2.380	-Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.20D+0.50L	1.053	+Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.20D+0.50L	1.053	-Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.20D	0.450	+Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.20D	0.450	-Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +0.90D	0.3375	+Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +0.90D	0.3375	-Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.40D	0.5250	-X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.40D	0.5250	+X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.20D+1.60L	2.380	-X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.20D+1.60L	2.380	+X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.20D+0.50L	1.053	-X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.20D+0.50L	1.053	+X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.20D	0.450	-X	Bottom	0.2160	AsMin	0.2857	5.808	OK

General Footing

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: FTNG#3

Footing Flexure

Flexure Axis & Load Combination	Mu k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
Z-Z, +1.20D	0.450	+X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +0.90D	0.3375	-X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +0.90D	0.3375	+X	Bottom	0.2160	AsMin	0.2857	5.808	OK

One Way Shear

Load Combination...	Vu @ -X	Vu @ +X	Vu @ -Z	Vu @ +Z	Vu:Max	Phi Vn	Vu / Phi*Vn	Status
+1.40D	4.71 psi	75.00 psi	0.06	OK				
+1.20D+1.60L	21.37 psi	75.00 psi	0.29	OK				
+1.20D+0.50L	9.46 psi	75.00 psi	0.13	OK				
+1.20D	4.04 psi	75.00 psi	0.05	OK				
+0.90D	3.03 psi	75.00 psi	0.04	OK				

Two-Way "Punching" Shear

Load Combination...	Vu	Phi*Vn	Vu / Phi*Vn	Status
+1.40D	20.88 psi	150.00psi	0.1392	OK
+1.20D+1.60L	94.66 psi	150.00psi	0.631	OK
+1.20D+0.50L	41.88 psi	150.00psi	0.2792	OK
+1.20D	17.90 psi	150.00psi	0.1193	OK
+0.90D	13.42 psi	150.00psi	0.08949	OK

All units k

General Footing

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: FTNG#4

Code References

Calculations per ACI 318-19, IBC 2021, ASCE 7-16

Load Combinations Used : IBC 2018

General Information

Material Properties

f'c : Concrete 28 day strength	=	2.50 ksi
fy : Rebar Yield	=	40.0 ksi
Ec : Concrete Elastic Modulus	=	3,122.0 ksi
Concrete Density	=	145.0 pcf
φ Values Flexure	=	0.90
Shear	=	0.750

Analysis Settings

Min Steel % Bending Reinf.	=	
Min Allow % Temp Reinf.	=	0.00180
Min. Overturning Safety Factor	=	1.0 : 1
Min. Sliding Safety Factor	=	1.0 : 1
Add Ftg Wt for Soil Pressure	:	Yes
Use ftg wt for stability, moments & shears	:	Yes
Add Pedestal Wt for Soil Pressure	:	No
Use Pedestal wt for stability, mom & shear	:	No

Soil Design Values

Allowable Soil Bearing	=	1.50 ksf
Soil Density	=	110.0 pcf
Increase Bearing By Footing Weight	=	No
Soil Passive Resistance (for Sliding)	=	150.0 pcf
Soil/Concrete Friction Coeff.	=	0.250

Increases based on footing Depth

Footing base depth below soil surface	=	ft
Allow press. increase per foot of depth when footing base is below	=	ksf
	=	ft

Increases based on footing plan dimension

Allowable pressure increase per foot of depth when max. length or width is greater than	=	ksf
	=	ft

Dimensions

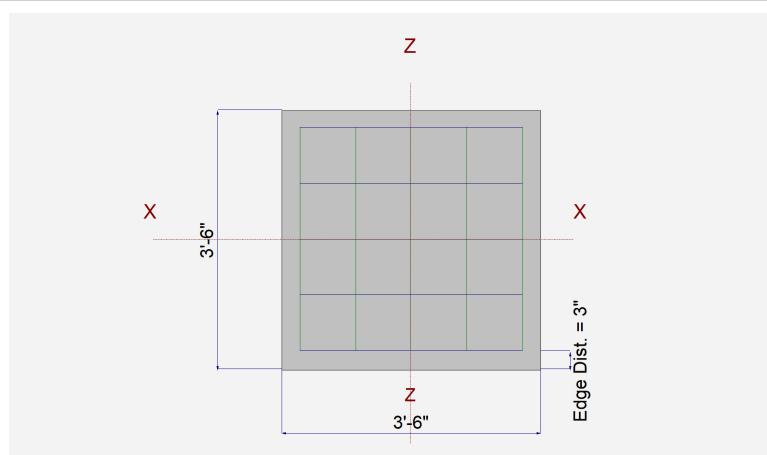
Width parallel to X-X Axis	=	3.50 ft
Length parallel to Z-Z Axis	=	3.50 ft
Footing Thickness	=	10.0 in

Pedestal dimensions...

px : parallel to X-X Axis	=	in
pz : parallel to Z-Z Axis	=	in
Height	=	in

Rebar Centerline to Edge of Concrete... at Bottom of footing

3.0 in

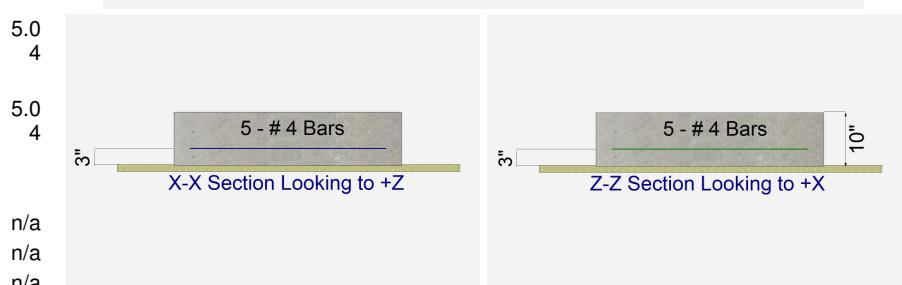


Reinforcing

Bars parallel to X-X Axis	=	
Number of Bars	=	5.0
Reinforcing Bar Size	=	# 4
Bars parallel to Z-Z Axis	=	
Number of Bars	=	5.0
Reinforcing Bar Size	=	# 4

Bandwidth Distribution Check (ACI 15.4.4.2)

Direction Requiring Closer Separation



# Bars required within zone	n/a
# Bars required on each side of zone	n/a

Applied Loads

	D	Lr	L	S	W	E	H
P : Column Load	=	3.480					k ksf
OB : Overburden	=		12.0				
M-xx	=						k-ft
M-zz	=						k-ft
V-x	=						k
V-z	=						k

General Footing

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: FTNG#4

DESIGN SUMMARY

Design OK

Min. Ratio	Item	Applied	Capacity	Governing Load Combination
PASS	0.9233	Soil Bearing	1.385 ksf	1.50 ksf +D+L about Z-Z axis
PASS	n/a	Overspinning - X-X	0.0 k-ft	0.0 k-ft No Overspinning
PASS	n/a	Overspinning - Z-Z	0.0 k-ft	0.0 k-ft No Overspinning
PASS	n/a	Sliding - X-X	0.0 k	0.0 k No Sliding
PASS	n/a	Sliding - Z-Z	0.0 k	0.0 k No Sliding
PASS	n/a	Uplift	0.0 k	0.0 k No Uplift
PASS	0.5031	Z Flexure (+X)	2.922 k-ft/ft	5.808 k-ft/ft +1.20D+1.60L
PASS	0.5031	Z Flexure (-X)	2.922 k-ft/ft	5.808 k-ft/ft +1.20D+1.60L
PASS	0.5031	X Flexure (+Z)	2.922 k-ft/ft	5.808 k-ft/ft +1.20D+1.60L
PASS	0.5031	X Flexure (-Z)	2.922 k-ft/ft	5.808 k-ft/ft +1.20D+1.60L
PASS	0.3498	1-way Shear (+X)	26.238 psi	75.0 psi +1.20D+1.60L
PASS	0.3498	1-way Shear (-X)	26.238 psi	75.0 psi +1.20D+1.60L
PASS	0.3498	1-way Shear (+Z)	26.238 psi	75.0 psi +1.20D+1.60L
PASS	0.3498	1-way Shear (-Z)	26.238 psi	75.0 psi +1.20D+1.60L
PASS	0.7747	2-way Punching	116.212 psi	150.0 psi +1.20D+1.60L

Detailed Results

Soil Bearing

Rotation Axis & Load Combination...	Gross Allowable	Xecc (in)	Zecc (in)	Actual Soil Bearing Stress @ Location	Bottom, -Z	Top, +Z	Left, -X	Right, +X	Actual / Allow Ratio
X-X, D Only	1.50	n/a	0.0	0.4049	0.4049	n/a	n/a	n/a	0.270
X-X, +D+L	1.50	n/a	0.0	1.385	1.385	n/a	n/a	n/a	0.923
X-X, +D+0.750L	1.50	n/a	0.0	1.140	1.140	n/a	n/a	n/a	0.760
X-X, +0.60D	1.50	n/a	0.0	0.2429	0.2429	n/a	n/a	n/a	0.162
Z-Z, D Only	1.50	0.0	n/a	n/a	n/a	0.4049	0.4049	0.4049	0.270
Z-Z, +D+L	1.50	0.0	n/a	n/a	n/a	1.385	1.385	1.385	0.923
Z-Z, +D+0.750L	1.50	0.0	n/a	n/a	n/a	1.140	1.140	1.140	0.760
Z-Z, +0.60D	1.50	0.0	n/a	n/a	n/a	0.2429	0.2429	0.2429	0.162

Overturning Stability

Rotation Axis & Load Combination...	Overspinning Moment	Resisting Moment	Stability Ratio	Status
Footing Has NO Overturning	All units k			

Sliding Stability

Force Application Axis Load Combination...	Sliding Force	Resisting Force	Stability Ratio	Status
Footing Has NO Sliding	All units k			

Footing Flexure

Flexure Axis & Load Combination	Mu k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
X-X, +1.40D	0.6090	+Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.40D	0.6090	-Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.20D+1.60L	2.922	+Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.20D+1.60L	2.922	-Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.20D+0.50L	1.272	+Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.20D+0.50L	1.272	-Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.20D	0.5220	+Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +1.20D	0.5220	-Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +0.90D	0.3915	+Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
X-X, +0.90D	0.3915	-Z	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.40D	0.6090	-X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.40D	0.6090	+X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.20D+1.60L	2.922	-X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.20D+1.60L	2.922	+X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.20D+0.50L	1.272	-X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.20D+0.50L	1.272	+X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +1.20D	0.5220	-X	Bottom	0.2160	AsMin	0.2857	5.808	OK

General Footing

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: FTNG#4

Footing Flexure

Flexure Axis & Load Combination	Mu k-ft	Side	Tension Surface	As Req'd in^2	Gvrn. As in^2	Actual As in^2	Phi*Mn k-ft	Status
Z-Z, +1.20D	0.5220	+X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +0.90D	0.3915	-X	Bottom	0.2160	AsMin	0.2857	5.808	OK
Z-Z, +0.90D	0.3915	+X	Bottom	0.2160	AsMin	0.2857	5.808	OK

One Way Shear

Load Combination...	Vu @ -X	Vu @ +X	Vu @ -Z	Vu @ +Z	Vu:Max	Phi Vn	Vu / Phi*Vn	Status
+1.40D	5.47 psi	75.00 psi	0.07	OK				
+1.20D+1.60L	26.24 psi	75.00 psi	0.35	OK				
+1.20D+0.50L	11.42 psi	75.00 psi	0.15	OK				
+1.20D	4.69 psi	75.00 psi	0.06	OK				
+0.90D	3.52 psi	75.00 psi	0.05	OK				

Two-Way "Punching" Shear

Load Combination...	Vu	Phi*Vn	Vu / Phi*Vn	Status
+1.40D	24.22 psi	150.00psi	0.1615	OK
+1.20D+1.60L	116.21 psi	150.00psi	0.7747	OK
+1.20D+0.50L	50.59 psi	150.00psi	0.3373	OK
+1.20D	20.76 psi	150.00psi	0.1384	OK
+0.90D	15.57 psi	150.00psi	0.1038	OK

All units k

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft wall

Code Reference:

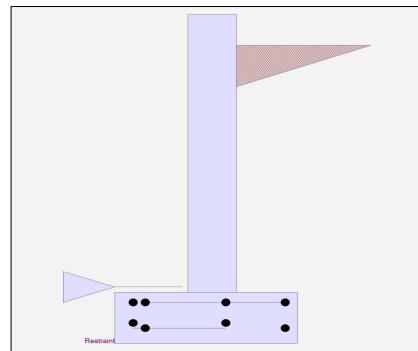
Calculations per IBC 2021 1807.3, ASCE 7-16

Criteria

Retained Height	=	4.00 ft
Wall height above soil	=	0.50 ft
Slope Behind Wall	=	0.00
Height of Soil over Toe	=	0.00 in
Water table above bottom of footing	=	0.0 ft

Soil Data

Allow Soil Bearing	=	1,500.0 psf
Equivalent Fluid Pressure Method	=	
Active Heel Pressure	=	35.0 psf/ft
	=	
Passive Pressure	=	150.0 psf/ft
Soil Density, Heel	=	110.00 pcf
Soil Density, Toe	=	110.00 pcf
Footing Soil Friction	=	0.400
Soil height to ignore for passive pressure	=	12.00 in



Surcharge Loads

Surcharge Over Heel	=	0.0 psf
Used To Resist Sliding & Overturning	=	
Surcharge Over Toe	=	0.0
Used for Sliding & Overturning	=	

Axial Load Applied to Stem

Axial Dead Load	=	0.0 lbs
Axial Live Load	=	0.0 lbs
Axial Load Eccentricity	=	0.0 in

Lateral Load Applied to Stem

Lateral Load	=	0.0 #/ft
...Height to Top	=	0.00 ft
...Height to Bottom	=	0.00 ft
Load Type	=	Wind (W) (Service Level)
Wind on Exposed Stem	=	0.0 psf (Strength Level)

Adjacent Footing Load

Adjacent Footing Load	=	0.0 lbs
Footing Width	=	0.00 ft
Eccentricity	=	0.00 in
Wall to Ftg CL Dist	=	0.00 ft
Footing Type	=	Spread Footing
Base Above/Below Soil at Back of Wall	=	0.0 ft
Poisson's Ratio	=	0.300

Earth Pressure Seismic Load

Method : Uniform		
Multiplier Used	=	10.000

(Multiplier used on soil density)

Uniform Seismic Force = 48.333
Total Seismic Force = 233.611

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft wall

Design Summary

Wall Stability Ratios		
Overturning	=	1.66 OK Slab Resists All Sliding !
Global Stability		
Global Stability	=	1.97
Total Bearing Load		
Total Bearing Load	=	1,129 lbs ...resultant ecc. = 7.55 in
Eccentricity outside middle third		
Soil Pressure @ Toe	=	1,213 psf OK
Soil Pressure @ Heel	=	0 psf OK
Allowable	=	1,500 psf
Soil Pressure Less Than Allowable		
ACI Factored @ Toe	=	1,698 psf
ACI Factored @ Heel	=	0 psf
Footing Shear @ Toe	=	7.9 psi OK
Footing Shear @ Heel	=	6.1 psi OK
Allowable	=	75.0 psi
Sliding Calcs		
Lateral Sliding Force	=	572.3 lbs

Vertical component of active lateral soil pressure IS
NOT considered in the calculation of soil bearing

Load Factors

Building Code	
Dead Load	1.200
Live Load	1.600
Earth, H	1.600
Wind, W	1.600
Seismic, E	1.000

Stem Construction

Design Height Above Ftg	Bottom
ft =	Stem OK 0.00
Wall Material Above "Ht"	= Concrete
Design Method	= SD SD SD
Thickness	= 8.00
Rebar Size	= # 4
Rebar Spacing	= 12.00
Rebar Placed at	= Edge

Design Data

fb/FB + fa/Fa	=	0.269
---------------	---	-------

Total Force @ Section

Service Level	lbs =
Strength Level	lbs = 641.3

Moment....Actual

Service Level	ft-# =
Strength Level	ft-# = 984.0
Moment.....Allowable	= 3,655.6

Shear.....Actual

Service Level	psi =
Strength Level	psi = 8.6
Shear.....Allowable	psi = 41.6
Anet (Masonry)	in2 =
Wall Weight	psf = 100.0
Rebar Depth 'd'	in = 6.25

Masonry Data

f'm	psi =
Fs	psi =
Solid Grouting	=
Modular Ratio 'n'	=
Equiv. Solid Thick.	=
Masonry Block Type	=
Masonry Design Method	= ASD

Concrete Data

f'c	psi = 2,500.0
Fy	psi = 40,000.0

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft wall

Concrete Stem Rebar Area Details

	<u>Vertical Reinforcing</u>	<u>Horizontal Reinforcing</u>
Bottom Stem		
As (based on applied moment) :	0.0553 in ² /ft	
0.0018bh : 0.0018(12)(8) :	0.1728 in ² /ft	
	=====	Horizontal Reinforcing Options :
Required Area :	0.1728 in ² /ft	One layer of : #4@ 13.89 in
Provided Area :	0.2 in ² /ft	Two layers of : #4@ 27.78 in
Maximum Area :	1.27 in ² /ft	#5@ 21.53 in #5@ 43.06 in
		#6@ 30.56 in #6@ 61.11 in

Footing Data

Toe Width	=	1.00 ft
Heel Width	=	1.50
Total Footing Width	=	2.50
Footing Thickness	=	10.00 in
Key Width	=	0.00 in
Key Depth	=	0.00 in
Key Distance from Toe	=	0.00 ft
f'c = 2,500 psi	Fy = 40,000 psi	
Footing Concrete Density	=	150.00 pcf
Min. As %	=	0.0018
Cover @ Top	2.00	@ Btm.= 3.00 in

Footing Design Results

	<u>Toe</u>	<u>Heel</u>	
Factored Pressure	= 1,698	0 psf	
Mu' : Upward	= 697	1 ft-#	
Mu' : Downward	= 75	235 ft-#	
Mu: Design	= 622 OK	234 ft-#	OK
phiMn	= 4,264	4,912 ft-#	
Actual 1-Way Shear	= 7.87	6.09 psi	
Allow 1-Way Shear	= 75.00	75.00 psi	
Toe Reinforcing	= # 4 @ 11.11 in		
Heel Reinforcing	= # 4 @ 11.11 in		
Key Reinforcing	= None Spec'd		
Footing Torsion, Tu	= 0.00 ft-lbs		
Footing Allow. Torsion, phi Tu	= 0.00 ft-lbs		

If torsion exceeds allowable, provide supplemental design for footing torsion.

Other Acceptable Sizes & Spacings

Toe: #4@ 11.11 in, #5@ 17.22 in, #6@ 24.44 in, #7@ 33.33 in, #8@ 43.88 in, #9@ 55.55 in, #10@ 70.55 in

Heel: #4@ 11.11 in, #5@ 17.22 in, #6@ 24.44 in, #7@ 33.33 in, #8@ 43.88 in, #9@ 55.55 in, #10@ 70.55 in

Key: No key defined

Min footing T&S reinf Area	0.54 in ²
Min footing T&S reinf Area per foot	0.22 in ² /ft
If one layer of horizontal bars:	If two layers of horizontal bars:
#4@ 11.11 in	#4@ 22.22 in
#5@ 17.22 in	#5@ 34.44 in
#6@ 24.44 in	#6@ 48.89 in

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft wall

Summary of Overturning & Resisting Forces & Moments

ItemOVERTURNING.....		RESISTING.....		
	Force lbs	Distance ft	Moment ft-#	Force lbs	Distance ft	Moment ft-#
HL Act Pres (ab water tbl)	408.8	1.61	658.7	Soil Over HL (ab. water tbl)	366.7	2.08
HL Act Pres (be water tbl)				Soil Over HL (bel. water tbl)		2.08
Hydrostatic Force				Water Table		763.9
Buoyant Force	=			Sloped Soil Over Heel	=	
Surcharge over Heel	=			Surcharge Over Heel	=	
Surcharge Over Toe	=			Adjacent Footing Load	=	
Adjacent Footing Load	=			Axial Dead Load on Stem	=	
Added Lateral Load	=			* Axial Live Load on Stem	=	
Load @ Stem Above Soil	=			Soil Over Toe	=	
Seismic Earth Load	=	163.5	2.42	Surcharge Over Toe	=	
	=			Stem Weight(s)	=	450.0
				Earth @ Stem Transitions	=	1.33
Total	=	572.3	O.T.M. =	Footing Weight	=	600.0
				Key Weight	=	312.5
				Vert. Component	=	390.6
				Total =	1,129.2 lbs R.M.=	1,754.5

Resisting/Overturning Ratio = **1.66**
Vertical Loads used for Soil Pressure = 1,129.2 lbs

If seismic is included, the OTM and sliding ratios may be 1.1 per section 1807.2.3 of IBC.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

* Axial live load NOT included in total displayed, or used for overturning resistance, but is included for soil pressure calculation.

Tilt

Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus 250.0 pci

Horizontal Defl @ Top of Wall (approximate only) 0.061 in

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft wall

Rebar Lap & Embedment Lengths Information

Stem Design Segment: Bottom

Stem Design Height: 0.00 ft above top of footing

Lap Splice length for #4 bar specified in this stem design segment (25.4.2.4a) = 15.60 in
Development length for #4 bar specified in this stem design segment = 12.00 in

Hooked embedment length into footing for #4 bar specified in this stem design segment = 0.00 in
As Provided = 0.2000 in²/ft
As Required = 0.1728 in²/ft

Cantilevered Retaining Wall

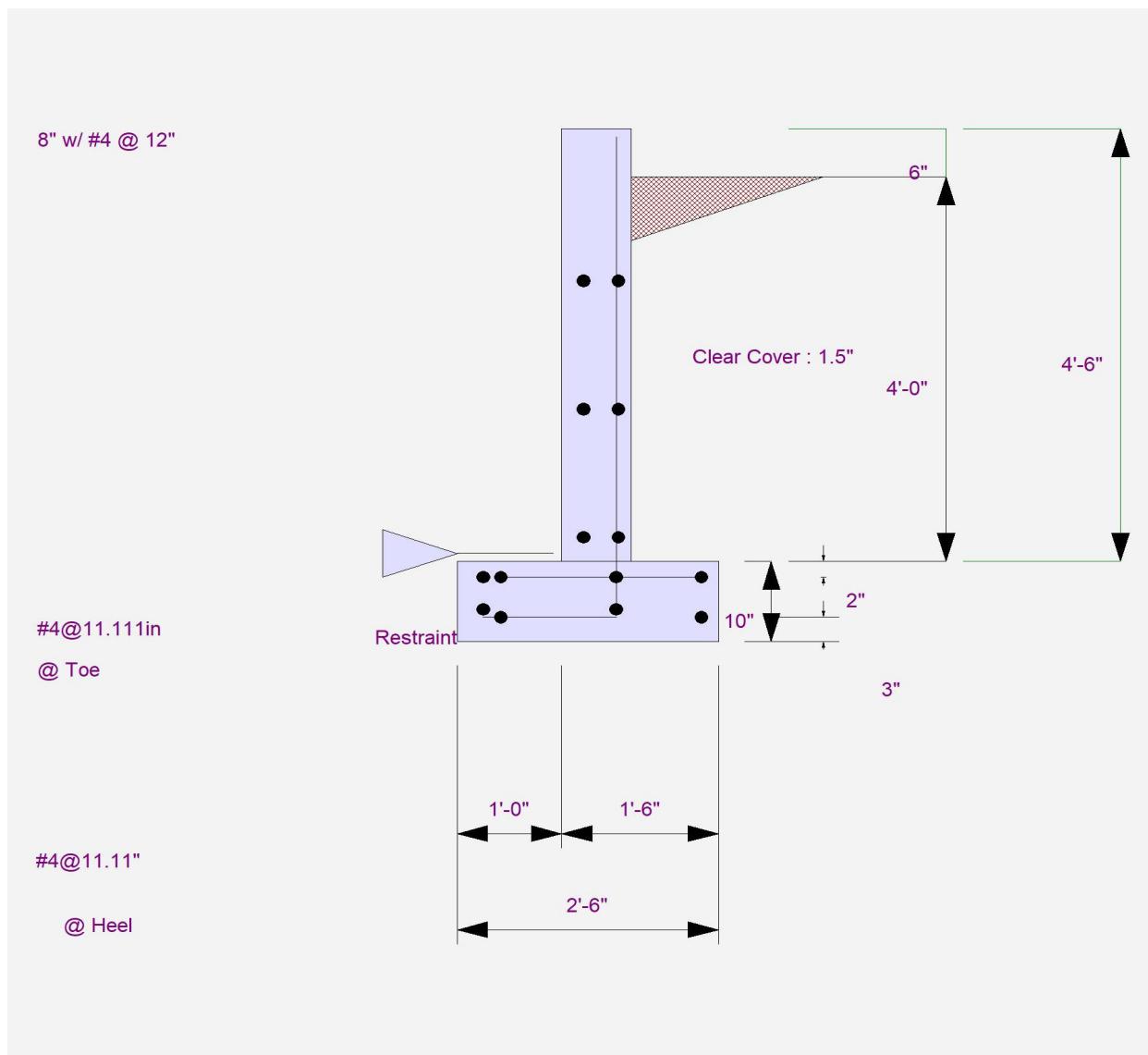
Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft wall



Cantilevered Retaining Wall

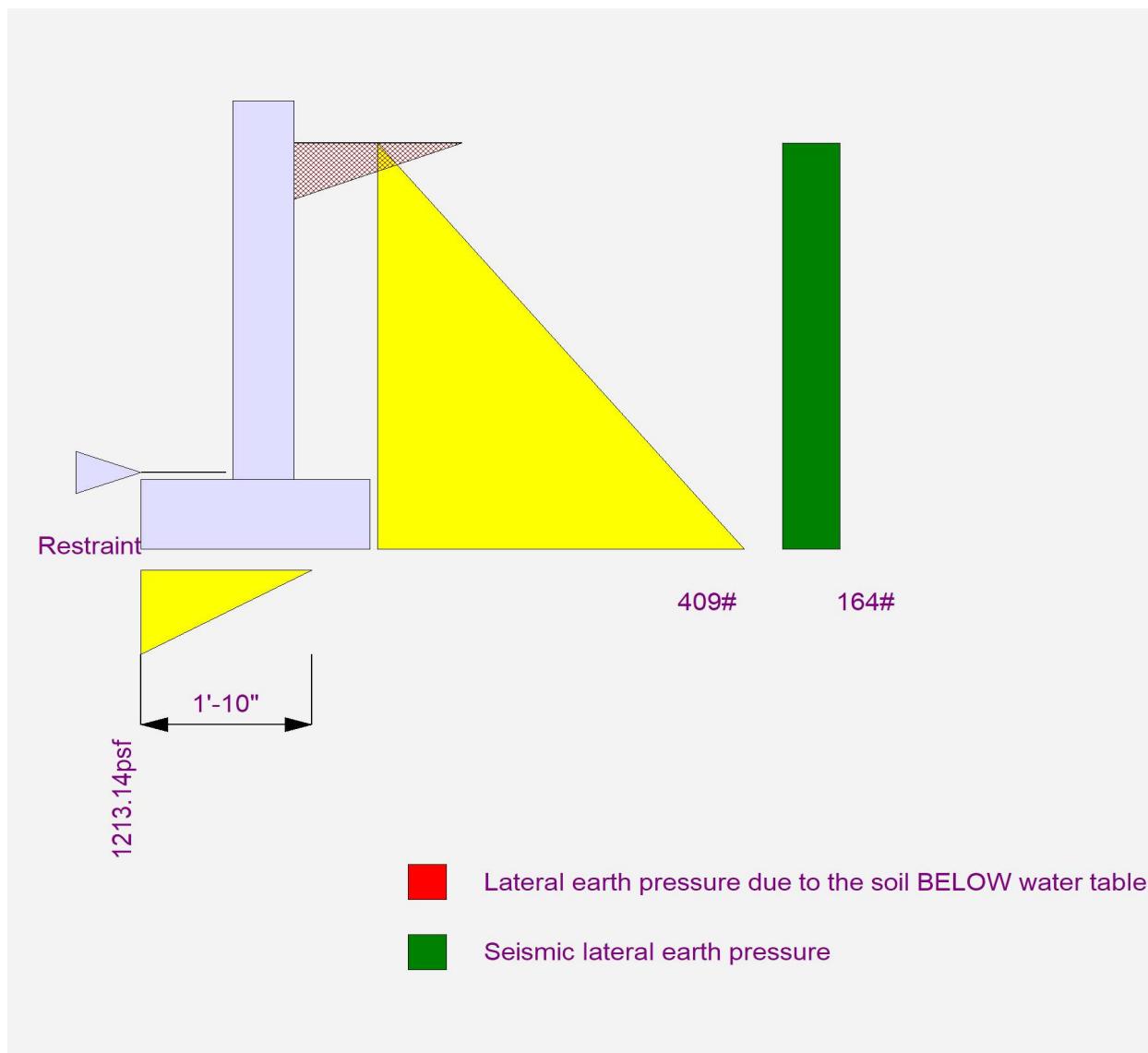
Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft wall



Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft wall

Code Reference:

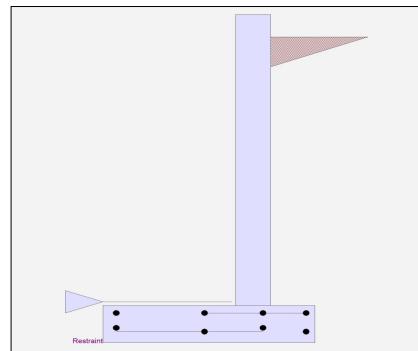
Calculations per IBC 2021 1807.3, ASCE 7-16

Criteria

Retained Height	=	6.00 ft
Wall height above soil	=	0.50 ft
Slope Behind Wall	=	0.00
Height of Soil over Toe	=	0.00 in
Water table above bottom of footing	=	0.0 ft

Soil Data

Allow Soil Bearing	=	1,500.0 psf
Equivalent Fluid Pressure Method	=	
Active Heel Pressure	=	35.0 psf/ft
	=	
Passive Pressure	=	150.0 psf/ft
Soil Density, Heel	=	110.00 pcf
Soil Density, Toe	=	110.00 pcf
Footing Soil Friction	=	0.400
Soil height to ignore for passive pressure	=	12.00 in



Surcharge Loads

Surcharge Over Heel	=	0.0 psf
Used To Resist Sliding & Overturning	=	
Surcharge Over Toe	=	0.0
Used for Sliding & Overturning	=	

Axial Load Applied to Stem

Axial Dead Load	=	0.0 lbs
Axial Live Load	=	0.0 lbs
Axial Load Eccentricity	=	0.0 in

Lateral Load Applied to Stem

Lateral Load	=	0.0 #/ft
...Height to Top	=	0.00 ft
...Height to Bottom	=	0.00 ft
Load Type	=	Wind (W) (Service Level)
Wind on Exposed Stem	=	0.0 psf (Strength Level)

Adjacent Footing Load

Adjacent Footing Load	=	0.0 lbs
Footing Width	=	0.00 ft
Eccentricity	=	0.00 in
Wall to Ftg CL Dist	=	0.00 ft
Footing Type	=	Spread Footing
Base Above/Below Soil at Back of Wall	=	0.0 ft
Poisson's Ratio	=	0.300

Earth Pressure Seismic Load

Method : Uniform	
Multiplier Used	= 10.000
(Multiplier used on soil density)	

Uniform Seismic Force = 68.333
Total Seismic Force = 466.944

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft wall

Design Summary

Wall Stability Ratios

Overturning	=	1.62	OK
Slab Resists All Sliding !			
Global Stability	=	1.50	
Total Bearing Load	=	1,700	lbs
...resultant ecc.	=	11.05	in
Eccentricity outside middle third			
Soil Pressure @ Toe	=	1,050	psf OK
Soil Pressure @ Heel	=	0	psf OK
Allowable	=	1,500	psf
Soil Pressure Less Than Allowable			
ACI Factored @ Toe	=	1,470	psf
ACI Factored @ Heel	=	0	psf
Footing Shear @ Toe	=	22.0	psi OK
Footing Shear @ Heel	=	8.7	psi OK
Allowable	=	75.0	psi

Sliding Calcs

Lateral Sliding Force	=	1,144.0	lbs
-----------------------	---	---------	-----

Vertical component of active lateral soil pressure IS
NOT considered in the calculation of soil bearing

Load Factors

Building Code	
Dead Load	1.200
Live Load	1.600
Earth, H	1.600
Wind, W	1.600
Seismic, E	1.000

Stem Construction

Design Height Above Ftg

ft =	0.00
Wall Material Above "Ht"	= Concrete
Design Method	= SD
Thickness	= 8.00
Rebar Size	= # 4
Rebar Spacing	= 8.00
Rebar Placed at	= Edge

Design Data

fb/FB + fa/Fa	=	0.599
---------------	---	-------

Total Force @ Section

Service Level	lbs =	
Strength Level	lbs =	1,418.0

Moment....Actual

Service Level	ft-# =	
Strength Level	ft-# =	3,246.0

Moment.....Allowable

	=	5,412.6
--	---	---------

Shear.....Actual		
Service Level	psi =	
Strength Level	psi =	18.9
Shear.....Allowable	psi =	47.6
Anet (Masonry)	in2 =	
Wall Weight	psf =	100.0
Rebar Depth 'd'	in =	6.25

Masonry Data

f'm	psi =	
Fs	psi =	
Solid Grouting	=	
Modular Ratio 'n'	=	
Equiv. Solid Thick.	=	
Masonry Block Type	=	
Masonry Design Method	= ASD	

Concrete Data

f'c	psi =	2,500.0
Fy	psi =	40,000.0

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft wall

Concrete Stem Rebar Area Details

	<u>Vertical Reinforcing</u>	<u>Horizontal Reinforcing</u>
Bottom Stem		
As (based on applied moment) :	0.1824 in ² /ft	
0.0018bh : 0.0018(12)(8) :	0.1728 in ² /ft	
	=====	Horizontal Reinforcing Options :
Required Area :	0.1824 in ² /ft	<u>One layer of :</u> #4@ 13.89 in
Provided Area :	0.3 in ² /ft	<u>Two layers of :</u> #4@ 27.78 in
Maximum Area :	1.27 in ² /ft	#5@ 21.53 in #5@ 43.06 in
		#6@ 30.56 in #6@ 61.11 in

Footing Data

Toe Width	=	2.50 ft
Heel Width	=	1.50
Total Footing Width	=	4.00
Footing Thickness	=	10.00 in
Key Width	=	0.00 in
Key Depth	=	0.00 in
Key Distance from Toe	=	0.00 ft
f'c = 2,500 psi	Fy = 40,000 psi	
Footing Concrete Density	=	150.00 pcf
Min. As %	=	0.0018
Cover @ Top	2.00	@ Btm.= 3.00 in

Footing Design Results

	<u>Toe</u>	<u>Heel</u>
Factored Pressure	= 1,470	0 psf
Mu' : Upward	= 3,412	0 ft-#
Mu' : Downward	= 469	327 ft-#
Mu: Design	= 2,943 OK	327 ft-# OK
phiMn	= 4,264	4,912 ft-#
Actual 1-Way Shear	= 21.98	8.71 psi
Allow 1-Way Shear	= 75.00	75.00 psi
Toe Reinforcing	= # 4 @ 11.11 in	
Heel Reinforcing	= # 4 @ 11.11 in	
Key Reinforcing	= None Spec'd	
Footing Torsion, Tu	= 0.00 ft-lbs	
Footing Allow. Torsion, phi Tu	= 0.00 ft-lbs	

If torsion exceeds allowable, provide supplemental design for footing torsion.

Other Acceptable Sizes & Spacings

Toe: #4@ 11.11 in, #5@ 17.22 in, #6@ 24.44 in, #7@ 33.33 in, #8@ 43.88 in, #9@ 55.55 in, #10@ 70.55 in

Heel: #4@ 11.11 in, #5@ 17.22 in, #6@ 24.44 in, #7@ 33.33 in, #8@ 43.88 in, #9@ 55.55 in, #10@ 70.55 in

Key: No key defined

Min footing T&S reinf Area	0.86 in ²
Min footing T&S reinf Area per foot	0.22 in ² /ft
If one layer of horizontal bars:	If two layers of horizontal bars:
#4@ 11.11 in	#4@ 22.22 in
#5@ 17.22 in	#5@ 34.44 in
#6@ 24.44 in	#6@ 48.89 in

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft wall

Summary of Overturning & Resisting Forces & Moments

ItemOVERTURNING.....		RESISTING.....		
	Force lbs	Distance ft	Moment ft-#	Force lbs	Distance ft	Moment ft-#
HL Act Pres (ab water tbl)	817.2	2.28	1,861.3	Soil Over HL (ab. water tbl)	550.0	3.58
HL Act Pres (be water tbl)				Soil Over HL (bel. water tbl)		3.58
Hydrostatic Force				Water Table		1,970.8
Buoyant Force	=			Sloped Soil Over Heel	=	
Surcharge over Heel	=			Surcharge Over Heel	=	
Surcharge Over Toe	=			Adjacent Footing Load	=	
Adjacent Footing Load	=			Axial Dead Load on Stem	=	
Added Lateral Load	=			* Axial Live Load on Stem	=	
Load @ Stem Above Soil	=			Soil Over Toe	=	
Seismic Earth Load	=	326.9	3.42	Surcharge Over Toe	=	
	=			Stem Weight(s)	=	650.0
				Earth @ Stem Transitions	=	2.83
Total	= 1,144.0	O.T.M.	= 2,978.1	Footing Weight	= 500.0	1,841.7
				Key Weight	=	2.00
				Vert. Component	=	1,000.0
				Total =	1,700.0 lbs R.M.=	4,812.5

Resisting/Overturning Ratio = 1.62
Vertical Loads used for Soil Pressure = 1,700.0 lbs

If seismic is included, the OTM and sliding ratios may be 1.1 per section 1807.2.3 of IBC.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

* Axial live load NOT included in total displayed, or used for overturning resistance, but is included for soil pressure calculation.

Tilt

Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus 250.0 pci

Horizontal Defl @ Top of Wall (approximate only) 0.047 in

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft wall

Rebar Lap & Embedment Lengths Information

Stem Design Segment: Bottom

Stem Design Height: 0.00 ft above top of footing

Lap Splice length for #4 bar specified in this stem design segment (25.4.2.4a) = 15.60 in
Development length for #4 bar specified in this stem design segment = 12.00 in

Hooked embedment length into footing for #4 bar specified in this stem design segment = 0.00 in
As Provided = 0.3000 in²/ft
As Required = 0.2432 in²/ft

Cantilevered Retaining Wall

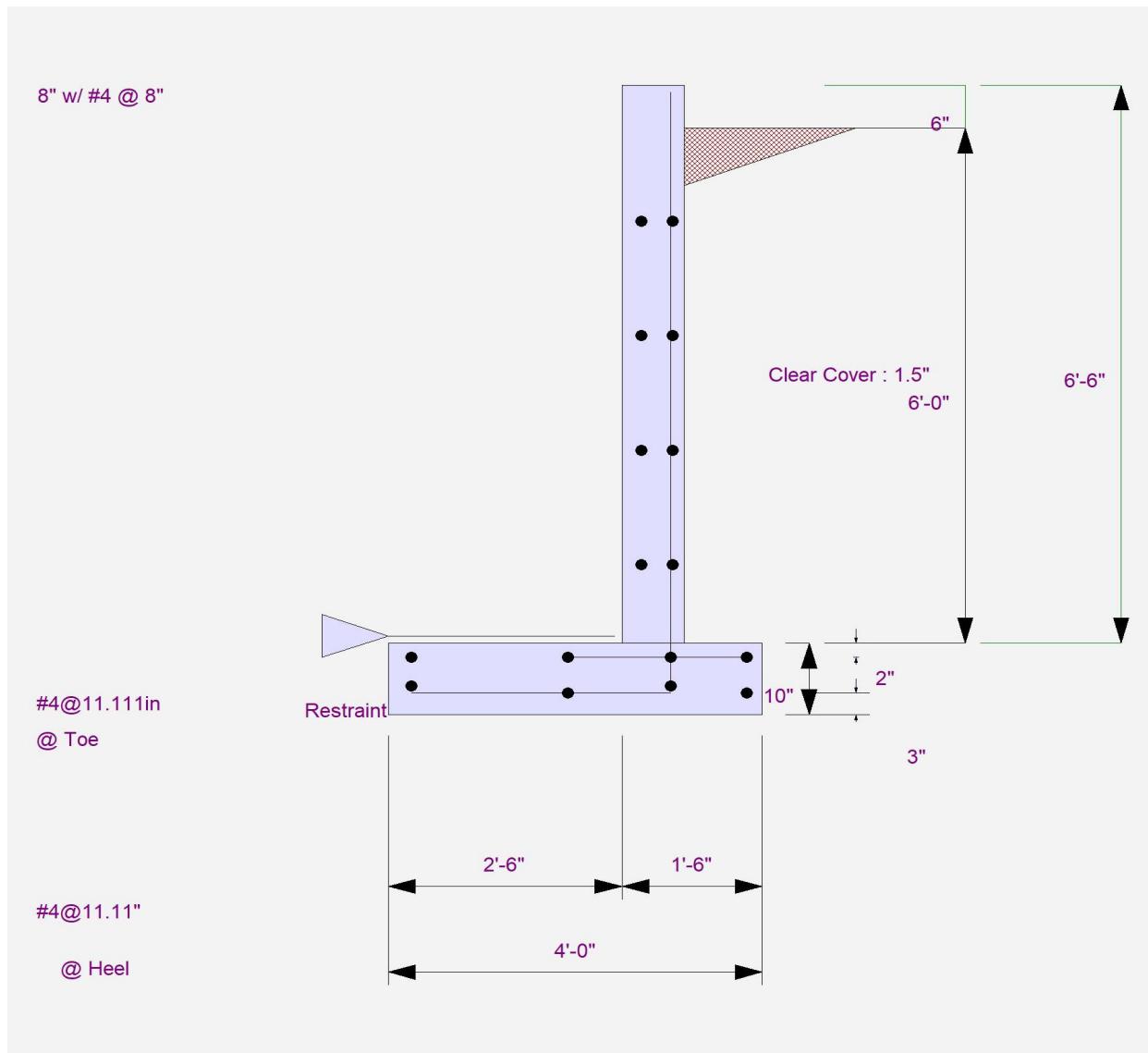
Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft wall



Cantilevered Retaining Wall

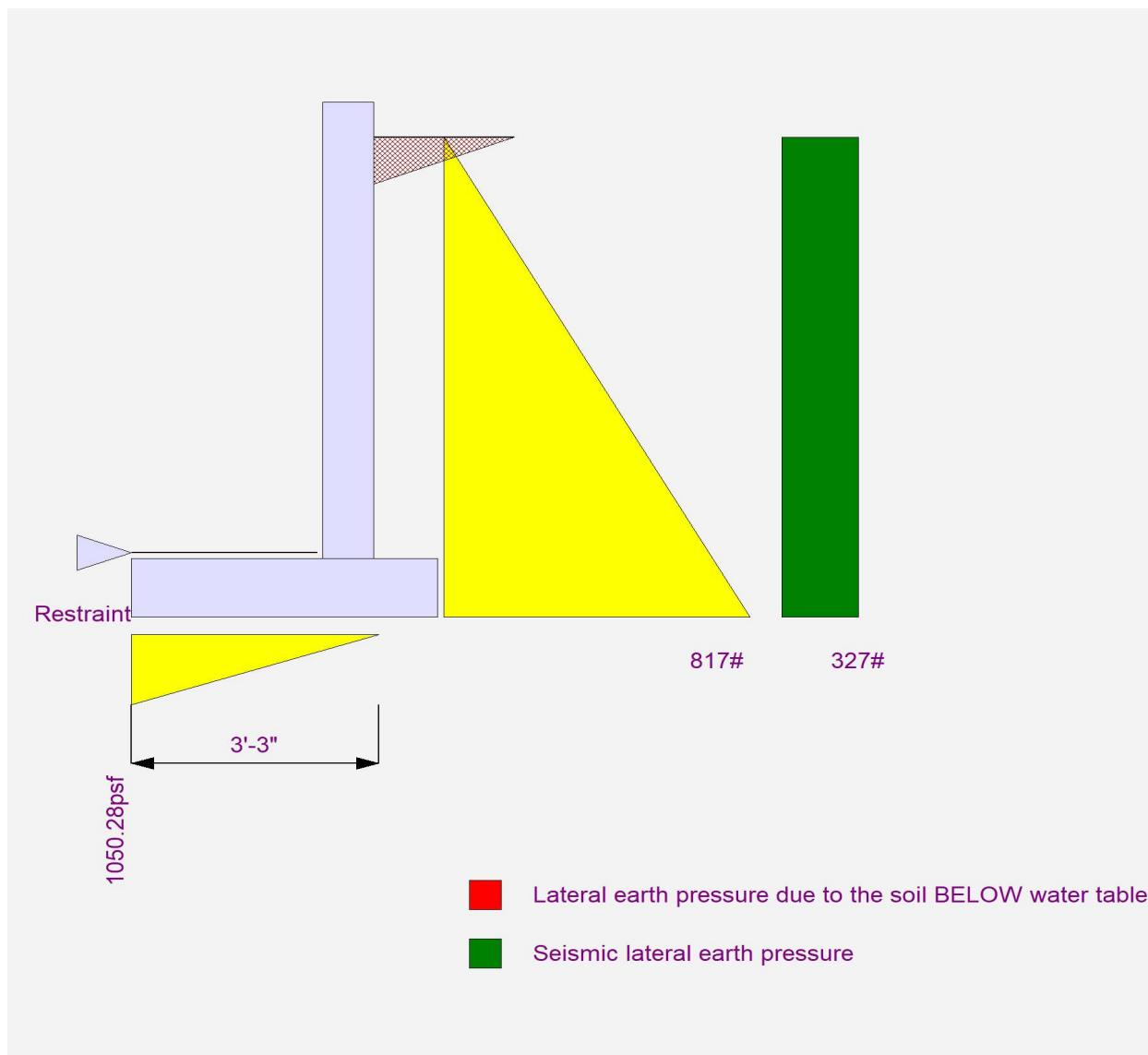
Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft wall



Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 8ft wall

Code Reference:

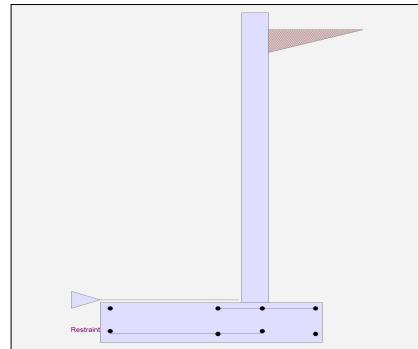
Calculations per IBC 2021 1807.3, ASCE 7-16

Criteria

Retained Height	=	8.00 ft
Wall height above soil	=	0.50 ft
Slope Behind Wall	=	0.00
Height of Soil over Toe	=	0.00 in
Water table above bottom of footing	=	0.0 ft

Soil Data

Allow Soil Bearing	=	1,500.0 psf
Equivalent Fluid Pressure Method	=	
Active Heel Pressure	=	35.0 psf/ft
	=	
Passive Pressure	=	150.0 psf/ft
Soil Density, Heel	=	110.00 pcf
Soil Density, Toe	=	110.00 pcf
Footing Soil Friction	=	0.400
Soil height to ignore for passive pressure	=	12.00 in



Surcharge Loads

Surcharge Over Heel	=	0.0 psf
Used To Resist Sliding & Overturning	=	
Surcharge Over Toe	=	0.0
Used for Sliding & Overturning	=	

Axial Load Applied to Stem

Axial Dead Load	=	0.0 lbs
Axial Live Load	=	0.0 lbs
Axial Load Eccentricity	=	0.0 in

Lateral Load Applied to Stem

Lateral Load	=	0.0 #/ft
...Height to Top	=	0.00 ft
...Height to Bottom	=	0.00 ft
Load Type	=	Wind (W) (Service Level)
Wind on Exposed Stem	=	0.0 psf (Strength Level)

Adjacent Footing Load

Adjacent Footing Load	=	0.0 lbs
Footing Width	=	0.00 ft
Eccentricity	=	0.00 in
Wall to Ftg CL Dist	=	0.00 ft
Footing Type	=	Spread Footing
Base Above/Below Soil at Back of Wall	=	0.0 ft
Poisson's Ratio	=	0.300

Earth Pressure Seismic Load

Method : Uniform	
Multiplier Used	= 10.000
(Multiplier used on soil density)	

Uniform Seismic Force = 91.667
Total Seismic Force = 840.278

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 8ft wall

Design Summary

Wall Stability Ratios

Overturning = 1.61 OK
Slab Resists All Sliding !

Global Stability = 1.51

Total Bearing Load = 2,986 lbs
...resultant ecc. = 15.37 in

Eccentricity outside middle third

Soil Pressure @ Toe = 1,355 psf OK

Soil Pressure @ Heel = 0 psf OK

Allowable = 1,500 psf

Soil Pressure Less Than Allowable

ACI Factored @ Toe = 1,897 psf

ACI Factored @ Heel = 0 psf

Footing Shear @ Toe = 23.4 psi OK

Footing Shear @ Heel = 12.1 psi OK

Allowable = 75.0 psi

Sliding Calcs

Lateral Sliding Force = 2,058.7 lbs

Vertical component of active lateral soil pressure IS
NOT considered in the calculation of soil bearing

Load Factors

Building Code

Dead Load = 1.200

Live Load = 1.600

Earth, H = 1.600

Wind, W = 1.600

Seismic, E = 1.000

Stem Construction

Design Height Above Ftg

ft = Stem OK 0.00

Wall Material Above "Ht" = Concrete

Design Method = SD SD SD

Thickness = 8.00

Rebar Size = # 5

Rebar Spacing = 10.00

Rebar Placed at = Edge

Design Data

fb/FB + fa/Fa = 0.801

Total Force @ Section

Service Level lbs =

Strength Level lbs = 2,525.3

Moment....Actual

Service Level ft-# =

Strength Level ft-# = 7,712.0

Moment.....Allowable = 9,623.1

Shear....Actual

Service Level psi =

Strength Level psi = 34.0

Shear.....Allowable psi = 51.3

Anet (Masonry) in2 =

Wall Weight psf = 100.0

Rebar Depth 'd' in = 6.19

Masonry Data

f'm psi =

Fs psi =

Solid Grouting =

Modular Ratio 'n' =

Equiv. Solid Thick. =

Masonry Block Type =

Masonry Design Method = ASD

Concrete Data

f'c psi = 2,500.0

Fy psi = 60,000.0

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 8ft wall

Concrete Stem Rebar Area Details

	<u>Vertical Reinforcing</u>	<u>Horizontal Reinforcing</u>
Bottom Stem		
As (based on applied moment) :	0.292 in ² /ft	
0.0018bh : 0.0018(12)(8) :	0.1728 in ² /ft	
	=====	Horizontal Reinforcing Options :
Required Area :	0.292 in ² /ft	#4@ 13.89 in #4@ 27.78 in
Provided Area :	0.372 in ² /ft	#5@ 21.53 in #5@ 43.06 in
Maximum Area :	0.8382 in ² /ft	#6@ 30.56 in #6@ 61.11 in

Footing Data

Toe Width	=	3.50 ft
Heel Width	=	2.00
Total Footing Width	=	5.50
Footing Thickness	=	14.00 in
Key Width	=	0.00 in
Key Depth	=	0.00 in
Key Distance from Toe	=	0.00 ft
f'c = 2,500 psi	Fy = 40,000 psi	
Footing Concrete Density	=	150.00 pcf
Min. As %	=	0.0018
Cover @ Top	2.00	@ Btm.= 3.00 in

Footing Design Results

	<u>Toe</u>	<u>Heel</u>
Factored Pressure	= 1,897	0 psf
Mu' : Upward	= 8,542	1 ft-#
Mu' : Downward	= 1,286	1,125 ft-#
Mu: Design	= 7,256 OK	1,124 ft-# OK
phiMn	= 9,918	10,388 ft-#
Actual 1-Way Shear	= 23.37	12.14 psi
Allow 1-Way Shear	= 75.00	75.00 psi
Toe Reinforcing	= # 5 @ 11.75 in	
Heel Reinforcing	= # 5 @ 12.30 in	
Key Reinforcing	= None Spec'd	
Footing Torsion, Tu	= 0.00 ft-lbs	
Footing Allow. Torsion, phi Tu	= 0.00 ft-lbs	

If torsion exceeds allowable, provide supplemental design for footing torsion.

Other Acceptable Sizes & Spacings

Toe: #4@ 7.57 in, #5@ 11.74 in, #6@ 16.66 in, #7@ 22.73 in, #8@ 29.92 in, #9@ 37.88 in, #10@ 48.11 in

Heel: #4@ 7.93 in, #5@ 12.30 in, #6@ 17.46 in, #7@ 23.80 in, #8@ 31.34 in, #9@ 39.68 in, #10@ 50.39 in

Key: No key defined

Min footing T&S reinf Area	1.66 in ²
Min footing T&S reinf Area per foot	0.30 in ² /ft
If one layer of horizontal bars:	If two layers of horizontal bars:
#4@ 7.94 in	#4@ 15.87 in
#5@ 12.30 in	#5@ 24.60 in
#6@ 17.46 in	#6@ 34.92 in

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 8ft wall

Summary of Overturning & Resisting Forces & Moments

ItemOVERTURNING.....		RESISTING.....		
	Force lbs	Distance ft	Moment ft-#	Force lbs	Distance ft	Moment ft-#
HL Act Pres (ab water tbl)	1,470.5	3.06	4,493.2	Soil Over HL (ab. water tbl)	1,173.3	4.83
HL Act Pres (be water tbl)				Soil Over HL (bel. water tbl)		4.83
Hydrostatic Force				Water Table		5,671.1
Buoyant Force	=			Sloped Soil Over Heel	=	
Surcharge over Heel	=			Surcharge Over Heel	=	
Surcharge Over Toe	=			Adjacent Footing Load	=	
Adjacent Footing Load	=			Axial Dead Load on Stem	=	
Added Lateral Load	=			* Axial Live Load on Stem	=	
Load @ Stem Above Soil	=			Soil Over Toe	=	
Seismic Earth Load	=	588.2	4.58	Surcharge Over Toe	=	
	=			Stem Weight(s)	=	850.0
	=			Earth @ Stem Transitions	=	3.83
Total	=	2,058.7	O.T.M. =	Footing Weight	=	3,258.3
				Key Weight	=	962.5
				Vert. Component	=	2.75
				Total =	2,985.8 lbs R.M.=	11,576.3

Resisting/Overturning Ratio = **1.61**
Vertical Loads used for Soil Pressure = 2,985.8 lbs

If seismic is included, the OTM and sliding ratios may be 1.1 per section 1807.2.3 of IBC.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

* Axial live load NOT included in total displayed, or used for overturning resistance, but is included for soil pressure calculation.

Tilt

Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus 250.0 pci

Horizontal Defl @ Top of Wall (approximate only) 0.058 in

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 8ft wall

Rebar Lap & Embedment Lengths Information

Stem Design Segment: Bottom

Stem Design Height: 0.00 ft above top of footing

Lap Splice length for #5 bar specified in this stem design segment (25.4.2.4a) = 23.40 in
Development length for #5 bar specified in this stem design segment = 18.00 in

Hooked embedment length into footing for #5 bar specified in this stem design segment = 0.00 in
As Provided = 0.3720 in²/ft
As Required = 0.2920 in²/ft

Cantilevered Retaining Wall

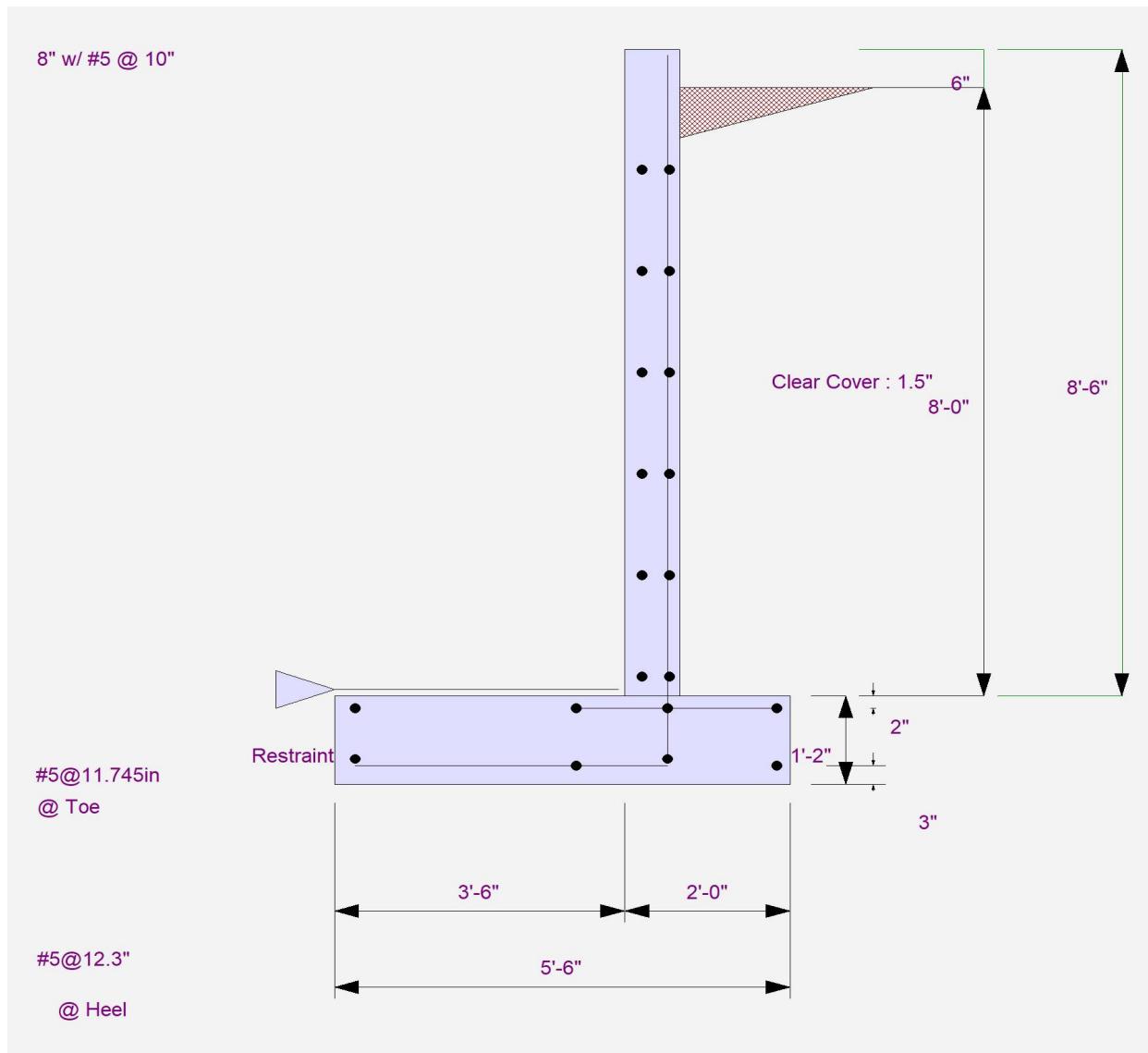
Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 8ft wall



Cantilevered Retaining Wall

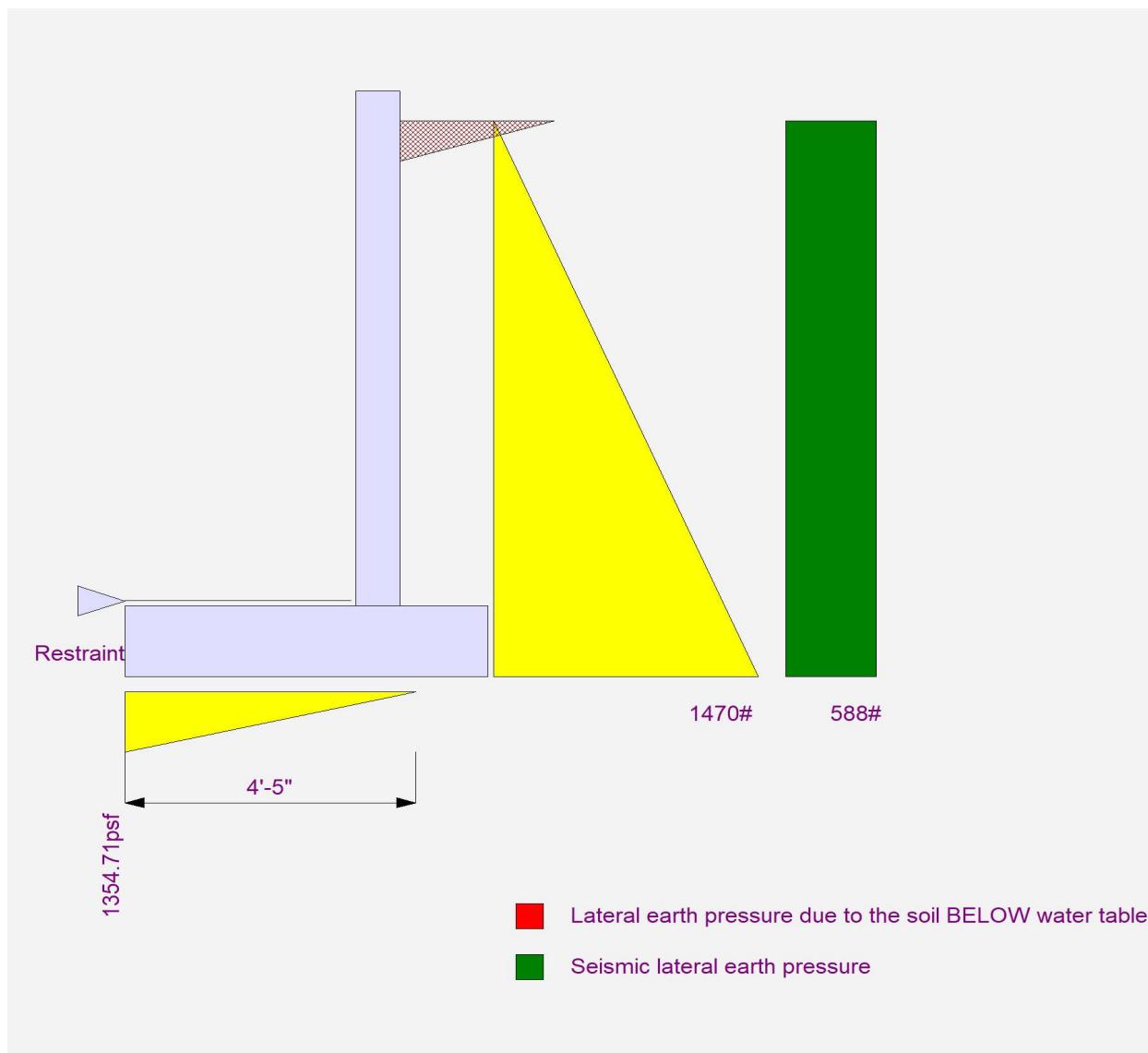
Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 8ft wall



Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 9ft wall

Code Reference:

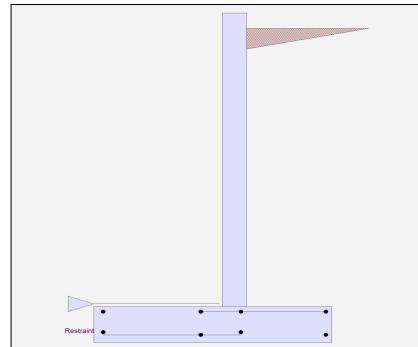
Calculations per IBC 2021 1807.3, ASCE 7-16

Criteria

Retained Height	=	9.00 ft
Wall height above soil	=	0.50 ft
Slope Behind Wall	=	0.00
Height of Soil over Toe	=	0.00 in
Water table above bottom of footing	=	0.0 ft

Soil Data

Allow Soil Bearing	=	1,500.0 psf
Equivalent Fluid Pressure Method	=	
Active Heel Pressure	=	35.0 psf/ft
	=	
Passive Pressure	=	150.0 psf/ft
Soil Density, Heel	=	110.00 pcf
Soil Density, Toe	=	110.00 pcf
Footing Soil Friction	=	0.400
Soil height to ignore for passive pressure	=	12.00 in



Surcharge Loads

Surcharge Over Heel	=	0.0 psf
Used To Resist Sliding & Overturning	=	
Surcharge Over Toe	=	0.0
Used for Sliding & Overturning	=	

Axial Load Applied to Stem

Axial Dead Load	=	0.0 lbs
Axial Live Load	=	0.0 lbs
Axial Load Eccentricity	=	0.0 in

Lateral Load Applied to Stem

Lateral Load	=	0.0 #/ft
...Height to Top	=	0.00 ft
...Height to Bottom	=	0.00 ft
Load Type	=	Wind (W) (Service Level)
Wind on Exposed Stem	=	0.0 psf (Strength Level)

Adjacent Footing Load

Adjacent Footing Load	=	0.0 lbs
Footing Width	=	0.00 ft
Eccentricity	=	0.00 in
Wall to Ftg CL Dist	=	0.00 ft
Footing Type	=	Spread Footing
Base Above/Below Soil at Back of Wall	=	0.0 ft
Poisson's Ratio	=	0.300

Earth Pressure Seismic Load

Method : Uniform	
Multiplier Used	= 10.000
(Multiplier used on soil density)	

Uniform Seismic Force = 101.667
Total Seismic Force = 1,033.611

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 9ft wall

Design Summary

Wall Stability Ratios

Overturning = 2.00 OK
Slab Resists All Sliding !

Global Stability = 1.62

Total Bearing Load = 4,398 lbs
...resultant ecc. = 12.12 in

Eccentricity within middle third

Soil Pressure @ Toe = 1,307 psf OK
Soil Pressure @ Heel = 46 psf OK

Allowable = 1,500 psf

Soil Pressure Less Than Allowable

ACI Factored @ Toe = 1,830 psf
ACI Factored @ Heel = 64 psf

Footing Shear @ Toe = 26.3 psi OK
Footing Shear @ Heel = 17.2 psi OK

Allowable = 75.0 psi

Sliding Calcs

Lateral Sliding Force = 2,532.3 lbs

Vertical component of active lateral soil pressure IS
NOT considered in the calculation of soil bearing

Load Factors

Building Code
Dead Load = 1.200
Live Load = 1.600
Earth, H = 1.600
Wind, W = 1.600
Seismic, E = 1.000

Stem Construction

Design Height Above Ftg

ft = Stem OK
= 0.00
Wall Material Above "Ht"
= Concrete
Design Method
= SD SD SD

Thickness = 8.00

Rebar Size = # 5

Rebar Spacing = 8.00

Rebar Placed at = Edge

Design Data

fb/FB + fa/Fa = 0.925

Total Force @ Section

Service Level lbs =
Strength Level lbs = 3,183.0

Moment....Actual

Service Level ft-# =
Strength Level ft-# = 10,921.5
Moment.....Allowable = 11,799.2

Shear.....Actual

Service Level psi =
Strength Level psi = 42.9
Shear.....Allowable psi = 55.3
Anet (Masonry) in2 =
Wall Weight psf = 100.0
Rebar Depth 'd' in = 6.19

Masonry Data

f'm psi =
Fs psi =
Solid Grouting =
Modular Ratio 'n' =
Equiv. Solid Thick. =
Masonry Block Type =
Masonry Design Method = ASD

Concrete Data

f'c psi = 2,500.0
Fy psi = 60,000.0

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 9ft wall

Concrete Stem Rebar Area Details

	<u>Vertical Reinforcing</u>	<u>Horizontal Reinforcing</u>
Bottom Stem As (based on applied moment) :	0.4135 in ² /ft	
0.0018bh : 0.0018(12)(8) :	0.1728 in ² /ft	
	=====	Horizontal Reinforcing Options :
Required Area :	0.4135 in ² /ft	#4@ 13.89 in #4@ 27.78 in
Provided Area :	0.465 in ² /ft	#5@ 21.53 in #5@ 43.06 in
Maximum Area :	0.8382 in ² /ft	#6@ 30.56 in #6@ 61.11 in

Footing Data

Toe Width	=	3.50 ft
Heel Width	=	3.00
Total Footing Width	=	6.50
Footing Thickness	=	14.00 in
Key Width	=	0.00 in
Key Depth	=	0.00 in
Key Distance from Toe	=	0.00 ft
f'c = 2,500 psi	Fy =	60,000 psi
Footing Concrete Density	=	150.00 pcf
Min. As %	=	0.0018
Cover @ Top	2.00	@ Btm.= 3.00 in

Footing Design Results

	<u>Toe</u>	<u>Heel</u>
Factored Pressure	= 1,830	64 psf
Mu' : Upward	= 9,268	750 ft-#
Mu' : Downward	= 1,286	3,806 ft-#
Mu: Design	= 7,982 OK	3,056 ft-# OK
phiMn	= 14,059	15,420 ft-#
Actual 1-Way Shear	= 26.32	17.19 psi
Allow 1-Way Shear	= 75.00	75.00 psi
Toe Reinforcing	= # 5 @ 12.30 in	
Heel Reinforcing	= # 5 @ 12.30 in	
Key Reinforcing	= None Spec'd	
Footing Torsion, Tu	= 0.00 ft-lbs	
Footing Allow. Torsion, phi Tu	= 0.00 ft-lbs	

If torsion exceeds allowable, provide supplemental design for footing torsion.

Other Acceptable Sizes & Spacings

Toe: #4@ 7.93 in, #5@ 12.30 in, #6@ 17.46 in, #7@ 23.80 in, #8@ 31.34 in, #9@ 39.68 in, #10@ 50.39 in

Heel: #4@ 7.93 in, #5@ 12.30 in, #6@ 17.46 in, #7@ 23.80 in, #8@ 31.34 in, #9@ 39.68 in, #10@ 50.39 in

Key: No key defined

Min footing T&S reinf Area	1.97 in ²
Min footing T&S reinf Area per foot	0.30 in ² /ft
If one layer of horizontal bars:	If two layers of horizontal bars:
#4@ 7.94 in	#4@ 15.87 in
#5@ 12.30 in	#5@ 24.60 in
#6@ 17.46 in	#6@ 34.92 in

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 9ft wall

Summary of Overturning & Resisting Forces & Moments

ItemOVERTURNING.....		RESISTING.....		
	Force lbs	Distance ft	Moment ft-#	Force lbs	Distance ft	Moment ft-#
HL Act Pres (ab water tbl)	1,808.8	3.39	6,129.9	Soil Over HL (ab. water tbl)	2,310.0	5.33
HL Act Pres (be water tbl)				Soil Over HL (bel. water tbl)		5.33
Hydrostatic Force				Water Table		
Buoyant Force	=			Sloped Soil Over Heel	=	
Surcharge over Heel	=			Surcharge Over Heel	=	
Surcharge Over Toe	=			Adjacent Footing Load	=	
Adjacent Footing Load	=			Axial Dead Load on Stem	=	
Added Lateral Load	=			* Axial Live Load on Stem	=	
Load @ Stem Above Soil	=			Soil Over Toe	=	
Seismic Earth Load	=	723.5	5.08	Surcharge Over Toe	=	
	=			Stem Weight(s)	=	950.0
				Earth @ Stem Transitions	=	3.83
Total	= 2,532.3	O.T.M.	= 9,807.8	Footing Weight	= 1,137.5	3,641.7
				Key Weight	=	3,696.9
				Vert. Component	=	
					Total = 4,397.5 lbs R.M.=	19,658.5

Resisting/Overturning Ratio = 2.00
Vertical Loads used for Soil Pressure = 4,397.5 lbs

If seismic is included, the OTM and sliding ratios may be 1.1 per section 1807.2.3 of IBC.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

* Axial live load NOT included in total displayed, or used for overturning resistance, but is included for soil pressure calculation.

Tilt

Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus 250.0 pci

Horizontal Defl @ Top of Wall (approximate only) 0.053 in

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 9ft wall

Rebar Lap & Embedment Lengths Information

Stem Design Segment: Bottom

Stem Design Height: 0.00 ft above top of footing

Lap Splice length for #5 bar specified in this stem design segment (25.4.2.4a) = 23.40 in
Development length for #5 bar specified in this stem design segment = 18.00 in

Hooked embedment length into footing for #5 bar specified in this stem design segment = 0.00 in
As Provided = 0.4650 in²/ft
As Required = 0.4135 in²/ft

Cantilevered Retaining Wall

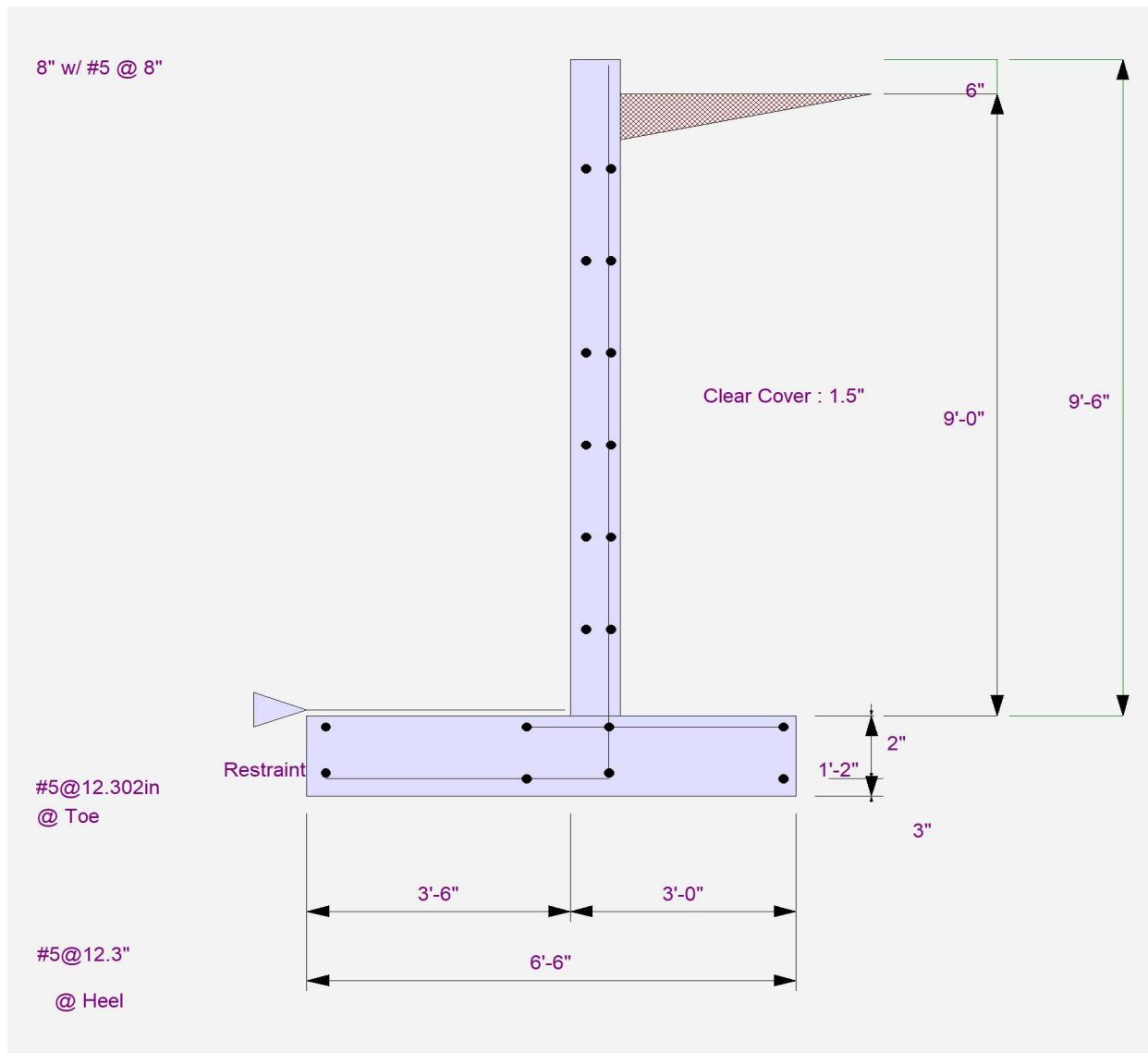
Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 9ft wall



Cantilevered Retaining Wall

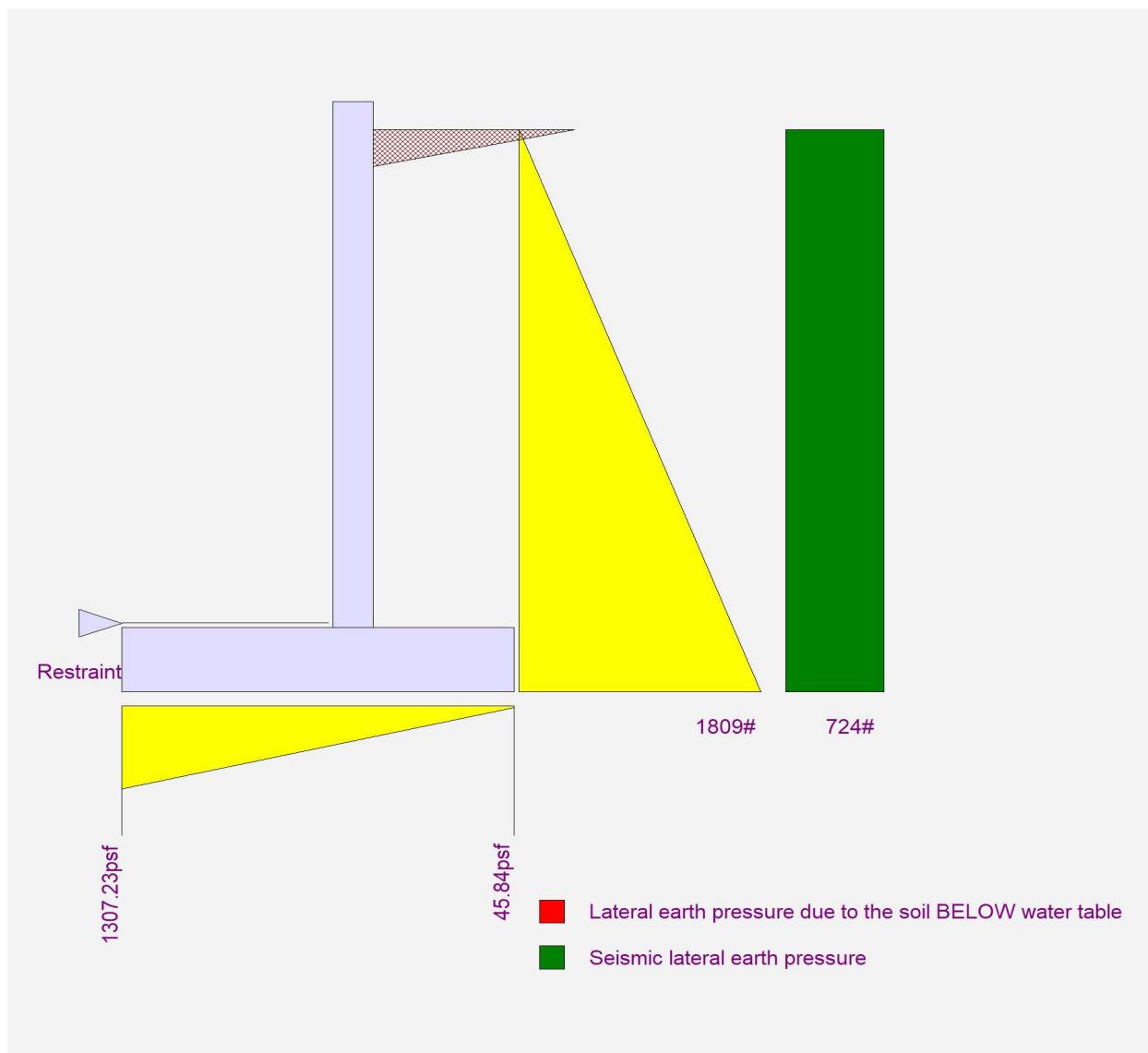
Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 9ft wall



Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft ret. wall with Key

Code Reference:

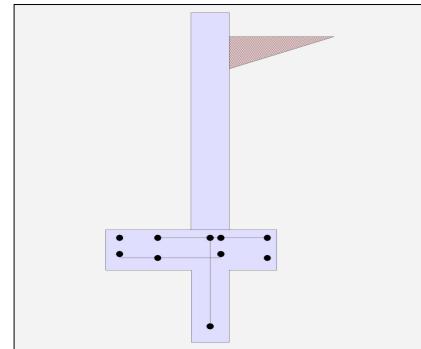
Calculations per IBC 2021 1807.3, ASCE 7-16

Criteria

Retained Height	=	4.00 ft
Wall height above soil	=	0.50 ft
Slope Behind Wall	=	0.00
Height of Soil over Toe	=	0.00 in
Water table above bottom of footing	=	0.0 ft

Soil Data

Allow Soil Bearing	=	1,500.0 psf
Equivalent Fluid Pressure Method	=	
Active Heel Pressure	=	35.0 psf/ft
	=	
Passive Pressure	=	150.0 psf/ft
Soil Density, Heel	=	110.00 pcf
Soil Density, Toe	=	110.00 pcf
Footing Soil Friction	=	0.400
Soil height to ignore for passive pressure	=	12.00 in



Surcharge Loads

Surcharge Over Heel	=	0.0 psf
NOT Used To Resist Sliding & Overturning	=	
Surcharge Over Toe	=	0.0
NOT Used for Sliding & Overturning	=	

Axial Load Applied to Stem

Axial Dead Load	=	0.0 lbs
Axial Live Load	=	0.0 lbs
Axial Load Eccentricity	=	0.0 in

Lateral Load Applied to Stem

Lateral Load	=	0.0 #/ft
...Height to Top	=	0.00 ft
...Height to Bottom	=	0.00 ft
Load Type	=	Wind (W) (Service Level)
Wind on Exposed Stem	=	0.0 psf (Strength Level)

Adjacent Footing Load

Adjacent Footing Load	=	0.0 lbs
Footing Width	=	0.00 ft
Eccentricity	=	0.00 in
Wall to Ftg CL Dist	=	0.00 ft
Footing Type	=	Spread Footing
Base Above/Below Soil at Back of Wall	=	0.0 ft
Poisson's Ratio	=	0.300

Earth Pressure Seismic Load

Method : Uniform		
Multiplier Used	=	6.000
(Multiplier used on soil density)		

$$\text{Uniform Seismic Force} = 29.000 \quad \text{Total Seismic Force} = 140.167$$

$$F_p / W_p \text{ Weight Multiplier} = 0.200 \quad g \text{ Added seismic base force} = 63.0 \text{ lbs}$$

Stem Weight Seismic Load

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft ret. wall with Key

Design Summary

Wall Stability Ratios

Overturning	=	2.39	OK
Sliding	=	1.53	OK
Global Stability	=	1.97	

Total Bearing Load	=	1,342	lbs
...resultant ecc.	=	4.41	in

Eccentricity within middle third

Soil Pressure @ Toe	=	776	psf	OK
Soil Pressure @ Heel	=	119	psf	OK

Allowable Soil Pressure Less Than Allowable

ACI Factored @ Toe	=	1,086	psf
ACI Factored @ Heel	=	166	psf
Footing Shear @ Toe	=	9.7	psi
Footing Shear @ Heel	=	3.6	psi
Allowable	=	75.0	psi

Sliding Calcs

Lateral Sliding Force	=	569.9	lbs
less 100% Passive Force	-	333.3	lbs
less 100% Friction Force	-	536.7	lbs
Added Force Req'd	=	0.0	lbs OK
....for 1.5 Stability	=	0.0	lbs OK

Vertical component of active lateral soil pressure IS
NOT considered in the calculation of soil bearing

Load Factors

Building Code	
Dead Load	1.200
Live Load	1.600
Earth, H	1.600
Wind, W	1.600
Seismic, E	1.000

Stem Construction

Design Height Above Ftg	ft =	Stem OK
Wall Material Above "Ht"	=	Concrete
Design Method	=	SD
Thickness	=	8.00
Rebar Size	=	# 4
Rebar Spacing	=	12.00
Rebar Placed at	=	Edge

Design Data

fb/FB + fa/Fa	=	0.282
---------------	---	-------

Total Force @ Section

Service Level	lbs =
Strength Level	lbs = 654.0

Moment....Actual

Service Level	ft-# =
Strength Level	ft-# = 1,031.8

Moment.....Allowable	= 3,655.6
----------------------	-----------

Shear.....Actual

Service Level	psi =
Strength Level	psi = 8.7
Shear.....Allowable	psi = 41.6
Anet (Masonry)	in2 =
Wall Weight	psf = 100.0
Rebar Depth 'd'	in = 6.25

Masonry Data

f'm	psi =
Fs	psi =
Solid Grouting	=
Modular Ratio 'n'	=
Equiv. Solid Thick.	=
Masonry Block Type	=
Masonry Design Method	= ASD

Concrete Data

f'c	psi = 2,500.0
Fy	psi = 40,000.0

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft ret. wall with Key

Concrete Stem Rebar Area Details

	<u>Vertical Reinforcing</u>	<u>Horizontal Reinforcing</u>
Bottom Stem		
As (based on applied moment) :	0.058 in ² /ft	
0.0018bh : 0.0018(12)(8) :	0.1728 in ² /ft	
	=====	Horizontal Reinforcing Options :
Required Area :	0.1728 in ² /ft	<u>One layer of :</u> #4@ 13.89 in
Provided Area :	0.2 in ² /ft	<u>Two layers of :</u> #4@ 27.78 in
Maximum Area :	1.27 in ² /ft	#5@ 21.53 in #5@ 43.06 in
		#6@ 30.56 in #6@ 61.11 in

Footing Data

Toe Width	=	1.50 ft
Heel Width	=	1.50
Total Footing Width	=	3.00
Footing Thickness	=	10.00 in
Key Width	=	8.00 in
Key Depth	=	18.00 in
Key Distance from Toe	=	1.50 ft
f'c = 2,500 psi	Fy = 40,000 psi	
Footing Concrete Density	= 150.00 pcf	
Min. As %	= 0.0018	
Cover @ Top	2.00	@ Btm.= 3.00 in

Footing Design Results

	<u>Toe</u>	<u>Heel</u>
Factored Pressure	= 1,086	166 psf
Mu' : Upward	= 1,049	87 ft-#
Mu' : Downward	= 169	235 ft-#
Mu: Design	= 881 OK	148 ft-# OK
phiMn	= 4,307	4,961 ft-#
Actual 1-Way Shear	= 9.70	3.56 psi
Allow 1-Way Shear	= 75.00	75.00 psi
Toe Reinforcing	= # 4 @ 11.00 in	
Heel Reinforcing	= # 4 @ 11.00 in	
Key Reinforcing	= # 4 @ 13.89 in	
Footing Torsion, Tu	= 0.00 ft-lbs	
Footing Allow. Torsion, phi Tu	= 0.00 ft-lbs	

If torsion exceeds allowable, provide supplemental design for footing torsion.

Other Acceptable Sizes & Spacings

Toe: #4@ 11.11 in, #5@ 17.22 in, #6@ 24.44 in, #7@ 33.33 in, #8@ 43.88 in, #9@ 55.55 in, #10@ 70.55 in

Heel: #4@ 11.11 in, #5@ 17.22 in, #6@ 24.44 in, #7@ 33.33 in, #8@ 43.88 in, #9@ 55.55 in, #10@ 70.55 in

Key: #4@ 13.88 in, #5@ 18 in, #6@ 18 in, #7@ 18 in

Min footing T&S reinf Area	0.65 in ²
Min footing T&S reinf Area per foot	0.22 in ² /ft
If one layer of horizontal bars:	If two layers of horizontal bars:
#4@ 11.11 in	#4@ 22.22 in
#5@ 17.22 in	#5@ 34.44 in
#6@ 24.44 in	#6@ 48.89 in

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft ret. wall with Key

Summary of Overturning & Resisting Forces & Moments

ItemOVERTURNING.....		RESISTING.....		
	Force lbs	Distance ft	Moment ft-#	Force lbs	Distance ft	Moment ft-#
HL Act Pres (ab water tbl)	408.8	1.61	658.7	Soil Over HL (ab. water tbl)	366.7	2.58
HL Act Pres (be water tbl)				Soil Over HL (bel. water tbl)		2.58
Hydrostatic Force				Water Table		947.2
Buoyant Force	=			Sloped Soil Over Heel	=	
Surcharge over Heel	=			Surcharge Over Heel	=	
Surcharge Over Toe	=			Adjacent Footing Load	=	
Adjacent Footing Load	=			Axial Dead Load on Stem	=	
Added Lateral Load	=			* Axial Live Load on Stem	=	
Load @ Stem Above Soil	=			Soil Over Toe	=	
Seismic Earth Load	=	98.1	2.42	Surcharge Over Toe	=	
Seismic Stem Self Wt	=	63.0	3.08	Stem Weight(s)	=	450.0
Total	=	569.9	O.T.M. =	Earth @ Stem Transitions	1,83	825.0
				Footing Weight	=	375.0
				Key Weight	=	150.0
				Vert. Component	=	275.0
				Total =	1,341.7 lbs R.M.=	2,609.7

Resisting/Overturning Ratio = **2.39**
Vertical Loads used for Soil Pressure = 1,341.7 lbs

If seismic is included, the OTM and sliding ratios may be 1.1 per section 1807.2.3 of IBC.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

Tilt

Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus 250.0 pci

Horizontal Defl @ Top of Wall (approximate only) 0.032 in

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft ret. wall with Key

Rebar Lap & Embedment Lengths Information

Stem Design Segment: Bottom

Stem Design Height: 0.00 ft above top of footing

Lap Splice length for #4 bar specified in this stem design segment (25.4.2.4a) = 15.60 in
Development length for #4 bar specified in this stem design segment = 12.00 in

Hooked embedment length into footing for #4 bar specified in this stem design segment = 0.00 in
As Provided = 0.2000 in²/ft
As Required = 0.1728 in²/ft

Cantilevered Retaining Wall

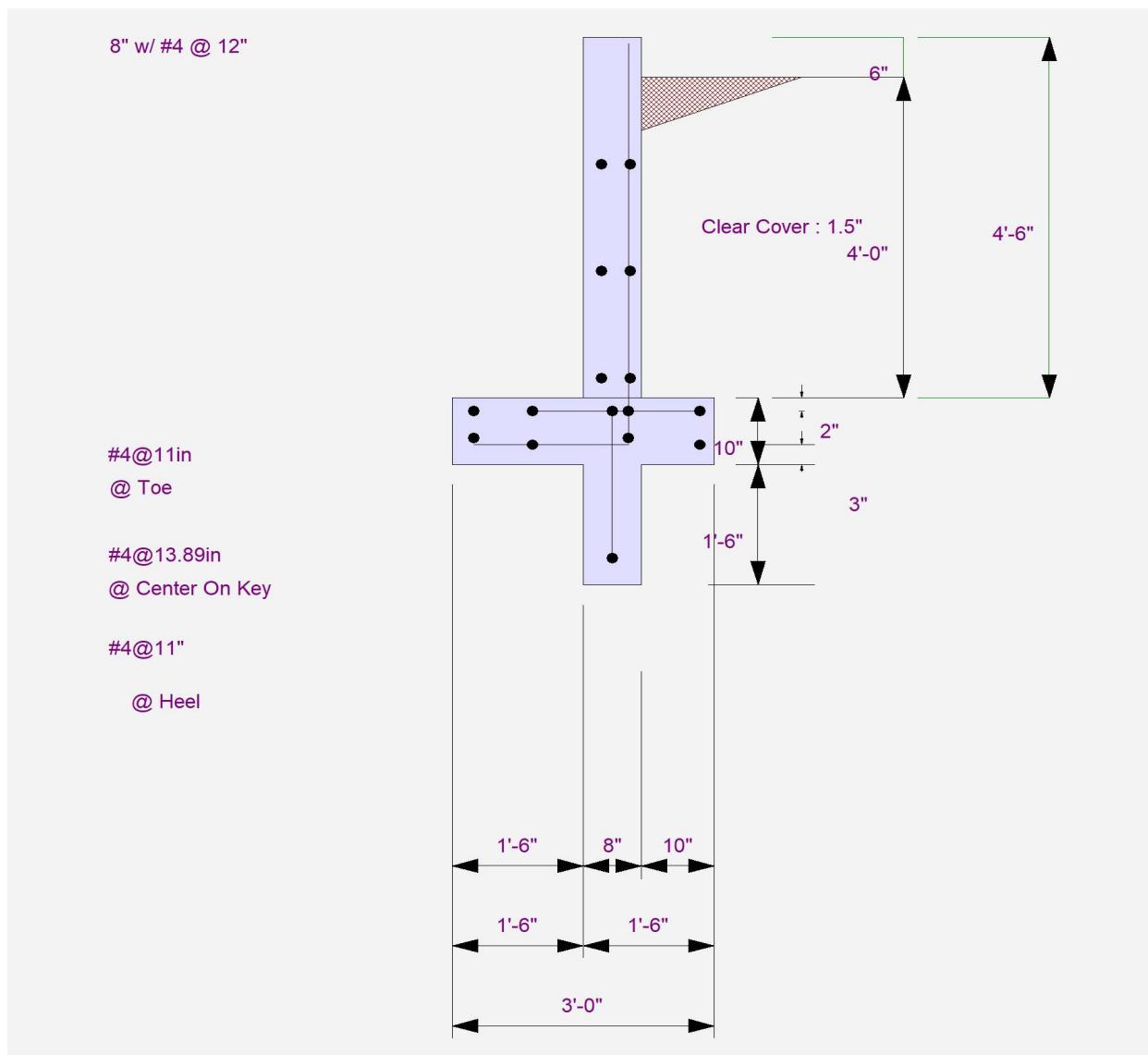
Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft ret. wall with Key



Cantilevered Retaining Wall

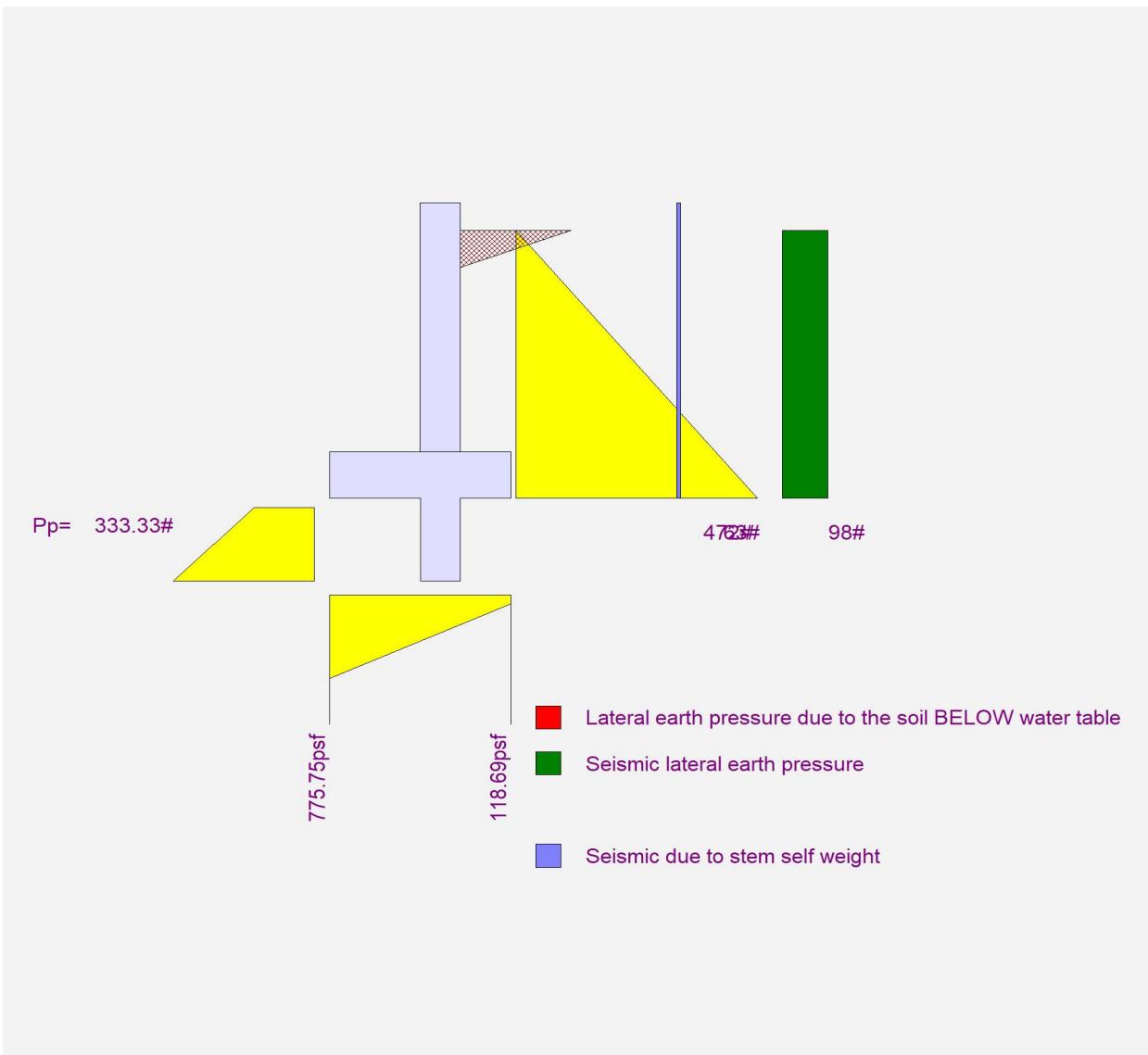
Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 4ft ret. wall with Key



Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft ret. wall with Key

Code Reference:

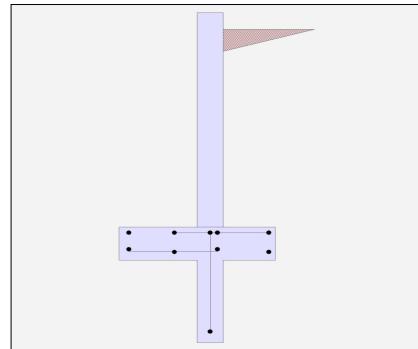
Calculations per IBC 2021 1807.3, ASCE 7-16

Criteria

Retained Height	=	6.00 ft
Wall height above soil	=	0.50 ft
Slope Behind Wall	=	0.00
Height of Soil over Toe	=	0.00 in
Water table above bottom of footing	=	0.0 ft

Soil Data

Allow Soil Bearing	=	1,500.0 psf
Equivalent Fluid Pressure Method	=	
Active Heel Pressure	=	35.0 psf/ft
	=	
Passive Pressure	=	150.0 psf/ft
Soil Density, Heel	=	110.00 pcf
Soil Density, Toe	=	110.00 pcf
Footing Soil Friction	=	0.400
Soil height to ignore for passive pressure	=	12.00 in



Surcharge Loads

Surcharge Over Heel	=	0.0 psf
Used To Resist Sliding & Overturning	=	
Surcharge Over Toe	=	0.0
Used for Sliding & Overturning	=	

Axial Load Applied to Stem

Axial Dead Load	=	0.0 lbs
Axial Live Load	=	0.0 lbs
Axial Load Eccentricity	=	0.0 in

Lateral Load Applied to Stem

Lateral Load	=	0.0 #/ft
...Height to Top	=	0.00 ft
...Height to Bottom	=	0.00 ft
Load Type	=	Wind (W) (Service Level)
Wind on Exposed Stem	=	0.0 psf (Strength Level)

Adjacent Footing Load

Adjacent Footing Load	=	0.0 lbs
Footing Width	=	0.00 ft
Eccentricity	=	0.00 in
Wall to Ftg CL Dist	=	0.00 ft
Footing Type	=	Spread Footing
Base Above/Below Soil at Back of Wall	=	0.0 ft
Poisson's Ratio	=	0.300

Earth Pressure Seismic Load

Method : Uniform	
Multiplier Used	= 6.000
(Multiplier used on soil density)	

$$\text{Uniform Seismic Force} = 42.000 \quad \text{Total Seismic Force} = 294.000$$

Stem Weight Seismic Load

$$F_p / W_p \text{ Weight Multiplier} = 0.200 \quad g \text{ Added seismic base force} = 91.0 \text{ lbs}$$

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft ret. wall with Key

Design Summary

Wall Stability Ratios

Overturning	=	2.01	OK
Sliding	=	1.56	OK
Global Stability	=	1.76	
Total Bearing Load	=	2,380	lbs
...resultant ecc.	=	8.24	in
Eccentricity outside middle third			
Soil Pressure @ Toe	=	1,208	psf OK
Soil Pressure @ Heel	=	0	psf OK
Allowable	=	1,500	psf
Soil Pressure Less Than Allowable			
ACI Factored @ Toe	=	1,692	psf
ACI Factored @ Heel	=	0	psf
Footing Shear @ Toe	=	15.6	psi OK
Footing Shear @ Heel	=	8.3	psi OK
Allowable	=	75.0	psi

Sliding Calcs

Lateral Sliding Force	=	1,154.3	lbs
less 100% Passive Force	-	843.8	lbs
less 100% Friction Force	-	952.0	lbs
Added Force Req'd	=	0.0	lbs OK
....for 1.5 Stability	=	0.0	lbs OK

Vertical component of active lateral soil pressure IS
NOT considered in the calculation of soil bearing

Load Factors

Building Code	
Dead Load	1.200
Live Load	1.600
Earth, H	1.600
Wind, W	1.600
Seismic, E	1.000

Stem Construction

Design Height Above Ftg	ft =	Stem OK
Wall Material Above "Ht"	=	Concrete
Design Method	=	SD SD SD
Thickness	=	8.00
Rebar Size	=	# 4
Rebar Spacing	=	10.00
Rebar Placed at	=	Edge

Design Data

fb/FB + fa/Fa	=	0.732
---------------	---	-------

Total Force @ Section

Service Level	lbs =	
Strength Level	lbs =	1,390.0

Moment....Actual

Service Level	ft-# =	
Strength Level	ft-# =	3,194.5
Moment.....Allowable	=	4,364.1

Shear.....Actual

Service Level	psi =	
Strength Level	psi =	18.5
Shear.....Allowable	psi =	44.2
Anet (Masonry)	in2 =	
Wall Weight	psf =	100.0
Rebar Depth 'd'	in =	6.25

Masonry Data

f'm	psi =	
Fs	psi =	
Solid Grouting	=	
Modular Ratio 'n'	=	
Equiv. Solid Thick.	=	
Masonry Block Type	=	
Masonry Design Method	=	ASD

Concrete Data

f'c	psi =	2,500.0
Fy	psi =	40,000.0

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft ret. wall with Key

Concrete Stem Rebar Area Details

	<u>Vertical Reinforcing</u>	<u>Horizontal Reinforcing</u>
Bottom Stem		
As (based on applied moment) :	0.1795 in ² /ft	
0.0018bh : 0.0018(12)(8) :	0.1728 in ² /ft	
	=====	
Required Area :	0.1795 in ² /ft	Horizontal Reinforcing Options :
Provided Area :	0.24 in ² /ft	One layer of : Two layers of :
Maximum Area :	1.27 in ² /ft	#4@ 13.89 in #4@ 27.78 in #5@ 21.53 in #5@ 43.06 in #6@ 30.56 in #6@ 61.11 in

Footing Data

Toe Width	=	2.00 ft
Heel Width	=	2.00
Total Footing Width	=	4.00
Footing Thickness	=	12.00 in
Key Width	=	8.00 in
Key Depth	=	30.00 in
Key Distance from Toe	=	2.00 ft
f'c = 2,500 psi	Fy =	40,000 psi
Footing Concrete Density	=	150.00 pcf
Min. As %	=	0.0018
Cover @ Top	2.00	@ Btm.= 3.00 in

Footing Design Results

	<u>Toe</u>	<u>Heel</u>
Factored Pressure	= 1,692	0 psf
Mu' : Upward	= 2,811	148 ft-#
Mu' : Downward	= 360	864 ft-#
Mu: Design	= 2,451 OK	716 ft-# OK
phiMn	= 6,646	7,432 ft-#
Actual 1-Way Shear	= 15.63	8.32 psi
Allow 1-Way Shear	= 75.00	75.00 psi
Toe Reinforcing	= # 4 @ 9.26 in	
Heel Reinforcing	= # 4 @ 9.25 in	
Key Reinforcing	= # 4 @ 10.00 in	
Footing Torsion, Tu	= 0.00 ft-lbs	
Footing Allow. Torsion, phi Tu	= 0.00 ft-lbs	

If torsion exceeds allowable, provide supplemental design for footing torsion.

Other Acceptable Sizes & Spacings

Toe: #4@ 9.25 in, #5@ 14.35 in, #6@ 20.37 in, #7@ 27.77 in, #8@ 36.57 in, #9@ 46.29 in, #10@ 58.79 in

Heel: #4@ 9.25 in, #5@ 14.35 in, #6@ 20.37 in, #7@ 27.77 in, #8@ 36.57 in, #9@ 46.29 in, #10@ 58.79 in

Key: #4@ 10 in, #5@ 15.5 in, #6@ 18 in, #7@ 18 in,

Min footing T&S reinf Area	1.04 in ²
Min footing T&S reinf Area per foot	0.26 in ² /ft
If one layer of horizontal bars:	If two layers of horizontal bars:
#4@ 9.26 in	#4@ 18.52 in
#5@ 14.35 in	#5@ 28.70 in
#6@ 20.37 in	#6@ 40.74 in

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft ret. wall with Key

Summary of Overturning & Resisting Forces & Moments

ItemOVERTURNING.....		RESISTING.....		
	Force lbs	Distance ft	Moment ft-#	Force lbs	Distance ft	Moment ft-#
HL Act Pres (ab water tbl)	857.5	2.33	2,000.8	Soil Over HL (ab. water tbl)	880.0	3.33
HL Act Pres (be water tbl)				Soil Over HL (bel. water tbl)		3.33
Hydrostatic Force				Water Table		2,933.3
Buoyant Force	=			Sloped Soil Over Heel	=	
Surcharge over Heel	=			Surcharge Over Heel	=	
Surcharge Over Toe	=			Adjacent Footing Load	=	
Adjacent Footing Load	=			Axial Dead Load on Stem	=	
Added Lateral Load	=			* Axial Live Load on Stem	=	
Load @ Stem Above Soil	=			Soil Over Toe	=	
Seismic Earth Load	=	205.8	3.50	Surcharge Over Toe	=	
Seismic Stem Self Wt	=	91.0	4.25	Stem Weight(s)	=	650.0
				Earth @ Stem Transitions	=	2.33
Total	=	1,154.3	O.T.M. =	Footing Weight	=	1,516.7
				Key Weight	=	1,200.0
				Vert. Component	=	583.3
					Total =	2,380.0 lbs R.M.=
						6,233.3

Resisting/Overturning Ratio = **2.01**
Vertical Loads used for Soil Pressure = 2,380.0 lbs

If seismic is included, the OTM and sliding ratios may be 1.1 per section 1807.2.3 of IBC.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

* Axial live load NOT included in total displayed, or used for overturning resistance, but is included for soil pressure calculation.

Tilt

Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus 250.0 pci

Horizontal Defl @ Top of Wall (approximate only) 0.055 in

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft ret. wall with Key

Rebar Lap & Embedment Lengths Information

Stem Design Segment: Bottom

Stem Design Height: 0.00 ft above top of footing

Lap Splice length for #4 bar specified in this stem design segment (25.4.2.4a) = 15.60 in
Development length for #4 bar specified in this stem design segment = 12.00 in

Hooked embedment length into footing for #4 bar specified in this stem design segment = 0.00 in
As Provided = 0.2400 in²/ft
As Required = 0.2394 in²/ft

Cantilevered Retaining Wall

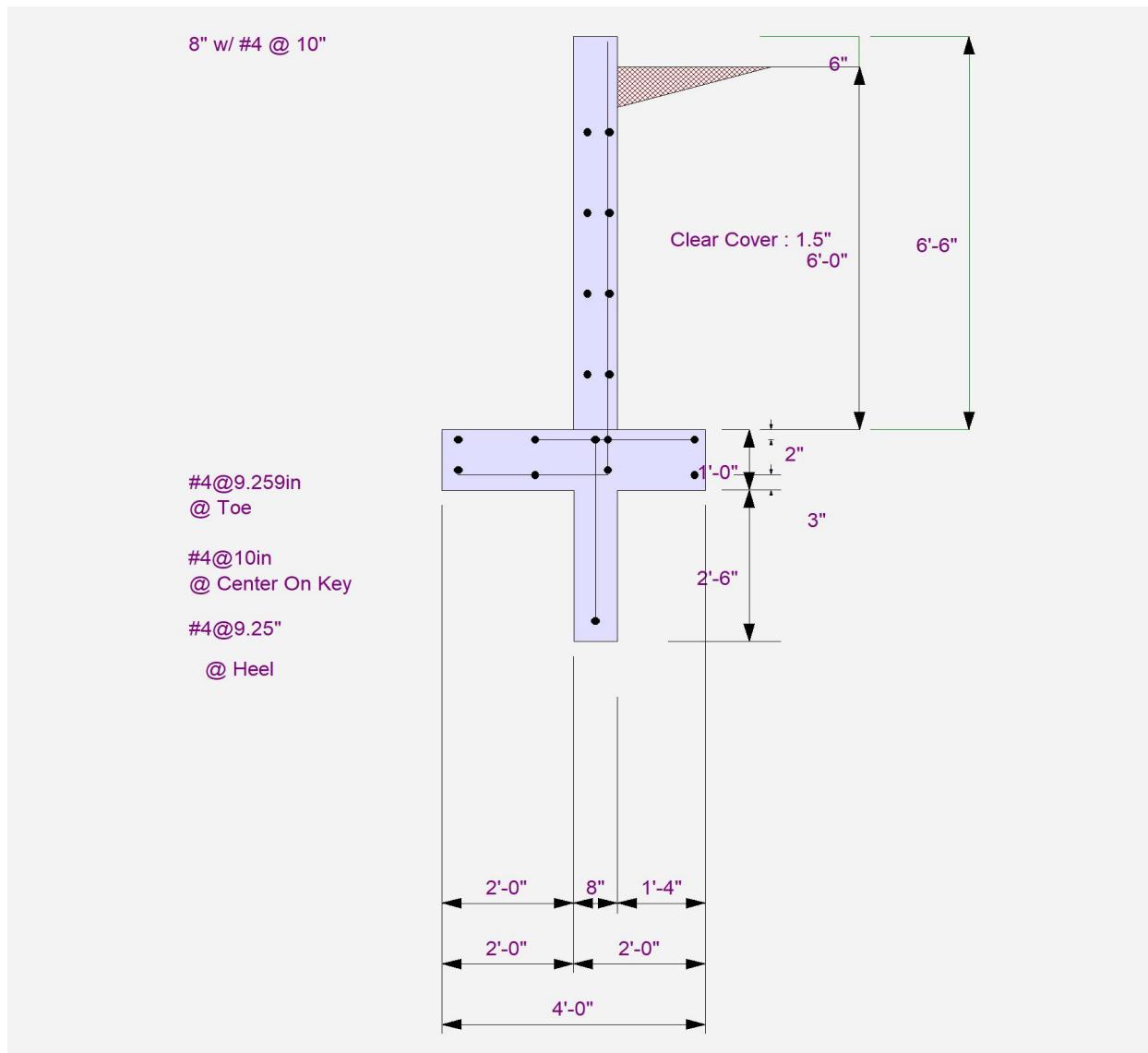
Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft ret. wall with Key



Cantilevered Retaining Wall

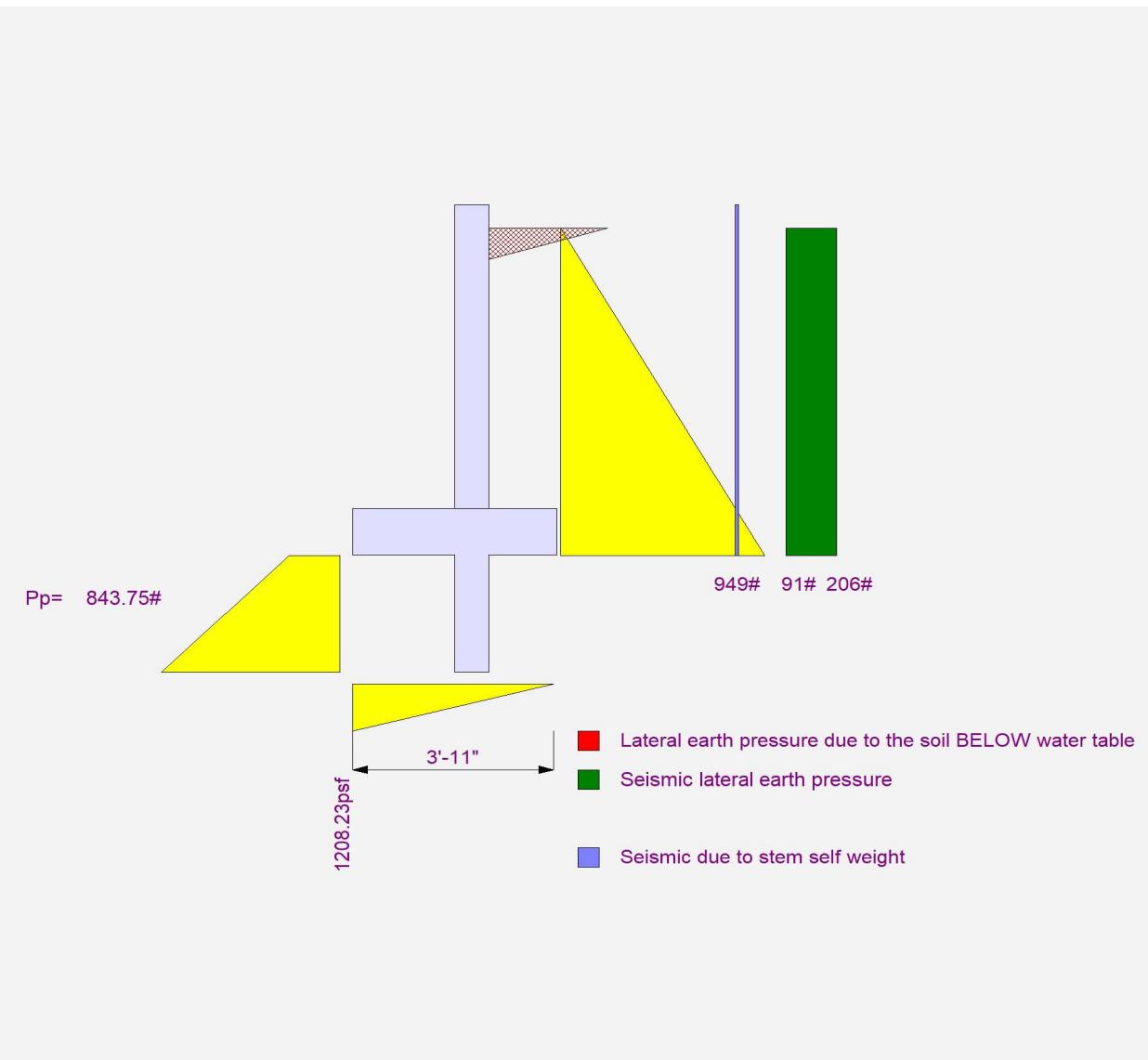
Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.08.30

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 6ft ret. wall with Key



Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.04.05

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 10ft wall

Code Reference:

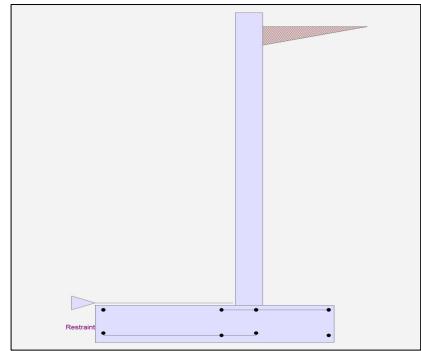
Calculations per IBC 2021 1807.3, ASCE 7-16

Criteria

Retained Height	=	10.00 ft
Wall height above soil	=	0.50 ft
Slope Behind Wall	=	0.00
Height of Soil over Toe	=	0.00 in
Water table above bottom of footing	=	0.0 ft

Soil Data

Allow Soil Bearing	=	1,500.0 psf
Equivalent Fluid Pressure Method	=	
Active Heel Pressure	=	35.0 psf/ft
	=	
Passive Pressure	=	150.0 psf/ft
Soil Density, Heel	=	110.00 pcf
Soil Density, Toe	=	110.00 pcf
Footing Soil Friction	=	0.400
Soil height to ignore for passive pressure	=	12.00 in



Surcharge Loads

Surcharge Over Heel	=	0.0 psf
Used To Resist Sliding & Overturning	=	
Surcharge Over Toe	=	0.0
Used for Sliding & Overturning	=	

Axial Load Applied to Stem

Axial Dead Load	=	0.0 lbs
Axial Live Load	=	0.0 lbs
Axial Load Eccentricity	=	0.0 in

Lateral Load Applied to Stem

Lateral Load	=	0.0 #/ft
...Height to Top	=	0.00 ft
...Height to Bottom	=	0.00 ft
Load Type	=	Wind (W) (Service Level)
Wind on Exposed Stem	=	0.0 psf (Strength Level)

Adjacent Footing Load

Adjacent Footing Load	=	0.0 lbs
Footing Width	=	0.00 ft
Eccentricity	=	0.00 in
Wall to Ftg CL Dist	=	0.00 ft
Footing Type	=	Spread Footing
Base Above/Below Soil at Back of Wall	=	0.0 ft
Poisson's Ratio	=	0.300

Earth Pressure Seismic Load

Method : Uniform		
Multiplier Used	=	10.000

(Multiplier used on soil density)

Uniform Seismic Force = 113.333
Total Seismic Force = 1,284.444

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.04.05

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 10ft wall

Design Summary

Wall Stability Ratios

Overturning = 1.92 OK
Slab Resists All Sliding !

Global Stability = 1.56

Total Bearing Load = 5,146 lbs
...resultant ecc. = 14.37 in

Eccentricity within middle third

Soil Pressure @ Toe = 1,413 psf OK
Soil Pressure @ Heel = 6 psf OK
Allowable = 1,500 psf

Soil Pressure Less Than Allowable

ACI Factored @ Toe = 1,978 psf
ACI Factored @ Heel = 9 psf
Footing Shear @ Toe = 27.9 psi OK
Footing Shear @ Heel = 16.8 psi OK
Allowable = 75.0 psi

Sliding Calcs

Lateral Sliding Force = 3,146.9 lbs

Vertical component of active lateral soil pressure IS
NOT considered in the calculation of soil bearing

Load Factors

Building Code
Dead Load 1.200
Live Load 1.600
Earth, H 1.600
Wind, W 1.600
Seismic, E 1.000

Stem Construction

Design Height Above Ftg ft = Stem OK 0.00

Wall Material Above "Ht" = Concrete
Design Method = SD SD SD
Thickness = 10.00
Rebar Size = # 6
Rebar Spacing = 10.00
Rebar Placed at = Edge

Design Data

fb/FB + fa/Fa = 0.901

Total Force @ Section

Service Level lbs =
Strength Level lbs = 3,933.3

Moment....Actual

Service Level ft-# =
Strength Level ft-# = 15,000.0
Moment.....Allowable = 16,636.7

Shear....Actual

Service Level psi =
Strength Level psi = 43.0
Shear.....Allowable psi = 53.8
Anet (Masonry) in2 =
Wall Weight psf = 125.0
Rebar Depth 'd' in = 7.63

Masonry Data

f'm psi =
Fs psi =
Solid Grouting =
Modular Ratio 'n' =
Equiv. Solid Thick. =
Masonry Block Type =
Masonry Design Method = ASD

Concrete Data

f'c psi = 2,500.0
Fy psi = 60,000.0

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.04.05

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 10ft wall

Concrete Stem Rebar Area Details

	<u>Vertical Reinforcing</u>	<u>Horizontal Reinforcing</u>
Bottom Stem As (based on applied moment) :	0.4562 in ² /ft	
0.0018bh : 0.0018(12)(10) :	0.216 in ² /ft	
	=====	Horizontal Reinforcing Options :
Required Area :	0.4562 in ² /ft	#4@ 11.11 in #4@ 22.22 in
Provided Area :	0.528 in ² /ft	#5@ 17.22 in #5@ 34.44 in
Maximum Area :	1.0329 in ² /ft	#6@ 24.44 in #6@ 48.89 in

Footing Data

Toe Width	=	4.25 ft
Heel Width	=	3.00
Total Footing Width	=	7.25
Footing Thickness	=	16.00 in
Key Width	=	0.00 in
Key Depth	=	0.00 in
Key Distance from Toe	=	0.00 ft
f'c = 2,500 psi	Fy = 60,000 psi	
Footing Concrete Density	=	150.00 pcf
Min. As %	=	0.0018
Cover @ Top	2.00	@ Btm.= 3.00 in

Footing Design Results

	<u>Toe</u>	<u>Heel</u>
Factored Pressure	= 1,978	9 psf
Mu' : Upward	= 14,392	482 ft-#
Mu' : Downward	= 2,168	3,662 ft-#
Mu: Design	= 12,224 OK	3,180 ft-# OK
phiMn	= 19,099	20,660 ft-#
Actual 1-Way Shear	= 27.86	16.81 psi
Allow 1-Way Shear	= 75.00	75.00 psi
Toe Reinforcing	= # 5 @ 10.76 in	
Heel Reinforcing	= # 5 @ 10.76 in	
Key Reinforcing	= None Spec'd	
Footing Torsion, Tu	= 0.00 ft-lbs	
Footing Allow. Torsion, phi Tu	= 0.00 ft-lbs	

If torsion exceeds allowable, provide supplemental design for footing torsion.

Other Acceptable Sizes & Spacings

Toe: #4@ 6.94 in, #5@ 10.76 in, #6@ 15.27 in, #7@ 20.83 in, #8@ 27.43 in, #9@ 34.72 in, #10@ 44.09 in

Heel: #4@ 6.94 in, #5@ 10.76 in, #6@ 15.27 in, #7@ 20.83 in, #8@ 27.43 in, #9@ 34.72 in, #10@ 44.09 in

Key: No key defined

Min footing T&S reinf Area	2.51 in ²
Min footing T&S reinf Area per foot	0.35 in ² /ft
If one layer of horizontal bars:	If two layers of horizontal bars:
#4@ 6.94 in	#4@ 13.89 in
#5@ 10.76 in	#5@ 21.53 in
#6@ 15.28 in	#6@ 30.56 in

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.04.05

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 10ft wall

Summary of Overturning & Resisting Forces & Moments

ItemOVERTURNING.....		RESISTING.....		
	Force lbs	Distance ft	Moment ft-#	Force lbs	Distance ft	Moment ft-#
HL Act Pres (ab water tbl)	2,247.8	3.78	8,491.6	Soil Over HL (ab. water tbl)	2,383.3	6.17
HL Act Pres (be water tbl)				Soil Over HL (bel. water tbl)		6.17
Hydrostatic Force				Water Table		
Buoyant Force	=			Sloped Soil Over Heel	=	
Surcharge over Heel	=			Surcharge Over Heel	=	
Surcharge Over Toe	=			Adjacent Footing Load	=	
Adjacent Footing Load	=			Axial Dead Load on Stem	=	
Added Lateral Load	=			* Axial Live Load on Stem	=	
Load @ Stem Above Soil	=			Soil Over Toe	=	
Seismic Earth Load	=	899.1	5.67	Surcharge Over Toe	=	
	=			Stem Weight(s)	=	1,312.5
	=			Earth @ Stem Transitions	=	4.67
Total	=	3,146.9	O.T.M. =	Footing Weight	=	6,125.0
				Key Weight	=	1,450.0
				Vert. Component	=	3.63
				Total =	5,145.8 lbs R.M.=	5,256.3
						26,078.5

Resisting/Overturning Ratio = **1.92**
Vertical Loads used for Soil Pressure = 5,145.8 lbs

If seismic is included, the OTM and sliding ratios may be 1.1 per section 1807.2.3 of IBC.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Sliding Resistance.

Vertical component of active lateral soil pressure IS NOT considered in the calculation of Overturning Resistance.

* Axial live load NOT included in total displayed, or used for overturning resistance, but is included for soil pressure calculation.

Tilt

Horizontal Deflection at Top of Wall due to settlement of soil

(Deflection due to wall bending not considered)

Soil Spring Reaction Modulus 250.0 pci

Horizontal Defl @ Top of Wall (approximate only) 0.057 in

The above calculation is not valid if the heel soil bearing pressure exceeds that of the toe, because the wall would then tend to rotate into the retained soil.

Project Title:
Engineer:
Project ID:
Project Descr:

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.04.05

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 10ft wall

Rebar Lap & Embedment Lengths Information

Stem Design Segment: Bottom

Stem Design Height: 0.00 ft above top of footing

Lap Splice length for #6 bar specified in this stem design segment (25.4.2.4a) = 28.08 in
Development length for #6 bar specified in this stem design segment = 21.60 in

Hooked embedment length into footing for #6 bar specified in this stem design segment = 12.60 in
As Provided = 0.5280 in²/ft
As Required = 0.4562 in²/ft

Project Title:
Engineer:
Project ID:
Project Descr:

Cantilevered Retaining Wall

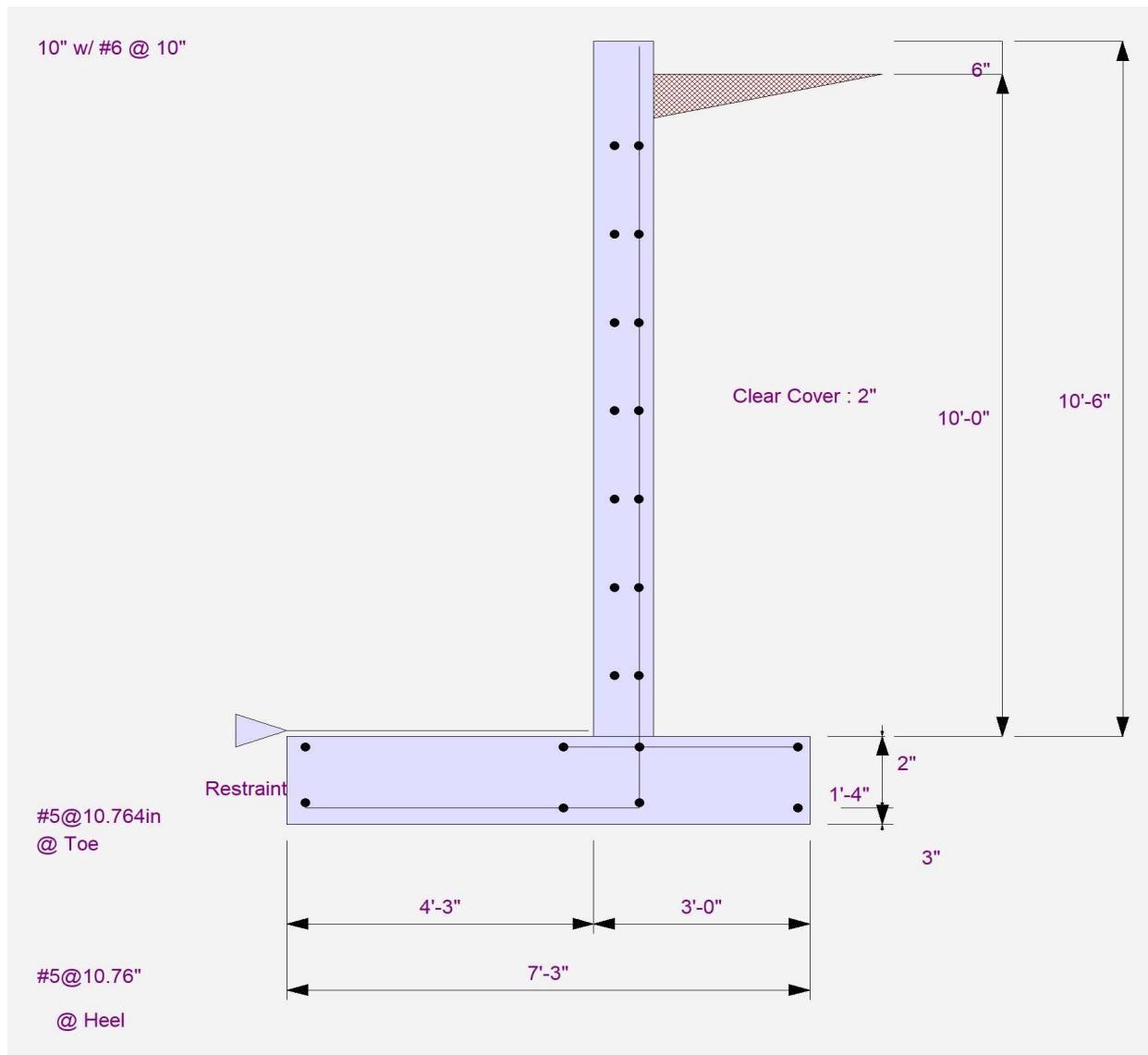
Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.04.05

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 10ft wall



Project Title:
Engineer:
Project ID:
Project Descr:

Cantilevered Retaining Wall

Project File: 23-043.ec6

LIC# : KW-06016495, Build:20.23.04.05

CK Engineering LLC

(c) ENERCALC INC 1983-2023

DESCRIPTION: 10ft wall

